

**UNIVERSIDAD AUTÓNOMA DE SAN LUÍS POTOSÍ**

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Doctorado Institucional en Ingeniería y Ciencia de Materiales

**Study on fabrication and lithium extraction properties of  
functionalized lithium ion-sieves**

PARA OBTENER EL GRADO DE  
**DOCTOR EN INGENIERÍA Y CIENCIA DE MATERIALES**

QUE PRESENTA

**Lingjie Zhang**

DIRECTORA

**Dra. Mildred Quintana Ruiz**

PATROCINADO POR SECIHTI Beca número 847199

**San Luis Potosí, S.L.P. Junio de 2026**

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**San Luis Potosí, S.L.P. Junio de 2026**

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**Lingjie Zhang**

Mexico

## Resumen

Debido a su papel crucial en la transformación energética orientada a la descarbonización, el suministro sostenible de litio (Li) se ha vuelto cada vez más crítico. La extracción de Li a partir de salmueras prácticamente inagotables se está convirtiendo en una alternativa preferente para garantizar el desarrollo sostenible de los recursos de litio, lo que exige el desarrollo de tecnologías de extracción verdes, eficientes y altamente selectivas. Los iono-tamices de litio ofrecen soluciones prometedoras para la extracción selectiva de litio a partir de salmueras, en particular los hidróxidos dobles laminares de litio-aluminio (LiAl-LDHs), gracias a su estructura de cavidades octaédricas específicamente adaptadas para  $\text{Li}^+$  y a su capacidad de desorción sin pérdidas por disolución. No obstante, aunque los LiAl-LDHs ya han sido utilizados en la extracción industrial de litio, persisten preocupaciones clave que limitan su aplicación a mayor escala.

En este trabajo, se sintetizan en primer lugar las relaciones estructura-rendimiento y los avances en la investigación de diversos iono-tamices, demostrando el alto grado de sofisticación y desarrollo alcanzado por los LiAl-LDHs. Posteriormente, al centrarse en los factores que influyen en el desempeño de los LiAl-LDHs para la extracción de Li, se resumen las principales limitaciones que restringen su desarrollo ulterior: i) baja capacidad de adsorción de  $\text{Li}^+$ ; ii) el efecto de “envenenamiento por iones sulfato ( $\text{SO}_4^{2-}$ )” en salmueras de tipo sulfato; y iii) la escasa viabilidad en salmueras de baja calidad. Con este objetivo, se desarrollan una serie de estrategias, que incluyen ingeniería de dopaje, control de las interacciones interlaminares, construcción de dominios multifuncionales y diseño molecular, para superar dichas limitaciones de los LiAl-LDHs. Como resultado, los LiAl-LDHs modificados exhiben capacidades de adsorción de  $\text{Li}^+$  significativamente mejoradas, selectividades ultraltas hacia  $\text{Li}^+$ , excelentes propiedades de resistencia al envenenamiento por sulfato y una notable estabilidad en diversos tipos de salmueras, incluyendo salmueras de lagos salinos, salmueras de tipo sulfato y salmueras de baja calidad. Sobre la base de estas ventajas, finalmente se obtiene carbonato de litio ( $\text{Li}_2\text{CO}_3$ ) de alta pureza (97.85 %) a partir de la salmuera empleando los LiAl-LDHs desarrollados. Esta tesis proporciona aportes teóricos y contribuciones técnicas para ampliar el aprovechamiento de recursos de salmuera accesibles con miras a una extracción sostenible de litio.

**Palabras clave:** Extracción de litio; Salmuera; Hidróxidos dobles laminares de litio-aluminio; Iono-tamiz; Adsorción; Modificación.

## Abstract

Owing to the crucial role in energy transformation for decarbonization, sustainable lithium (Li) supply has become increasingly critical. Li extraction from abundant brines is becoming a preferred alternative to ensure the sustainable development of Li resources, which requires green, effective, and selective extraction techniques. Lithium ion-sieves offer promising solutions for selective lithium extraction from brines, especially lithium aluminum layered double hydroxides (LiAl-LDHs) due to their tailored  $\text{Li}^+$  octahedral cavity structure and desorption without dissolution loss. While LiAl-LDHs have been used for industrial Li extraction, the crucial concerns remain regarding the wider applications.

Herein, the structure-performance relationships and research progress of various ion-sieves are first synthesized, demonstrating the sophistication and advancement of LiAl-LDHs. Further, by focusing on the influencing factors of LiAl-LDHs for Li extraction, the main limitations that restrict their further development were summarized: i) low  $\text{Li}^+$  adsorption capacity; ii) ‘sulfate ion ( $\text{SO}_4^{2-}$ ) poisoning’ effect in  $\text{SO}_4^{2-}$ -type brines; and iii) poor feasibility in low-quality brines. To this end, a series of strategies are developed, including doping engineering, steering interlayer interaction, constructing multiple functional domains, and molecular tailoring engineering, to overcome these concerns of LiAl-LDHs. Accordingly, the modified LiAl-LDHs exhibit significantly improved  $\text{Li}^+$  adsorption capacities, high  $\text{Li}^+$  selectivity, excellent anti-sulfate poisoning features and stabilities in various brines, involving salt lake brines,  $\text{SO}_4^{2-}$ -type brines, and low-quality brines. On the basis of these merits, high-purity (97.85%)  $\text{Li}_2\text{CO}_3$  is finally produced from the brine using the as-obtained LiAl-LDHs. The thesis provides theoretical insights and technical contributions for expanding accessible brine resources towards sustainable Li extraction.

**Keywords:** Lithium extraction; Brine; Lithium aluminum layered double hydroxides; Ion-sieve; Adsorption; Modification

## Extended Abstract

Driven by global electrification and decarbonization strategies, the market demand for lithium (Li) is skyrocketing. To enable the sustainable supply of Li, there is an urgent and timely need to extract and recover Li from various resources, especially abundant brines. The development of lithium adsorbents constructed from selective nano-ion sieves opens an advanced avenue for Li extraction from brines. Therein, lithium aluminum layered double hydroxides (LiAl-LDHs) have emerged as the most promising adsorbents for lithium extraction from brines. However, the wider application of LiAl-LDHs is challenging, the crucial concerns remain to be resolved.

Here, the structure-performance relationships and research progress of various ion-sieves are first synthesized, including LiAl-LDHs, lithium titanium oxide type lithium-ion sieves (LTO-LISs), lithium manganese oxide type lithium-ion sieves (LMO-LISs), ion-imprinted polymers (Li-IIPs) and ion-exchange resins. Taking the adsorption capacity, adsorption rate, selectivity, reusability, and cost into account, LiAl-LDHs present are the sophistication and advancement for industrial applications. Further, the main limitations that restrict the further development of LiAl-LDHs are summarized through revealing the influencing factors of Li extraction, namely, low Li<sup>+</sup> adsorption capacity, ‘sulfate ion (SO<sub>4</sub><sup>2-</sup>) poisoning’ effect in SO<sub>4</sub><sup>2-</sup>-type brines, and poor feasibility in low-quality brines.

To improve suboptimal Li<sup>+</sup> adsorption performance of LiAl-LDHs, a doping engineering strategy is developed to fabricate novel Zn<sup>2+</sup>-doped LiAl-LDH (LiZnAl-LDH). Combining experiments and simulation calculations, it is revealed that the doping engineering endows LiZnAl-LDH with increased specific surface area, hydrophilic, surface attraction for Li<sup>+</sup>, and oxygen vacancies, which increase the adsorption energy ( $E_{ad}$ ) of Li<sup>+</sup> adsorption, while reduce Gibbs free energy ( $\Delta G$ ) of Li<sup>+</sup> insertion and energy barrier of Li<sup>+</sup> diffusion. Consequently, LiZnAl-LDH exhibits the remarkable higher Li<sup>+</sup> adsorption capacity (13.4 mg/g) and selectivity (separation factors of 213, 834, 171 for Li<sup>+</sup>/K<sup>+</sup>, Li<sup>+</sup>/Na<sup>+</sup>, Li<sup>+</sup>/Mg<sup>2+</sup>, respectively), as well as excellent reusability in the real brine compared to the pristine LiAl-LDH.

To impart an anti-sulfate poisoning feature to LiAl-LDHs, a steering interlayer interaction strategy by embedding portion of PO<sub>4</sub><sup>3-</sup> into interlayers of LiAl-LDH beads (BLDH-P) is developed. Owing to the lower binding energy ( $E_b$ ) and stronger diffusion energy barrier of SO<sub>4</sub><sup>2-</sup> within interlayers, BLDH-P features the property of preventing

SO<sub>4</sub><sup>2-</sup> intercalation, with the unchanged adsorption and desorption capacity in Lop Nor brine (the largest SO<sub>4</sub><sup>2-</sup>-type brine in the world). BLDH-P also shows excellent Li extraction performance, as the results of enlarged interlayer spacing and selective electrostatic repulsion. The static and dynamic Li<sup>+</sup> uptake reaches 5.26 mg/g and 3.96 mg/g, with high separation factors of 39.84, 48.14, and 144.87 for Li<sup>+</sup>/K<sup>+</sup>, Li<sup>+</sup>/Na<sup>+</sup>, and Li<sup>+</sup>/Mg<sup>2+</sup>, respectively, superior to those of reported and commercialized LiAl-LDH.

To strengthen the anti-sulfate poisoning performance of LiAl-LDHs, an organic modification strategy is developed to construct multiple functional domains of LiAl-LDHs (LiAl-LDH/PAM) using polyacrylamide (PAM). Benefiting from the newly created multiple SO<sub>4</sub><sup>2-</sup> repelling domains in the interface and interlayer of the LiAl-LDH/PAM, the energy barrier for SO<sub>4</sub><sup>2-</sup> migration over interface and interlayer is significantly increased, which hinders the SO<sub>4</sub><sup>2-</sup> intercalation during long-term Li cycling extraction. Accordingly, anti-sulfate poisoning properties exceed all previously reported LiAl-LDHs, where the adsorption capacity loss of the LiAl-LDH/PAM is less than 6% in ten cycle experiments in Lop Nor brine. Additionally, PAM enhances the affinity between the LiAl-LDHs and Li<sup>+</sup>, resulting in the excellent Li<sup>+</sup> selectivity and the maximum adsorption capacity (13.25 mg/g).

To realize high-efficiency lithium recovery from diverse low-quality brines, a proof-of-concept polymer side-chain structure design (SCSD) strategy that delivers intralayer engineering of LiAl-LDHs (LiAl-LDH/PR) with functional polymers is developed. The results of simulations and experiments demonstrate that the SCSD strategy engineers LiAl-LDHs with a Li<sup>+</sup>-enriched intralayer domain, which overcomes the diffusion-limited Li<sup>+</sup> uptake in low-quality brines. Notably, the local chemical microenvironment and spatial microstructure of LiAl-LDH/PR can be readily tuned through rational designs of side-chains of polymer to accommodate Li extraction from different brines. Consequently, LiAl-LDH/PR realizes an ultra-high recovery efficiency of 91.62% from real oilfield brine with ultra-low Li<sup>+</sup> concentration of 19.7 mg/L and a sustainable Li extraction and production of high-purity Li<sub>2</sub>CO<sub>3</sub> from one of the largest low-quality brines in the world.

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## Contents

Acknowledgement .....	I
Resumen.....	I
Abstract.....	II
Extended Abstract .....	III
Contents .....	V
Index of Figures .....	VIII
Index of Tables.....	XIV
Chapter 1. Introduction.....	1
1.1. Justification.....	1
1.2. Hypothesis.....	2
1.3. Objectives .....	3
1.3.1. General objective .....	3
1.3.2. Goals .....	3
1.4. References.....	4
Chapter 2. Background.....	7
2.1. Introduction.....	7
2.2. Various lithium adsorbents and structure-property relationship .....	9
2.2.1. LiAl-LDHs.....	9
2.2.2. LTO-LISs .....	11
2.2.3. LMO-LISs.....	12
2.2.4. Ion-Imprinted polymers .....	15
2.2.5. Other lithium adsorbents.....	16
2.3. Comparison of various lithium adsorbents .....	17
2.4. Conclusions and perspectives .....	20
2.5. References.....	20
Chapter 3. Doping engineering of lithium-aluminum layered double hydroxides for high-efficiency lithium extraction from salt lake brines .....	27
3.1. Introduction.....	27
3.2. Experimental section.....	29
3.2.1. Material synthesis .....	29
3.2.2. Characterizations.....	30

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3.2.3. Lithium-ion extraction performance evaluation .....	30
3.2.4. Calculation details.....	31
3.3. Results and discussion .....	32
3.3.1. Optimization of doping strategy .....	32
3.3.2. Fabrication and characterization of LiZnAl-LDH .....	33
3.3.3. Lithium-ion extraction performance .....	38
3.3.4. Mechanisms of enhanced performance for lithium extraction by Zn-doping .....	42
3.4. Conclusions.....	44
3.5. References.....	45
Chapter 4. Steering interlayer interaction of lithium-aluminum layered double hydroxide beads for stable lithium extraction from sulfate-type brines .....	49
4.1. Introduction.....	49
4.2. Experimental section.....	51
4.2.1. Reagents and materials .....	51
4.2.2. Preparation of BLDH-P .....	51
4.2.3. Characterizations.....	52
4.2.4. Lithium-ion extraction .....	52
4.2.5. Theoretical calculations .....	53
4.3. Results and discussion .....	54
4.3.1. Construction and optimization of LiAl-LDH beads .....	54
4.3.2. Characterization of LiAl-LDH beads intercalated with $\text{PO}_4^{3-}$ .....	57
4.3.3. Lithium extraction performance in sulfate-type brines.....	60
4.3.4. Mechanisms of stable extraction in sulfate-type brines.....	66
4.4. Conclusions.....	71
4.5. References.....	72
Chapter 5. Constructing multiple functional domains of lithium aluminum layered double hydroxides for sustainable lithium extraction in sulfate-type brines ..	76
5.1. Introduction.....	76
5.2. Experimental section.....	77
5.2.1. Reagents and materials .....	77
5.2.2. Preparation of LiAl-LDH-PAM .....	78
5.2.3. Characterizations.....	78
5.2.4. Lithium-ion extraction .....	78

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5.2.5. Theoretical calculations .....	79
5.2.6. Numerical simulation.....	79
5.3. Results and discussion .....	81
5.3.1. Synthesis and characterization.....	81
5.3.2. Lithium extraction performance .....	85
5.3.3. Anti-sulfate ion poisoning performance.....	87
5.3.4. Mechanisms of anti-sulfate ion poisoning.....	92
5.4. Conclusions.....	94
5.5. References.....	94
Chapter 6. Molecular tailoring engineering of lithium aluminum layered double hydroxides for lithium extraction from low-quality brines.....	97
6.1. Introduction.....	97
6.2. Experimental section.....	99
6.2.1. Reagents and materials .....	99
6.2.2. Preparation of LiAl-LDH/PR.....	100
6.2.3. Characterizations.....	100
6.2.4. Lithium-ion extraction and $\text{Li}_2\text{CO}_3$ production .....	101
6.2.5. Theoretical calculations .....	101
6.2.6. Numerical simulation.....	102
6.3. Results and discussion .....	102
6.3.1. Intralayer/interlayer engineering design .....	102
6.3.2. Synthesis and characterization.....	106
6.3.3. Lithium extraction performance .....	109
6.3.4. Lithium recovery and precipitation of $\text{Li}_2\text{CO}_3$ .....	115
6.3.5. Practical application assessment.....	119
6.4. Conclusions.....	121
6.5. References.....	122
Chapter 7. Conclusions.....	126
Chapter 8. Perspectives.....	128
Appendix I. Articles published during the Ph. D studies.....	129
Appendix II. Experimental data.....	132

## Index of Figures

Figure 2.1 Global lithium resource reserve in brines and ores, and the range of Li concentration in different type of brines. ....	7
Figure 2.2 Schematic of the technologies for lithium recovery from brines. (a) The general recovery process. $\text{Li}^+$ separation stages include three technologies, (b) adsorption, also known as ion exchange, (c) nanofiltration, NF, and (d) electro dialysis. $\text{Li}^+$ concentration stages include two technologies, (e) reverse osmosis, RO, and (f) evaporation concentration. ....	8
Figure 2.3 Schematic of selective lithium recovery by lithium adsorbents.....	9
Figure 2.4 Schematic structures of various lithium adsorbents. (a) LiAl-LDH, (b) $\text{Li}_2\text{TiO}_3$ , (c) $\text{Li}_4\text{Ti}_5\text{O}_{12}$ , (d) $\text{LiMn}_2\text{O}_4$ , (e) $\text{Li}_{1.33}\text{Mn}_{1.67}\text{O}_4$ , (f) 12-Crown-4, (g) Calix[4]arene, (h) $\text{LiFePO}_4$ ..	11
Figure 2.5 Comparison of various lithium adsorbents. (a) Adsorption capacity, (b) adsorption equilibrium time, (c) $\text{Li}^+$ selectivity for, (d) regeneration stability, and (e) optimal pH value of LiAl-LDHs, LTO-LIS, TMO-LIS, Li-IIPs, and Resins. ....	18
Figure 2.6 Performance heatmap of LiAl-LDHs, LTO-LIS, TMO-LIS, Li-IIPs, and Resins. ....	19
Figure 3.1 (a) The adsorption capacity of $\text{Li}^+$ on LiAl-LDHs doped with various metal cations; (b) The surface zeta potential of LiAl-LDHs doped with various metal cations; (c) The relationship between surface zeta potential and adsorption capacity of $\text{Li}^+$ .....	33
Figure 3.2 The schematic illustration of the fabrication strategy for LiZnAl-LDHs.....	33
Figure 3.3 (a) TEM images, (b-c) HRTEM image, (d) SAED pattern and (e-f) STEM-EDS of LiZnAl-LDH-5%.....	34
Figure 3.4 XRD patterns of the LiAl-LDH and LiZnAl-LDHs. ....	35
Figure 3.5 Crystal sizes of the LiAl-LDH and LiZnAl-LDHs based on Scherrer equation. ...	35
Figure 3.6 $\text{N}_2$ adsorption-desorption isotherms of the LiAl-LDH and LiZnAl-LDHs. ....	36
Figure 3.7 (a) Raman spectra and (b) EPR analyses of the LiAl-LDH and LiZnAl-LDHs. ...	37
Figure 3.8 XPS spectra of the LiAl-LDH and LiZnAl-LDH-5%.....	37
Figure 3.9 Contact angles of the LiAl-LDH and LiZnAl-LDHs.....	38
Figure 3.10 (a) The $\text{Li}^+$ adsorption capacity and (b) increase of LiZnAl-LDHs with different $\text{Zn}^{2+}$ doping amounts in brine. ....	38
Figure 3.11 The intraparticle diffusion model for $\text{Li}^+$ adsorption process of the LiAl-LDH and LiZnAl-LDHs.....	39
Figure 3.12 The comparison of the selectivity of LiZnAl-LDHs with different content of $\text{Zn}^{2+}$ for (a) $\text{Li}^+/\text{K}^+$ , (b) $\text{Li}^+/\text{Na}^+$ , and (c) $\text{Li}^+/\text{Mg}^{2+}$ in the brine. ....	40
Figure 3.13 (a) The adsorption capacity of $\text{Li}^+$ with different initial concentration on the LiAl-LDH and LiZnAl-LDH-5%. (b) Langmuir and (c) Freundlich models of $\text{Li}^+$ on pristine LiAl-LDH and LiZnAl-LDH-5%.....	40
Figure 3.14 The $\text{Li}^+$ desorption capacity of LiZnAl-LDH-5%. Inset is the $\text{Mg}^{2+}/\text{Li}^+$ mass ratios in brine and desorption solution. ....	41
Figure 3.15 (a) The reusability and stability of LiZnAl-LDH-5%. (b) The SEM image of LiZnAl-LDH-5% after lithium extraction. (c) XRD patterns of LiZnAl-LDH-5% before and	

after lithium extraction. ....	42
Figure 3.16 Comparison of Li extraction performance of different lithium-aluminum layered double hydroxides. ....	42
Figure 3.17 Optimal configuration of hydrated lithium ions.....	43
Figure 3.18 (a) Three-steps schematic representation of Li extraction on pristine LiAl-LDH and LiZnAl-LDH. (b) Theoretical calculation analysis: The adsorption energy of $\text{Li}(\text{H}_2\text{O})_4^+$ on pristine LiAl-LDH and LiZnAl-LDHs surface; (c) The Gibbs free energy of Li-insertion reaction on pristine LiAl-LDH and LiZnAl-LDHs; (d) The diffusion energy barrier of $\text{Li}^+$ within pristine LiAl-LDH and LiZnAl-LDHs. ....	44
Figure 4.1 Schematic illustration of the fabrication strategy for BLDH-P beads.....	54
Figure 4.2 Optical photographs of the BLDH-P with various PVC/PAN ratios after 24h of vigorous shaking in brine. ....	55
Figure 4.3 Mass losses, dissolution amounts of $\text{Al}^{3+}$ and dissolution COD of BLDH-P beads with various PVC/PAN ratios in strong acid and alkali solutions. ....	55
Figure 4.4 (a) Contact angles, and (b) SEM images of BLDH-P beads with various PVC/PAN ratios. ....	56
Figure 4.5 $\text{Li}^+$ adsorption capacities of BLDH-P beads with various PVC/PAN ratios. ....	56
Figure 4.6 Schematic illustration of effect of PVC/PAN ratios on BLDH-P beads. ....	57
Figure 4.7 XRD patterns of LiAl-LDH-Cl powder, LiAl-LDH-P powder and BLDH-P bead. ....	57
Figure 4.8 FT-IR spectra of PVC, PAN and BLDH-P bead. ....	58
Figure 4.9 SEM images and EDS mapping images of BLDH-P internal.....	58
Figure 4.10 (a) Nitrogen adsorption-desorption isotherms, and (b) pore size distributions of BLDH-Cl and BLDH-P bead. ....	59
Figure 4.11 ESP distributions of $\text{Cl}^-$ , $\text{SO}_4^{2-}$ , $\text{PO}_4^{3-}$ and their solvation energies. ....	60
Figure 4.12 (a) Adsorption kinetics of $\text{Li}^+$ on BLDH-P and BLDH-Cl during the adsorption process. (b) The pseudo-first-order and (c) pseudo-second-order kinetic models of the BLDH-P and BLDH-Cl. ....	60
Figure 4.13 The intraparticle diffusion model of $\text{Li}^+$ on BLDH-P and BLDH-Cl during the adsorption process. ....	61
Figure 4.14 (a) Langmuir and (b) Freundlich isotherm models of BLDH-P and BLDH-Cl. ..	62
Figure 4.15 (a) Desorption capacities of BLDH-P and BLDH-Cl during ten desorption cycles. (b) The XRD patterns of LiAl-LDH-Cl powder, BLDH-Cl and BLDH-P after ten adsorption-desorption cycles. ....	63
Figure 4.16 Adsorption capacities of BLDH-P and BLDH-Cl during ten cycles.....	63
Figure 4.17 The selectivity of BLDH-P and BLDH-Cl.....	64
Figure 4.18 (a) Schematic illustration of the fixed bed column device. (b) The $\text{Li}^+$ breakthrough curves and (c) the $\text{Li}^+$ adsorption curves of BLDH-Cl and BLDH-P. ....	64
Figure 4.19 Comparison of $\text{Li}^+$ dynamic extraction properties of different LiAl-LDHs.....	65
Figure 4.20 The dynamic desorption capacity of BLDH-P in fixed bed. ....	65

Figure 4.21 (a) The dynamic adsorption-desorption cycling adsorption performance of BLDH-P. (b) SEM images and (c) XRD patterns of BLDH-P after different cycling numbers.....	66
Figure 4.22 The optimized anion structure and binding energy between anions. ....	67
Figure 4.23 (a) Ionic potentials of different anions. (b) Quantitative diagram of anion interaction disparity. ....	67
Figure 4.24 Amounts of interlayer $\text{SO}_4^{2-}$ of BLDH-P and BLDH-Cl during five desorption cycles. ....	68
Figure 4.25 (a-e) The EDS spectra of BLDH-Cl after various desorption times. (f) The amount of S element in BLDH-Cl from the results of EDS spectra. (g-k) The EDS spectra of BLDH-P after various desorption times. (l) The amount of S element in BLDH-P from the results of EDS spectra.....	69
Figure 4.26 Relative energies for the diffusion of $\text{SO}_4^{2-}$ and $\text{Cl}^-$ within LiAl-LDH-P or LiAl-LDH-Cl.....	70
Figure 4.27 Optimized structures of initial state, transition state and final state configurations for $\text{SO}_4^{2-}/\text{Cl}^-$ diffusion reaction within LiAl-LDH-P or LiAl-LDH-Cl.....	70
Figure 4.28 Schematic illustration of adsorption, desorption and re-adsorption processes of BLDH-P and BLDH-Cl. ....	71
Figure 5.1 Two-dimension model of LiAl-LDHs and bulk phase of $\text{Li}_2\text{SO}_4$ . ....	80
Figure 5.2 Schematic illustration of the LiAl-LDH modified with PAM.....	81
Figure 5.3 (a) TEM image, (b) HRTEM image, (c) SAED pattern of the pristine LiAl-LDH (d) TEM image, (e) HRTEM image, (f) SAED pattern of the LiAl-LDH/PAM. tom distance profiles from lattice fringes of (003) plane of (g) the pristine LiAl-LDH and (h) the LiAl-LDH/PAM. (i) Mapping images of the LiAl-LDH/PAM.....	82
Figure 5.4 XRD patterns of the pristine LiAl-LDH and LiAl-LDH/PAM. ....	83
Figure 5.5 Zeta potentials of the pristine LiAl-LDH and LiAl-LDH/PAM.....	83
Figure 5.6 (a) XPS survey spectra of the pristine LiAl-LDH and LiAl-LDH/PAM. (b) XPS spectrum for the N 1s core level of the LiAl-LDH/PAM. ....	84
Figure 5.7 XPS spectra of O 1s core level of the pristine LiAl-LDH and LiAl-LDH/PAM. ..	84
Figure 5.8 Schematic of multiple functional domains of LiAl-LDH/PAM and interactions between LiAl-LDH and polymer building blocks.....	85
Figure 5.9 $\text{Li}^+$ adsorption kinetics of the pristine LiAl-LDH and LiAl-LDH/PAM in Lop Nor brine.....	85
Figure 5.10 (a) Pseudo-first-order and (b) pseudo-second-order kinetic models of $\text{Li}^+$ adsorption on the pristine LiAl-LDH and LiAl-LDH/PAM in Lop Nor brine. ....	86
Figure 5.11 (a) The adsorption capacity of $\text{Li}^+$ on the pristine LiAl-LDH and LiAl-LDH/PAM in Lop Nor brine with different $\text{Li}^+$ concentration. (b) Langmuir and (c) Freundlich models of $\text{Li}^+$ on the pristine LiAl-LDH and LiAl-LDH/PAM.....	86
Figure 5.12 Dispersion coefficient ( $K_d$ ) values of the pristine LiAl-LDH and LiAl-LDH/PAM in Lop Nor brine. ....	87
Figure 5.13 The $\text{SO}_4^{2-}$ exchange capacities of the pristine LiAl-LDH and LiAl-LDH/PAM..	88

Figure 5.14 Li <sup>+</sup> re-adsorption capacity of the pristine LiAl-LDH and LiAl-LDH/PAM in Lop Nor brine.....	88
Figure 5.15 Li <sup>+</sup> uptakes of the pristine LiAl-LDH and LiAl-LDH/PAM during the adsorption-desorption cycling experiments.....	89
Figure 5.16 XRD patterns of pristine LiAl-LDH and LiAl-LDH/PAM after ten adsorption-desorption cycles.....	89
Figure 5.17 The interlayer spacing of LiAl-LDHs before and after 10 adsorption-desorption cycling experiments.....	90
Figure 5.18 Contour plots of Raman spectra of (a) pristine LiAl-LDH and (b) LiAl-LDH/PAM during 10 adsorption-desorption cycling experiments.....	91
Figure 5.19 Comparison of the anti-sulfate ion poisoning performance between proposed LiAl-LDHs and reported LiAl-LDH-based adsorbents in SO <sub>4</sub> <sup>2-</sup> -type brines.....	91
Figure 5.20 The binding energy between SO <sub>4</sub> <sup>2-</sup> and PAA.....	92
Figure 5.21 Energy barrier for (a) SO <sub>4</sub> <sup>2-</sup> migration over interface and (b) interlayer of the pristine LiAl-LDH and LiAl-LDH/PAM.....	92
Figure 5.22 Energy barrier for (a) SO <sub>4</sub> <sup>2-</sup> migration over interface and (b) interlayer of the pristine LiAl-LDH and LiAl-LDH/PP.....	93
Figure 5.23 Numerical simulation of SO <sub>4</sub> <sup>2-</sup> diffusion in (a) pristine LiAl-LDH, and (b) LiAl-LDH/PAM.....	93
Figure 5.24 The SO <sub>4</sub> <sup>2-</sup> concentration as a function of Y distance from the results of Numerical simulations.....	93
Figure 6.1 Schematic of the LiAl-LDH structure and the effects of polymer side-chain structure design strategy on Li extraction of LiAl-LDHs.....	99
Figure 6.2 Electrostatic potential and the minimum electrostatic potential value of PAA, PSS, PAM.....	103
Figure 6.3 Binding energies between (a) Li <sup>+</sup> , (b) Mg <sup>2+</sup> , (c) Na <sup>+</sup> , (d) K <sup>+</sup> and PAA, PSS, PAM, respectively.....	103
Figure 6.4 Schematic of size screening effect of LiAl-LDHs on Li <sup>+</sup> .....	104
Figure 6.5 Optimized structures of (a) LiAl-LDH, (b) LiAl-LDH/PAA, (c) LiAl-LDH/PAM, and (d) LiAl-LDH/PSS.....	104
Figure 6.6 Projected density of states (PDOS) of Li and Al atoms of LiAl-LDH, LiAl-LDH/PAA, LiAl-LDH/PSS, and LiAl-LDH/PAM.....	105
Figure 6.7 Numerical simulation of Li <sup>+</sup> diffusion in (a) pristine LiAl-LDH and (b) LiAl-LDH/PSS.....	105
Figure 6.8 The Li <sup>+</sup> concentration as a function of Y distance from the results of numerical simulations.....	106
Figure 6.9 SEM images of (a) LiAl-LDH, (b) LiAl-LDH/PAA, (c) LiAl-LDH/PAM, and (d) LiAl-LDH/PSS.....	106
Figure 6.10 (a) XRD patterns and (b) zeta potentials of the pristine LiAl-LDH and LiAl-LDH/PR.....	107

Figure 6.11 XPS spectra for the C 1s, S 2p, and N 1s core level of the pristine LiAl-LDH and LiAl-LDH/PR.....	107
Figure 6.12 (a) FT-IR spectra and (b) XPS spectra for O 1s core levels of the pristine LiAl-LDH and LiAl-LDH/PR. ....	108
Figure 6.13 (a) N <sub>2</sub> adsorption-desorption isotherms and (b) pore size distributions of the pristine LiAl-LDH and LiAl-LDH/PR. ....	108
Figure 6.14 Contact angle images of the pristine LiAl-LDH and LiAl-LDH/PR. ....	109
Figure 6.15 (a) Li <sup>+</sup> uptake and (b) uptake kinetics of the pristine LiAl-LDH and LiAl-LDH/PR in Lop Nor brine. (c) Pseudo-first-order and (d) pseudo-second-order kinetic models of Li <sup>+</sup> uptake on the pristine LiAl-LDH and LiAl-LDH/PR.....	110
Figure 6.16 The intraparticle diffusion model for Li <sup>+</sup> adsorption process of the pristine LiAl-LDH and LiAl-LDH/PR in Lop Nor brine. ....	111
Figure 6.17 (a) Li <sup>+</sup> desorption kinetics of the pristine LiAl-LDH and LiAl-LDH/PR. (b) Mg <sup>2+</sup> /Li <sup>+</sup> ratios before and after extraction by the pristine LiAl-LDH and LiAl-LDH/PR. ....	111
Figure 6.18 Dispersion coefficient ( <i>K<sub>d</sub></i> ) values of the pristine LiAl-LDH and LiAl-LDH/PR in Lop Nor brine. ....	112
Figure 6.19 The radar chart for performance comparison analysis of LiAl-LDHs. ....	112
Figure 6.20 (a) Comparative analysis of brine composition (pie charts) and (b) Li uptake (bar plots) for Lop Nur brine, Diluted East Tajjinar brine, and East Tajjinar brine. ....	113
Figure 6.21 (a) Li <sup>+</sup> uptake of LiAl-LDHs in Qianjiang Oilfield brine. (b) Comparison of lithium extraction of LiAl-LDH/PR to other LiAl-LDH-based adsorbents in Li <sup>+</sup> -low aqueous with concentrations below 100 mg L <sup>-1</sup> . ....	114
Figure 6.22 (a) The lithium extraction property heatmap and (b) application scope chart of LiAl-LDH/PR in low-quality brine. ....	115
Figure 6.23 Repeated Li <sup>+</sup> uptake and accumulated Li <sup>+</sup> recovery efficiency in Lop Nor brine. ....	115
Figure 6.24 The Li extraction efficiency in Lop Nor brine. ....	116
Figure 6.25 TOC values of original brine, residual liquid and desorption solution during the adsorption-desorption process. ....	116
Figure 6.26 (a) The accumulated Li <sup>+</sup> recovery amount in the eluent. (b) The metal ion concentration of desorption solution. ....	117
Figure 6.27 (a) Schematic diagram of the purification-concentration-precipitation process for Li <sub>2</sub> CO <sub>3</sub> production. (b) Change curves of metal ion concentration during the concentration stage of desorption solution. ....	117
Figure 6.28 The proportion of lithium among the metal species in (a) the precipitation powder and (b) the purification powder. Inset is SEM images of the corresponding powder. ....	118
Figure 6.29 XRD patterns of precipitated Li <sub>2</sub> CO <sub>3</sub> before and after purification. Inset picture is the obtained Li <sub>2</sub> CO <sub>3</sub> product. ....	118
Figure 6.30 The optical photograph of the LiAl-LDH/PAM beads. ....	119
Figure 6.31 (a) Schematic of the fixed bed column device, (b) Li <sup>+</sup> adsorption capacity curves,	

(c)  $\text{Li}^+$  breakthrough and recovery ratio curves in dynamic lithium extraction process, and (d) the dynamic adsorption-desorption cycling adsorption performance of LiAl-LDH/PAM beads. .... 120

Figure 6.32 Inputs and shares of the preparation of the LiAl-LDH/PAM. .... 120

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## Index of Tables

Table 3.1 Composition of the Lop Nor brine.....	29
Table 3.2 The textural properties of the LiAl-LDH and LiZnAl-LDHs. ....	36
Table 3.3 Parameters for the reactive kinetic models of Li <sup>+</sup> on samples. ....	39
Table 3.4 The cation concentrations of adsorbents elution solutions. ....	41
Table 4.1 Properties of Lop Nor brine before and after static extraction. ....	51
Table 4.2 The textural properties of BLDH-P and BLDH-Cl.....	59
Table 4.3 Kinetic model parameters of BLDH-P and BLDH-Cl.....	61
Table 4.4 The intraparticle diffusion model calculated parameters for the adsorption of Li <sup>+</sup> on samples. ....	61
Table 4.5 Adsorption isotherm models parameters of BLDH-P and BLDH-Cl. ....	62
Table 5.1 Properties of Lop Nor brine before and after static extraction. ....	77
Table 5.2 Adsorption kinetic model parameters of the pristine LiAl-LDH and LiAl-LDH/PAM. ....	86
Table 6.1 Composition of brines used in the experiments.....	100
Table 6.2 Key parameters of multiphysics simulations. ....	102
Table 6.3 The textural properties of pristine LiAl-LDH, LiAl-LDH/PAA, LiAl-LDH/PSS and LiAl-LDH/PAM. ....	109
Table 6.4 Composition variation during the re-adsorption-desorption purification of desorption solution. ....	117
Table 6.5 Prices of substances required to synthesize materials. ....	121

## Chapter 1. Introduction

### 1.1. Justification

Lithium (Li), a critical energy metal and strategic resource, has been hailed as the “white oil” and “white gold” of the 21st century due to its huge economic success and crucial role in the energy transition, particularly in rechargeable lithium-ion batteries (LIBs) [1-4]. With the fast commercialization of LIBs, both lithium demand and price are skyrocketing. It is projected that the demand for Li is expected to grow at over 30% per annum by 2030 [5]. Unquestionably, cost-effective and sustainable extraction of lithium is imperative.

Currently, Li is mainly sourced from ores and brines, in which harvesting Li from the latter, typically salt lake brines, has aroused rising interest in the lithium industry due to the abundant reserves (tons of thousands of times more than ore reserves), environmentally friendly operation and cost-effectiveness compared to conventional ore mining [6-10]. As such, one important way to enable the sustainable supply of lithium is to develop a promising approach for lithium extraction from brines. Nevertheless, lithium in brines is normally accompanied by high concentrations of cations such as  $Mg^{2+}$ ,  $Na^+$ ,  $K^+$ , and  $Ca^{2+}$ . These cations, especially  $Mg^{2+}$ , possess similar properties to  $Li^+$  [11], causing challenges in lithium recovery from brines [12,13].

Recently, adsorption has served as a critical technique for selective lithium extraction from brines, in particular those with high  $Mg^{2+}/Li^+$  ratios, due to the advantages of the minimal pre-processing requirement of the brine, high lithium selectivity and recovery, additional concentration function, cost-effective and environment-friendly advantages [14-17]. Notably, the lithium recovery efficiency significantly depends on the lithium adsorbents. Despite numerous lithium adsorbents have been developed, lithium aluminum layered double hydroxides (LiAl-LDHs) are the only  $Li^+$  adsorbents for industrial application because of simple preparation and easy elution in water without dissolution loss [18-20]. Therefore, it is imperative to fabricate high-performance and robust-stability LiAl-LDHs for guaranteeing the sustainability of Li resources.

The structure of LiAl-LDHs is a two-dimensional structure formed by the insertion of  $Li^+$  into ordered octahedral voids in the  $Al(OH)_3$  layer, and anions (usually  $Cl^-$ ) and water molecules are also inserted into the interlayer synchronously to balance the

charge. Therefore, the chemical formula of Li/Al-LDHs can be described as  $m\text{LiCl}\cdot 2\text{Al}(\text{OH})_3\cdot n\text{H}_2\text{O}$  ( $0 < m < 1$ ) [21]. While LiAl-LDHs have been used as an industrial and commercial-scale adsorbent for lithium extraction, their more extensive applications are still limited, and crucial concerns remain: i) the low  $\text{Li}^+$  adsorption capacity. According to the chemical formula, LiAl-LDHs have inherently limited  $\text{Li}^+$  theoretical maximum adsorption capacity ( $\sim 30 \text{ mg g}^{-1}$ ), while the practical adsorption capacity of LiAl-LDH ( $4 \sim 8 \text{ mg g}^{-1}$ ) is always far below the theoretical capacity [22,23]. It is worth noting that such limited extraction efficiency will further deteriorate in low-quality brines containing low  $\text{Li}^+$  concentration, which significantly restrict the availability of lithium resource for conventional LiAl-LDHs. ii) LiAl-LDHs easily suffer from the ‘sulfate ion ( $\text{SO}_4^{2-}$ ) poisoning’ effect in  $\text{SO}_4^{2-}$ -type brines. During the lithium extraction from sulfate-rich brines that are the second most significant type of brines in the world,  $\text{SO}_4^{2-}$  readily intercalates into the interlayer of LiAl-LDHs and strongly binds to  $\text{Li}^+$ , making desorption very challenging and gradually reducing  $\text{Li}^+$  adsorption capacity [24,25]. Apparently, targeted design and innovation in LiAl-LDHs adsorbents aiming on efficient  $\text{Li}^+$  adsorption and strong anti-sulfate intercalation is important for sustainable Li extraction from various brines.

## 1.2. Hypothesis

Considering the unique layered structures, LiAl-LDHs inherently feature tunable microstructures of the host layer and microenvironments of the guest interlayer. Therefore, the intralayer and interlayer modification are two obvious practicable routes for LiAl-LDHs to enhance lithium extraction and anti-sulfate ion poisoning performances. Previous studies have confirmed that the intralayer doping engineering is a simple yet effective strategy for improving physicochemical property of adsorbents, thereby facilitating adsorption [26]. By modulating dopants and levels of doping, adsorbents show a highly flexible tunability in terms of microstructures and affinity towards various ions [27], which offers promising pathways for enhancing the  $\text{Li}^+$  adsorption capacity of LiAl-LDHs. Also, previous researches have reported that interlayer anions of LDHs can be precisely regulated via anion exchange, and the species and content of interlayer anions affect the structures and physicochemical properties of LDHs [28,29], which encourages the modification of LiAl-LDHs to hinder the intercalation of  $\text{SO}_4^{2-}$  and following “ $\text{SO}_4^{2-}$  poisoning” effect. Therefore, we hypothesize that the rational intralayer and interlayer engineering of LiAl-LDHs can enhance  $\text{Li}^+$  adsorption capacity, improve selectivity, and suppress sulfate intercalation,

thereby enabling stable lithium extraction from different types of brines.

### **1.3. Objectives**

#### **1.3.1. General objective**

Building on the structural properties of LiAl-LDHs, the study aims to design and develop a series of novel LiAl-LDH-based lithium adsorbents, overcoming the limitations of low adsorption capacity and vulnerability to sulfate poisoning. By bridging fundamental structure-function relationships with practical performance, the study offers theoretical insights and technical support for the development of next-generation high-performance lithium adsorbents. These advances hold significant promise for promoting sustainable lithium extraction from brines and securing the global lithium supply for clean energy technologies.

#### **1.3.2. Goals**

(1) Improving the  $\text{Li}^+$  adsorption capacity of LiAl-LDHs via doping engineering. By regulating dopant cation species and their dosage, the structural and physicochemical properties of LiAl-LDHs are optimized to comprehensively improve the adsorption capacity, selectivity, stability and reusability of LiAl-LDHs.

(2) Enabling an anti-sulfate poisoning feature of LiAl-LDHs via steering interlayer interaction. By modulating the intercalated anions, the interlayer environments and physicochemical properties of LiAl-LDHs are steered to create a strong electrostatic repulsion region to inhibit the intercalation of  $\text{SO}_4^{2-}$  for effective and continuous Li extraction from  $\text{SO}_4^{2-}$ -type brines.

(3) Strengthening anti-sulfate poisoning performance via constructing multiple functional domains in LiAl-LDHs. Leveraging the enriched hydroxyl groups on the interface and ion exchange feature of LiAl-LDHs,  $\text{SO}_4^{2-}$  barrier domains are created at the interface and within the interlayer by organic modification to increase barrier energies of  $\text{SO}_4^{2-}$  migration, enabling highly feasible for long-term Li extraction from  $\text{SO}_4^{2-}$ -type brine.

(4) Achieving high-efficiency lithium recovery from various low-quality brines via polymer side-chain structure design. By tuning the side-chain structure of polymer building blocks, the electric charge and ionophilic properties of LiAl-LDHs are precisely controlled for purpose-driven lithium extraction from low-quality brines with different characteristics, and ultimately producing high-purity  $\text{Li}_2\text{CO}_3$ .

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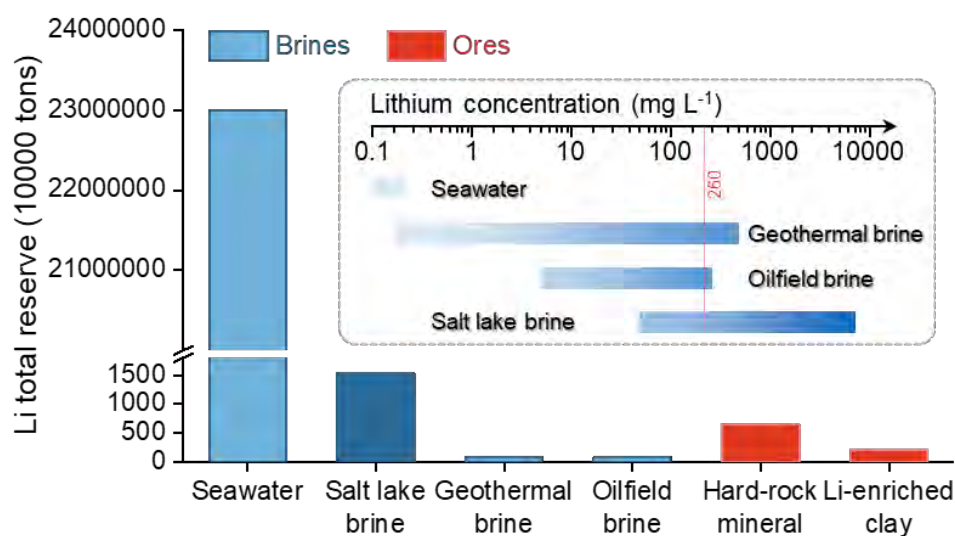
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## Chapter 2. Background

### 2.1. Introduction

Lithium (Li) is a critical element for the clean energy transition, for which the global demand is growing exponentially [1]. The demand for Li is expected to grow at over 30% per annum by 2030 [2]. The sustainable supply of Li is, therefore, particularly urgent and challenging [3]. Currently, the main sources of Li are ores (including hard-rock minerals and Li-enriched clays) and brines (including seawater, salt lake brines, geothermal brines, and oilfield brines) (Figure 2.1). Herein, harvesting Li from brines, typically salt lake brines, has attracted increasing interest from the lithium industry due to the abundant reserves (thousands of times greater than the ore reserves), environmentally friendly operation and cost-effectiveness compared to conventional ore mining [4-6]. Therefore, one important way to enable the sustainable supply of lithium is to develop a promising approach for lithium extraction from brines.

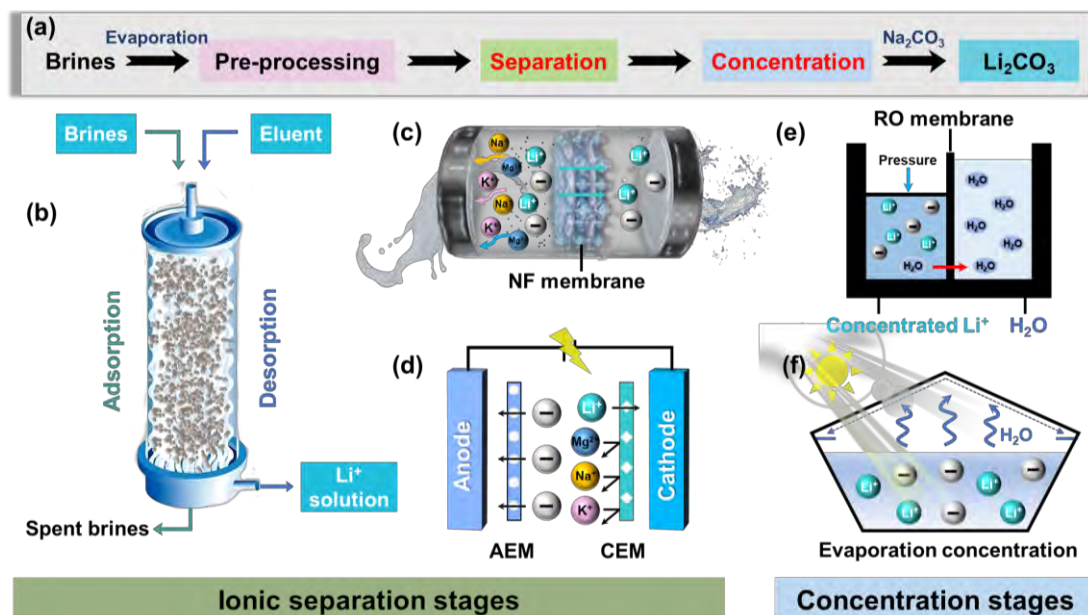


**Figure 2.1** Global lithium resource reserve in brines and ores, and the range of Li concentration in different type of brines.

(Note: The statistics are from the Mineral Commodity Summaries 2023 and the Mineral Resources Program by U.S. Geological Survey (USGS).)

Li in brines is normally accompanied by many high concentrations of cations such as  $Mg^{2+}$ ,  $Na^+$ ,  $K^+$ , and  $Ca^{2+}$ . These cations, especially  $Mg^{2+}$ , possess similar ionic radii to  $Li^+$  in bare or hydrated state [7], which causes it challenging to recover and produce

high purity lithium from brines [8,9]. In such cases, alternative lithium extraction technologies have been proposed, involving adsorption [10], nanofiltration [11], electro dialysis [12], reverse osmosis [13], evaporation concentration [14], and so forth (Figure 2.2).



**Figure 2.2** Schematic of the technologies for lithium recovery from brines. (a) The general recovery process. Li<sup>+</sup> separation stages include three technologies, (b) adsorption, also known as ion exchange, (c) nanofiltration, NF, and (d) electro dialysis. Li<sup>+</sup> concentration stages include two technologies, (e) reverse osmosis, RO, and (f) evaporation concentration.

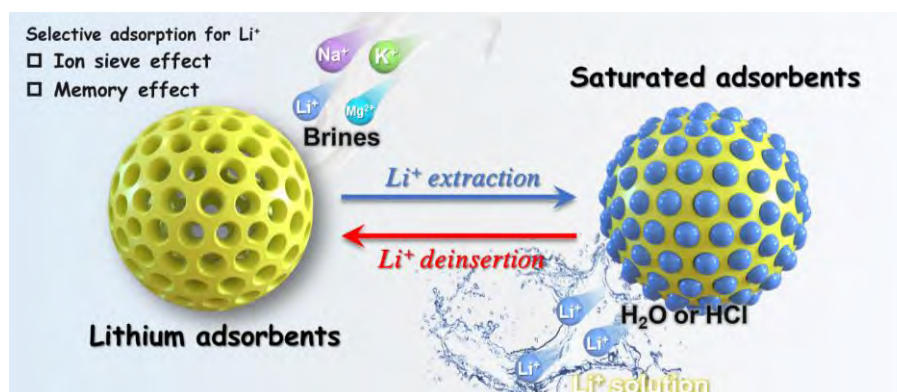
(Note: AEM, anion exchange membrane; CEM, cation exchange membrane; RO, reverse osmosis.)

Of the above advanced technologies, adsorption is not only a critical procedure in lithium extraction process, but also is considered to the most versatile technique for direct lithium extraction from salt lake brines, especially those with low grades and high Mg<sup>2+</sup>/Li<sup>+</sup> ratios, due to the advantages of the minimal pre-processing requirement of the brine, high lithium selectivity and recovery, additional concentration function, cost-effective and environment-friendly advantages [15-17]. Notably, the lithium recovery efficiency significantly depends on the lithium adsorbents. The selection of lithium adsorbents commonly relies on the performance of adsorbents (including adsorption capacity, selectivity, stability, cycle regeneration, etc.), the structures of adsorbents (including macro and microstructure), brine characteristics (including pH,

lithium concentration, temperature,  $\text{Mg}^{2+}/\text{Li}^+$  ratio, etc.). Thus, this chapter will focus on various lithium adsorbents and the full adsorption process for the extraction and recovery of  $\text{Li}^+$  from brines.

## 2.2. Various lithium adsorbents and structure-property relationship

The mainly studied lithium adsorbents involve inorganic metal-based adsorbents and organic adsorbents. The common metal-based adsorbents are lithium-aluminum layered double hydroxides (LiAl-LDHs), lithium titanium oxide type lithium-ion sieves (LTO-LISs), and lithium manganese oxide type lithium-ion sieves (LMO-LISs), in which template  $\text{Li}^+$  are introduced and then eluted from the crystalline structure of aluminum hydroxides or Mn and Ti oxides to generate lithium ion-specific vacancies for selective lithium extraction due to ion sieve and memory effect (Figure 2.3) [18]. Organic adsorbents include ion-imprinted polymers (Li-IIPs) and ion-exchange resins. Among them, heterocyclic compounds, such as crown ethers, attract particular attention by virtue of their ability to bind selectively to  $\text{Li}^+$  [19].



**Figure 2.3** Schematic of selective lithium recovery by lithium adsorbents.

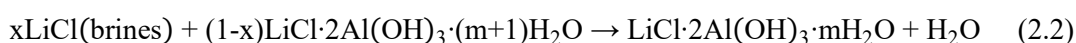
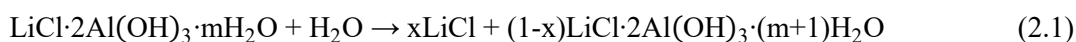
### 2.2.1. LiAl-LDHs

**The structure and property:** Lithium-aluminum layered double hydroxides were first derived from aluminum hydroxides, which were coated on ion exchange resins in 1978 to recover lithium from brine [20,21], forming crystalline layered double hydroxides upon contact with  $\text{Li}^+$ . The products were then eluted with dilute  $\text{LiCl}$  solution to recover the adsorbed  $\text{Li}^+$  [15]. Such produced adsorbents were called lithium-aluminum layered double hydroxides (LiAl-LDHs) [22].

The chemical structure model of LiAl-LDHs is presented in Figure 2.4a. Specifically, the structures of LiAl-LDHs, formed by the intercalation of lithium salts into the ordered octahedrons vacancies in the structure of  $\text{Al}(\text{OH})_3$  layers [23,24], are

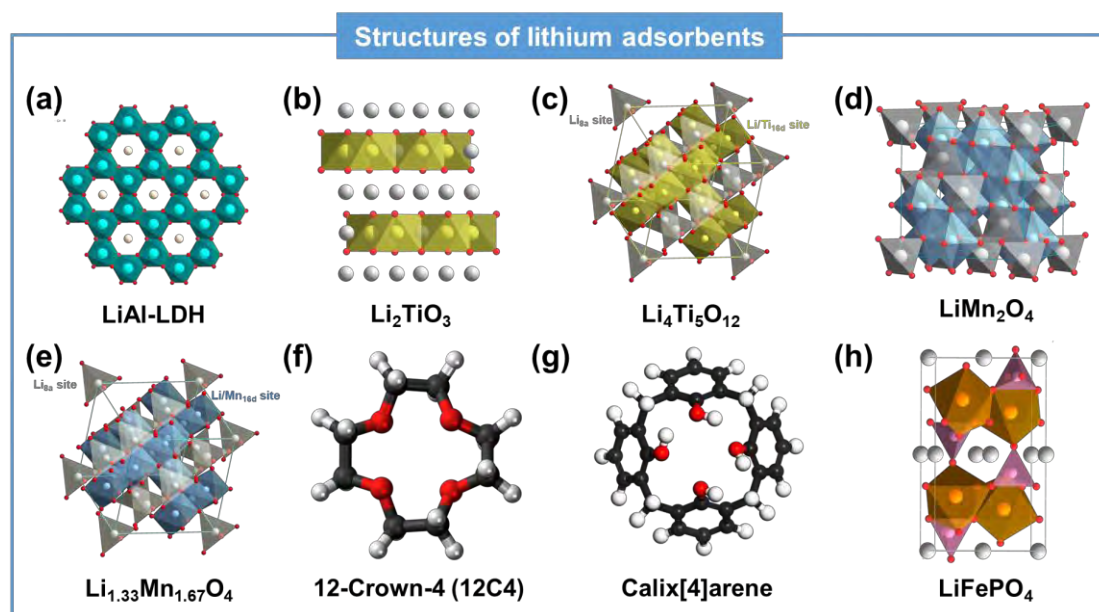
hexagonal layered structure, where  $\text{Al}^{3+}$  occupy two-thirds of the octahedrons vacancies created by close-packed oxygen layers and the  $\text{Li}^+$  ( $\sim 0.68 \text{ \AA}$ ) are inserted in the remaining unoccupied vacancies with radius of approximately  $0.70 \text{ \AA}$  to form  $[\text{LiAl}_2(\text{OH})_6]^+$  layers by hydrogen bonding, electrostatic interaction, and van der Waals forces [25-27]. During the insertion of  $\text{Li}^+$  into the  $\text{Al}(\text{OH})_3$  layers, the anions (e.g.,  $\text{Cl}^-$ ,  $\text{NO}_3^-$ ,  $\text{CO}_3^{2-}$ ) and water molecules are incorporation into the interlayer to keep charge balance [28], and then  $[\text{LiAl}_2(\text{OH})_6]^+$  layers are separated along the c-axis [23,29].

**Lithium intercalation/deintercalation mechanisms:** Among the metal-based adsorbents, the lithium intercalation and deintercalation mechanisms of LiAl-LDHs are the clearest, and were studied as early as 1998 [30], which have been checked, supplemented, and improved by recent researches. To extract  $\text{Li}^+$  from brines, the obtained LiAl-LDHs have to be desorbed and activated with deionized water or dilute  $\text{Li}^+$  solution to release octahedrons vacancies. Li et al. [31] reported that based on the structural memory effect, specific channels are formed during the desorption of LiAl-LDHs, involving specific layer spacing, sorption site sizes and interlayer path networks. Numerous interfacial channels with highly matched geometric configuration of  $\text{Li}^+$  are created between the layers. Therefore, the  $\text{Li}^+$  is quite easily inserted into the space between LDH layers. At the same time, the radius of  $\text{Li}^+$  ( $\sim 0.68 \text{ \AA}$ ) is slightly smaller than that of octahedrons vacancies ( $0.70 \text{ \AA}$ ) [25], hence  $\text{Li}^+$  tends to migrate from the interlayer space to the vacancies to be adsorbed [30]. Furthermore, for the charge balance, the intercalation of  $\text{Li}^+$  is accompanied by the insertion of anions [32]. Intercalation of  $\text{Li}^+$  results in weakened hydrogen bonding due to electrostatic repulsion between  $\text{Li}^+$  and protons, which provides the feasibility of insertion of anions between the layers [30]. In summary, taking  $\text{Cl}^-$  as an anion as an example, the intercalation (Equation 2.1) and deintercalation (Equation 2.2) mechanisms of  $\text{Li}^+$  can be expressed by the following formulas [24,33].



**Limitations and challenges:** As mentioned earlier, LiAl-LDHs have been applied as the lithium extraction adsorbents on industrial- and commercial-scale applications. However, LiAl-LDH have inherently limited  $\text{Li}^+$  theoretical maximum adsorption capacity ( $\sim 30 \text{ mg g}^{-1}$ ) [34], which limits the further development of LiAl-LDH. Moreover, the practical adsorption capacity of LiAl-LDH ( $4 \sim 8 \text{ mg g}^{-1}$ ) was always far below the theoretical capacity [35]. Additionally, LiAl-LDHs readily suffer from the

‘sulfate ion ( $\text{SO}_4^{2-}$ ) poisoning’ effect in  $\text{SO}_4^{2-}$ -type brines, causing the gradual decrease in adsorption capacity. Therefore, improvement in the  $\text{Li}^+$  adsorption capacity and anti-sulfate poisoning property of LiAl-LDHs has become major challenges to foster further progress of the Li extraction industry.



**Figure 2.4** Schematic structures of various lithium adsorbents. (a) LiAl-LDH, (b)  $\text{Li}_2\text{TiO}_3$ , (c)  $\text{Li}_4\text{Ti}_5\text{O}_{12}$ , (d)  $\text{LiMn}_2\text{O}_4$ , (e)  $\text{Li}_{1.33}\text{Mn}_{1.67}\text{O}_4$ , (f) 12-Crown-4, (g) Calix[4]arene, (h)  $\text{LiFePO}_4$ .

(Note: The gray, green, yellow, blue, orange, violet, black, red, and white spheres represent the Li, Al, Ti, Mn, Fe, P, C, O, and H atoms, respectively.)

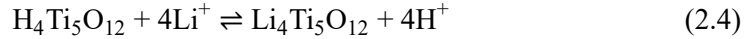
### 2.2.2. LTO-LISs

**The structure and property:** Lithium titanates were earlier used in the lithium battery industry due to excellent cyclability. The first exploration of lithium extraction using lithium titanates occurred in Japan in 1989, when Onodera et al. [36] successfully prepared a new inorganic titanium compound, now known as lithium titanium oxide type lithium-ion sieves (LTO-LISs), with high selectivity for  $\text{Li}^+$  via calcining a mixture of  $\text{Li}_2\text{CO}_3$  and  $\text{TiO}_2$  and treating the pyrolysis product with acid. Since then, LTO has been extensively studied.

Currently, LTO-LISs are mainly divided into two types: the layered titanate  $\text{H}_2\text{TiO}_3$  and spinel phase  $\text{H}_4\text{Ti}_5\text{O}_{12}$  [35]. Layered  $\text{H}_2\text{TiO}_3$  are derived from layered  $\text{Li}_2\text{TiO}_3$  precursors. To better describe the crystal structure,  $\text{Li}_2\text{TiO}_3$  precursors can also be expressed as  $\text{Li}[\text{Li}_{1/3}\text{Ti}_{2/3}]\text{O}_2$ , consisting of cubic close packed O, as well as Li and Ti placed in octahedral voids, where Ti and O atoms form a  $[\text{TiO}_6]$  octahedral structure,

and Li are located in the adjacent two  $[\text{TiO}_6]$  octahedra, forming alternating  $(\text{LiTi}_2)$  and  $(\text{Li})$  layers [37]. The  $(\text{Li})$  layers are filled only by Li atoms, while 1/3 of Li and 2/3 of Ti occupy another  $(\text{LiTi}_2)$  layers [38]. Therefore, Li in the  $(\text{Li})$  layers account for 75% of the total lithium in the  $\text{Li}_2\text{TiO}_3$  structure, while the remaining 25% of Li are located in the  $(\text{LiTi}_2)$  layer [39], as shown in Figure 2.4b. Further, layered  $\text{H}_2\text{TiO}_3$  are obtained by replacing  $\text{Li}^+$  in  $\text{Li}_2\text{TiO}_3$  with  $\text{H}^+$  using acid. Spinel phase  $\text{Li}_4\text{Ti}_5\text{O}_{12}$ , another LTO-LISs, are formed by the interspaced arrangement of  $[\text{LiO}_4]$  tetrahedral structural units and  $[\text{TiO}_6]$  octahedral structural units with  $Fd\bar{3}m$  space group as well as cubic symmetry, and a lattice constant of 0.836 nm [40]. As displayed in Figure 2.4c, in the crystal structure of  $\text{Li}_4\text{Ti}_5\text{O}_{12}$ ,  $\text{Li}^+$  occupy the tetrahedral 8a sites and 1/6 of the octahedral 16d sites, while the remaining octahedral 16d sites are occupied by  $\text{Ti}^{4+}$  with a  $\text{Li}^+/\text{Ti}^{4+}$  ratio of 1:5 [41]. Besides, the oxygen ions are located at position 32e. Thus, spinel phase  $\text{H}_4\text{Ti}_5\text{O}_{12}$  can be represented as  $\text{Li}_{(8a)}[\text{Li}_{1/3}\text{Ti}_{5/3}]_{(16d)}\text{O}_{4(32e)}$  [42].

**Lithium intercalation/deintercalation mechanisms:** In general, the major  $\text{Li}^+$  intercalation and deintercalation mechanisms of LTO-LIS are deemed to be ion exchange mechanism between  $\text{Li}^+$  and  $\text{H}^+$ , and this exchange happens during the preparation, adsorption, and desorption processes of LTO-LISs, which can be expressed as following:



**Limitations and challenges:** Although the theoretical  $\text{Li}^+$  adsorption capacity is high (127.3 mg  $\text{g}^{-1}$  for  $\text{H}_2\text{TiO}_3$  and 60.8 mg  $\text{g}^{-1}$  for  $\text{H}_4\text{Ti}_5\text{O}_{12}$ ), both the  $\text{Li}^+$  adsorption and desorption rates are relatively slow (requiring one day to attain equilibrium at room temperature) [39]. In addition, due to the mechanism of ion-exchange, the adsorption process of LTO-LISs always requires a high-alkaline solution environment, which is difficult to realize in most brines. Other limitation of LTO-LISs applications is the relatively high cost of preparation. Overall, LTO-LIS is also gradually showing industrial promise, especially for alkaline brines. Before that, however, the disadvantages of slow and costly extraction have to be addressed.

### 2.2.3. LMO-LISs

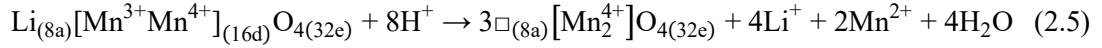
**The structure and property:** One of the first lithium manganese oxide type lithium-ion sieves (LMO-LISs) was  $\lambda$ - $\text{MnO}_2$ . In 1981, Hunter et al. [43] found that the lithium of  $\text{LiMn}_2\text{O}_4$  could be almost completely desorb and converse to  $\text{MnO}_2$  after

acid treatment, while the resultant material reserved the structural framework of the  $\text{LiMn}_2\text{O}_4$ , which was called  $\lambda\text{-MnO}_2$ . Since this discovery, numerous LMO-LISs have been well developed.

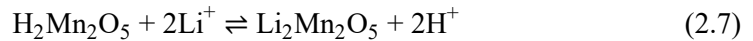
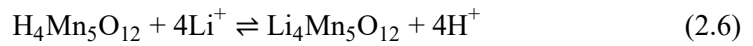
The typical precursors of LMO-LISs present spinel structures. Among them, the most common LMO-LISs precursors include  $\text{LiMn}_2\text{O}_4$ ,  $\text{Li}_{1.33}\text{Mn}_{1.67}\text{O}_4$  (or  $\text{Li}_4\text{Mn}_5\text{O}_{12}$ ), and  $\text{Li}_{1.6}\text{Mn}_{1.6}\text{O}_4$  (or  $\text{Li}_2\text{Mn}_2\text{O}_5$ ), which produce the  $\lambda\text{-MnO}_2$ ,  $\text{MnO}_2 \cdot 0.31\text{H}_2\text{O}$ , and  $\text{MnO}_2 \cdot 0.5\text{H}_2\text{O}$  with  $\text{Li}^+$  selective adsorption capacity by acid treatment [44,45]. LMO-LISs can be represent by one general formula  $\text{Li}_{1+x}\text{Mn}_{2-x}\text{O}_4$  ( $0 \leq x \leq 0.33$ ) [46]. At  $x$  is 0, the  $\text{LiMn}_2\text{O}_4$  is obtained.  $\text{LiMn}_2\text{O}_4$  is the most typical class of spinel (formula  $\text{AB}_2\text{O}_4$ ) with a cubic crystal structure belonging to the  $Fd\bar{3}m$  space group, and the lattice constant of 0.825 nm [47]. The structure of  $\text{LiMn}_2\text{O}_4$  was shown in Figure 2.4d. The oxygen atoms are densely packed in a face-centered cubic configuration with adjacent oxygen octahedra common-edge connection, the  $\text{Li}^+$  occupy the tetrahedral 8a sites, and the  $\text{Mn}^{3+}$  and  $\text{Mn}^{4+}$  are randomly located at the octahedral 16d sites in a molar ratio of 1:1, and the oxygen anions occupy the 32e sites of the face-centered cubes [48]. Thus, the  $\text{LiMn}_2\text{O}_4$  spinel can be represented by the formula of  $\text{Li}_{(8a)}[\text{Mn}^{3+}\text{Mn}^{4+}]_{(16d)}\text{O}_{4(32e)}$  with a mean oxidation state of 3.5+ for Mn [49]. When  $x$  is 0.33, the “0.33” of Li implies that some  $\text{Li}^+$  occupy the 16d sites and replace part of the Mn ions without changing the whole crystal framework, and the oxidation state of Mn is 4+ [50,51]. It can be seen from Figure 2.4e that  $\text{Li}_{1.33}\text{Mn}_{1.67}\text{O}_4$  (or  $\text{Li}_4\text{Mn}_5\text{O}_{12}$ ) has similar chemical structure as  $\text{Li}_4\text{Ti}_5\text{O}_{12}$ . For  $\text{Li}_{1.6}\text{Mn}_{1.6}\text{O}_4$ , a new type of spinel-structured LMO-LISs, two models  $\text{Li}_{(8a)1}\text{Li}_{(16c)0.2}\text{Li}_{(16d)0.4}\text{Mn}_{(16d)1.6}\text{O}_{(32e)4}$  and  $\text{Li}_{(8a)1}\text{Li}_{(16d)0.5}\text{Mn}_{(16d)1.5}\text{O}_{(32e)3.75}$  are favored, where  $\text{Li}^+$  mainly occupy the 8a and 16d sites, and  $\text{Mn}^{4+}$  occupy the 16d sites of a cubic closed-packed oxygen framework [52,53]. According to the formulas of precursors, the theoretical maximum lithium capacities of  $\lambda\text{-MnO}_2$ ,  $\text{MnO}_2 \cdot 0.31\text{H}_2\text{O}$ , and  $\text{MnO}_2 \cdot 0.5\text{H}_2\text{O}$  are 39.9, 59.5, and 72.8  $\text{mg g}^{-1}$ , respectively [54].

**Lithium intercalation/deintercalation mechanisms:** Compared to the LiAl-LDH and LTO-LISs, the  $\text{Li}^+$  intercalation/deintercalation mechanisms of LMO-LISs are more complex and controversial. In recent years, redox and ion exchange mechanisms have been commonly accepted by researchers. For  $\text{LiMn}_2\text{O}_4$ , the intercalation and deintercalation of  $\text{Li}^+$  were first proposed in research by Hunter as a pair of redox reactions [43], which can be expressed as following Equation 2.5 (where  $\square$  represents vacancies for  $\text{Li}^+$ ). Such conclusion was confirmed and elaborated in the work of Gao et al. [51]. They suggested that Li occupying only the 8a site on  $\text{LiMn}_2\text{O}_4$ , i.e.,  $[\text{Li}_{(8a)}\text{O}_4]$

groups, are decomposed during acid treatment. Meanwhile, due to  $[\text{Mn}^{3+}\text{O}_6]$  octahedrons are not as steady as  $\text{Mn}^{3+}$ ,  $\text{Mn}^{3+}$  release electrons to become stable  $\text{Mn}^{4+}$  accompanying by the  $[\text{Mn}^{3+}\text{O}_6]$  accept electrons and then decompose to  $\text{Mn}^{2+}$ . Finally, the generated  $\text{O}^{2-}$  react with  $\text{H}^+$  to form  $\text{H}_2\text{O}$ . However, the individual redox mechanism hardly explains the phenomenon of the positive effect of the adsorption capacity with solution pH in the adsorption process. Therefore, Ooi et al. [55] and Feng et al. [45] put forward a composite mechanism of redox and ion exchange that  $\text{Mn}^{3+}$  deliver redox sites and  $\text{Mn}^{4+}$  supplied ion-exchange sites. Specifically,  $\text{LiMn}_2\text{O}_4$  was firstly treated by  $\text{HCl}$ . Then, the  $[\text{Li}_{(8a)}\text{O}_4]$  groups decomposed, and  $[\text{Mn}^{3+}\text{O}_6]$  group released electrons into stable  $[\text{Mn}^{4+}\text{O}_6]$ , and another  $[\text{Mn}^{3+}\text{O}_6]$  accepted electrons and broke down. Finally,  $\text{Mn}^{2+}$ ,  $\text{Li}^+$  and  $\text{H}_2\text{O}$  were produced and went into solution, and only  $[\text{Mn}^{4+}\text{O}_6]$  groups constructed the crystal skeleton of  $\lambda\text{-MnO}_2$ .



In the cases of  $\text{Li}_{1.33}\text{Mn}_{1.67}\text{O}_4$  and  $\text{Li}_{1.6}\text{Mn}_{1.6}\text{O}_4$ , the ion-exchange is considered as the  $\text{Li}^+$  intercalation and deintercalation mechanism based on the stable oxidation state of Mn [56]. For instance, Wang et al. [57] used complexometric titration with EDTA to measure the amount of Mn, and found that the valence of Mn in  $\text{Li}_{1.6}\text{Mn}_{1.6}\text{O}_4$  was close to 4+. Furthermore, the change in the Mn valence during adsorption and desorption of  $\text{Li}^+$  was feeble, which meant that the redox reaction could be neglected. Therefore, the  $\text{Li}^+$  intercalation/deintercalation reaction of  $\text{Li}_{1.33}\text{Mn}_{1.67}\text{O}_4$  (Equation 2.6) and  $\text{Li}_{1.6}\text{Mn}_{1.6}\text{O}_4$  (Equation 2.7) may be expressed by the following equations:



**Limitations and challenges:** The Mn loss induced by Jahn-Teller effect ( $\text{Mn}^{3+} \rightarrow \text{Mn}^{3+} + \text{Mn}^{2+}$ ) has been deemed to be the most severe limitation for the practical application of LMO-LISs during the desorption with acid treatment ( $0.1\text{-}0.5 \text{ mol L}^{-1}$ ) [54]. For  $\text{LiMn}_2\text{O}_4$ , the desorption process is accompanied by the disproportionation reaction of  $\text{Mn}^{3+}$ , resulting in the continues manganese dissolution. Although disproportionation theoretically does not occur in  $\text{Li}_{1.33}\text{Mn}_{1.67}\text{O}_4$  and  $\text{Li}_{1.6}\text{Mn}_{1.6}\text{O}_4$  owing to Mn valence close to 4+, the strong acid solution can corrode the LMO during acid desorption [58]. As a recent example, Bao et al. [59] prepared  $\text{Li}_{1.6}\text{Mn}_{1.6}\text{O}_4$  for recovering  $\text{Li}^+$  from salt lake brine. However, the adsorption amount decreased by 44.2% and the Mn loss was more than 15% after 10 adsorption-desorption cycles.

#### 2.2.4. Ion-Imprinted polymers

**The structure and property:** In 1967, Pedersen successfully synthesized a series of cyclic polyether, and found that most of them were capable of complexing with alkali and alkaline earth metal cations by ion-dipole interaction [60]. Inspired in this work, ion-imprinted technique based on polymers have been rapidly developed.

Recently, the ion-imprinted polymers for lithium extraction (Li-IIPs) mainly include crown ether and calixarene [61,62], which are macrocyclic organic ligands with unique cavity structures matching  $\text{Li}^+$  diameter (1.36 Å) [63], especially 12-crown-4-ether (12C4) with the ring diameter of 1.20-1.50 Å and calix[4]arene with the ring diameter of 1.20-1.60 Å [64,65]. The structures were shown in Figure 2.4f-g. Herein, 12C4 is liquid at ambient temperature, making it difficult to be recovered after the adsorption process. Therefore, crown ether needs to be immobilized or grafted onto solid materials. For instance, 12C4 incorporated graphene-in-polyethersulfone (PES) nanofiber membrane owned superior  $\text{Li}^+$  uptake of 86.3 mg g<sup>-1</sup>, and adsorption capacity could still maintain more than 93% of initial value after 10 regeneration cycles [66]. Calix[4]arene and their derivatives have been attracting attention as another types of host compounds with  $\text{Li}^+$  discrimination properties. Calix[4]arene exhibit a high adsorption potential, while the relatively slow kinetics for  $\text{Li}^+$ . A high-efficient recovery of  $\text{Li}^+$  from seawater had been realized within 24 h by using ester-functionalized  $\text{Li}^+$  imprinted composite membrane adsorbent containing calix[4]arene with poly-dopamine PDA modified [67].

**Lithium intercalation/deintercalation mechanisms:** The intercalation mechanisms of  $\text{Li}^+$  into Li-IIPs can be attributed to two aspects: i) the “macrocyclic effect” from the size and shape of the generated cavities; and i) the “chelating effect” between the four oxygen atoms of ligand and  $\text{Li}^+$  [68]. Moreover, in acidic conditions, the oxygen atoms of ligand trend to protonate, inducing the electrostatic repulsion towards  $\text{Li}^+$ , weakening the complexation of ligand with  $\text{Li}^+$  [61]. Hence, the deintercalation of Li-IIPs can be conducted by using acid solution. Taking 12C4 as an example, the intercalation and deintercalation processes of  $\text{Li}^+$  can be expressed as following:



**Limitations and challenges:** Although the crown ethers and calixarenes have been recognized as the promising adsorption units for alkali and alkaline earth metal cations, the industrial application still is limited by several practical problems, including high

cost, toxicity, and suboptimal selectivity. Particularly, compared with the inorganic metal-based lithium adsorbents, the preparation procedures of Li-IIPs are complicated and cumbersome, and the raw materials are relatively expensive, which cause the high cost. Moreover, the selectivity of Li-IIPs for  $\text{Li}^+$  is remarkable low than inorganic metal-based lithium adsorbent, and typical the separation factor can only reach approximately 10. Apparently, the selectivity of Li-IIPs is rarely sufficient for industrial requirements in brines with high  $\text{Mg}^{2+}/\text{Li}^+$  ratio.

### 2.2.5. Other lithium adsorbents

As one of the most sophisticated adsorbents, the researches of ion-exchange resins for lithium extraction are gradually reported as well [69,70]. There are numerous types of Li-exchange resins. According the ionic form of resin, it can be divided into  $\text{Na}^+$  type and  $\text{H}^+$  type, while depending on the acidity strength, it can also be classified into strongly acidic resin and weakly acidic resin [71,72]. Normally, the capacity and selectivity of ion-exchange resins mainly are determined by the nature of the acidic functional group, the form of the cation, and the density of the structure [72,73]. Lemaire et al. [74] used Amberlite IR 120 resin to adsorb  $\text{Li}^+$  from  $\text{LiCl}$  solution and found that the adsorption capacity of sodium form was higher than that of hydrogen form. Güneysu reported that the adsorption of the carboxylated weakly acidic  $\text{H}^+$  type resin (CNP 80) outperformed sulfonated strongly acidic  $\text{Na}^+$  type resin (Armfield) [72]. However, the ion-exchange resins show poor selectivity for  $\text{Li}^+$ , which is ascribed to the low affinity towards  $\text{Li}^+$  compared to other cations [74]. The adsorption capacity of commercial strong acid-type cation exchange UBK 10 resin ( $\text{Na}$  type) in environmental lithium-bearing solution followed the order:  $\text{K}^+ > \text{Li}^+ > \text{Ca}^{2+} > \text{Mg}^{2+}$  [75]. Therefore, the ion-exchange resins are effective in selective extracting  $\text{Li}^+$  only after coupling inorganic metal-based adsorbents. In fact, in the first study on the use of ion-exchange resins to selectively extract and recover lithium from brines in the 1970s, the Li extraction was realized by compounding the resin with  $\text{Al}(\text{OH})_3$  [21].

In addition to the aforementioned promising adsorbents, several other metal oxides also show certain Li extraction ability, including lithium-iron-phosphates ( $\text{LiFePO}_4$ ) [76], Zr-phosphate ( $\text{Zr}(\text{LiPO}_4)_2$ ) [77], Sb-oxides ( $\text{LiSbO}_3$ ) [78], Ta-oxides ( $\text{LiTaO}_3$ ) [79],  $\text{H}_8\text{Nb}_{22}\text{O}_{59} \cdot 8\text{H}_2\text{O}$  [80], and so forth. The theoretical maximum  $\text{Li}^+$  adsorption capacity of those metal oxide adsorbents ranges from 22 to 53  $\text{mg g}^{-1}$ . Nevertheless, their inferior adsorption selectivity for  $\text{Li}^+$  and complicated adsorption-desorption

procedures severely hinder their application in lithium extraction from brines. For example,  $\text{LiFePO}_4$  (Figure 2.4h) with the theoretically possible maximum  $\text{Li}^+$  adsorption capacity of  $44 \text{ mg g}^{-1}$  is capable of recovering monovalent cations, in which the presence of  $\text{Na}^+$  and  $\text{K}^+$  in brines will compete the adsorption sites [81]. Meanwhile, for the reason that the adsorption process is primarily dominated by redox reactions ( $\text{Fe}^{3+}\text{PO}_4 + \text{e}^- + \text{Li}^+ \rightarrow \text{LiFe}^{2+}\text{PO}_4$ ), oxidizing agents are required [76], which made it has attracted attention in the field of electrochemical lithium extraction [82,83]. Therefore, these materials used as adsorbents have rarely been reported in recent years.

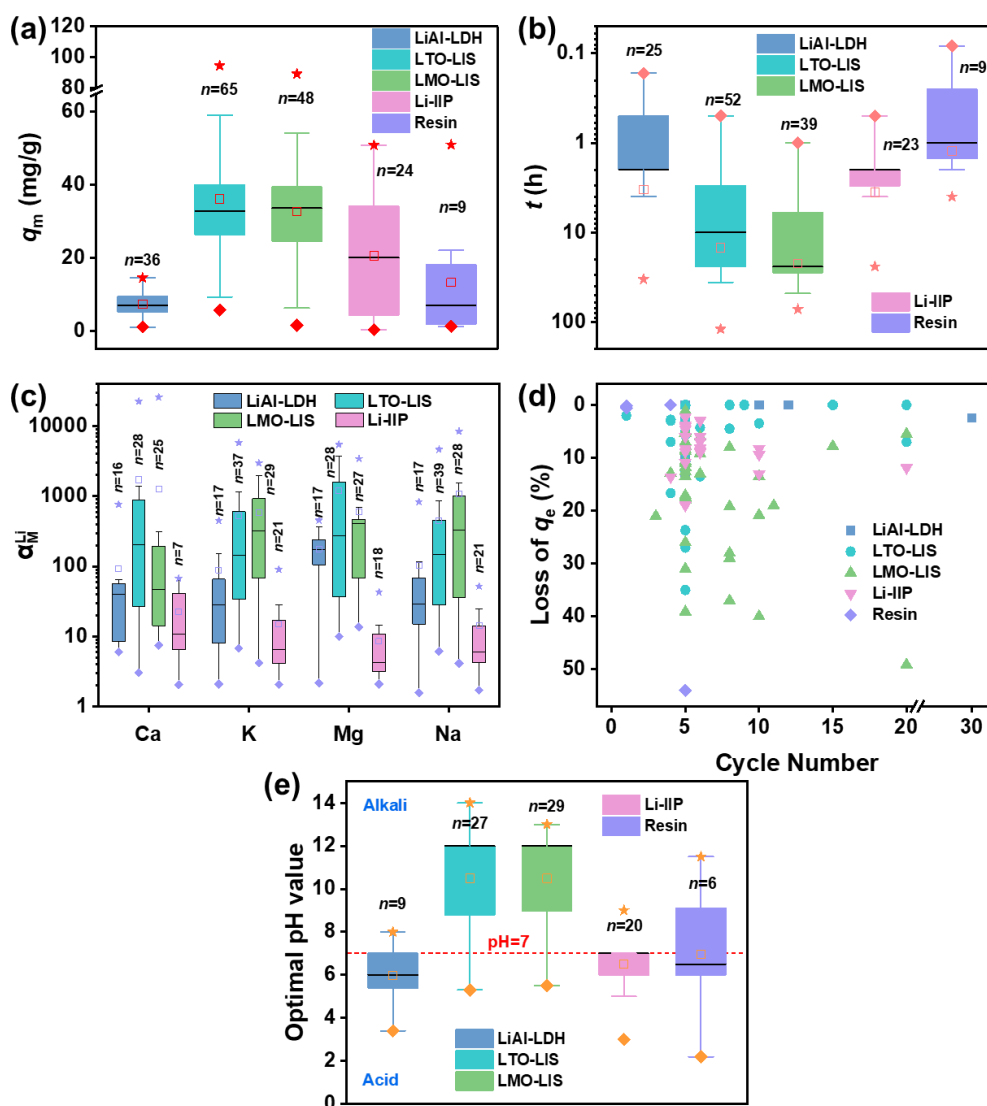
Recently, inspired by the specific coordination of fluorine-containing electrolytes towards  $\text{Li}^+$  in lithium-ion batteries, a novel F-rich supramolecular nano-container crosslinked hydrogel with extraordinary  $\text{Li}^+$  adsorption capacity ( $122.3 \text{ mg g}^{-1}$ ) and  $\alpha_{\text{Li/Na}}$  (153.72) was prepared, which provides a new insight into the design of lithium adsorbents [84]. In the future, more delicate research as well as practical application evaluation should be carried out.

### 2.3. Comparison of various lithium adsorbents

After elucidating the structures and performances of various Li extraction adsorbents, it is worth to perform a comprehensive comparison between different adsorbents. For visual comparison, several figures of merit were here proposed, as shown in Figure 2.5.

In the case of maximum adsorption capacity ( $q_m$ ), LTO-LISs and LMO-LISs possess significantly higher  $q_m$ , wherein the average reach  $32.79$  and  $33.65 \text{ mg g}^{-1}$ , and medium values are  $36.13$  and  $32.72 \text{ mg g}^{-1}$ , respectively (Figure 2.5a). In contrast, LiAl-LDHs exhibited lowest  $q_m$ . In general, the order of the actual adsorption capacity followed that of the theoretical maximum adsorption capacity. LiAl-LDHs and resins typically own fast  $\text{Li}^+$  adsorption kinetics (Figure 2.5b). In comparison, the Li extraction processes of LTO-LISs and LMO-LISs are remarkable slow, usually lasting 12-24 h. Based on the results of  $q_m$  and adsorption equilibrium time, Li-IIPs seem to have relatively balanced adsorption ability. However, the practical applications of Li-IIPs are hindered by their poor selectivity (Figure 2.5c). Considering the high  $\text{Mg}^{2+}/\text{Li}^+$  ratio of brines, the  $\text{Li}^+$  selectivity is a vital indicator for assessing the practical potential of lithium adsorbents. Three common inorganic metal oxides adsorbents (namely LiAl-LDHs, LTO-LISs and LMO-LISs) show considerable lithium-magnesium separation capability with extraordinary  $\alpha_{\text{Li/Mg}}$ , normally greater than 100. Specifically, LTO-LISs

present better Li extraction than others in the brines containing  $\text{Ca}^{2+}$ , while LMO-LISs are slightly superior to LTO-LISs for Li extraction in alkali metal brines. The resins possess almost no selectivity for lithium extraction, so comparative analyses of their performance are unavailable in this study. The excellent stability and regeneration ability always are expected, and the promising adsorbents need to be in the upper right area of Figure 2.5d. A quick glance at the area will suffice to see that LiAl-LDHs show best reusability, followed by LTO-LISs, while LMO-LISs are less reusable due to the Mn loss induced by Jahn-Teller effect [54]. Notably, LiAl-LDHs require a simple desorption procedure in water without dissolution loss [85], whereas others, including LTO-LISs, LMO-LISs, Li-IIPs and resins, rely on strong acids (such as HCl) to complete the desorption process, which may not only corrode equipment, but also contaminate the brine.



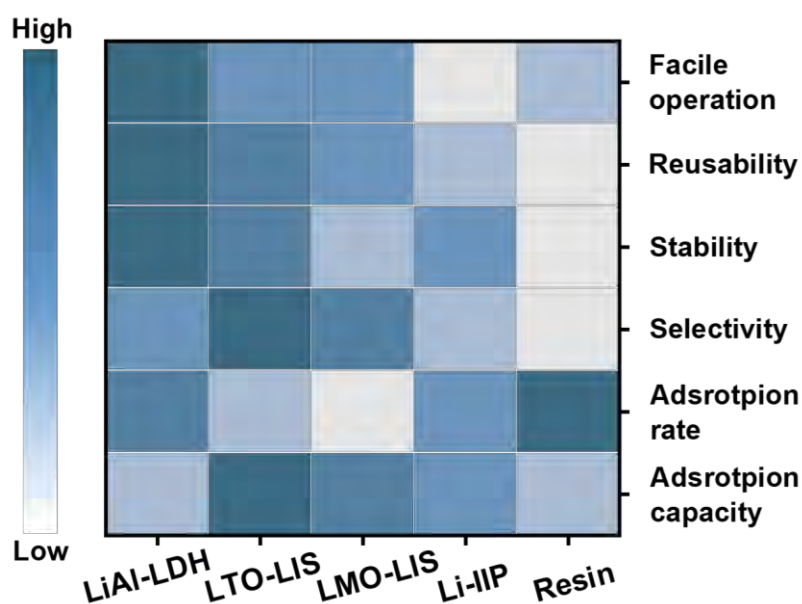
**Figure 2.5** Comparison of various lithium adsorbents. (a) Adsorption capacity, (b)

adsorption equilibrium time, (c)  $\text{Li}^+$  selectivity for, (d) regeneration stability, and (e) optimal pH value of LiAl-LDHs, LTO-LIS, TMO-LIS, Li-IIPs, and Resins.

(Note: The “★” and “◆” stand for the maximum and minimum values, respectively. The upper and lower edges of the boxes are 75% and 25% of the data, and the cross line in the box refers the median value and the “□” refers the mean value. Data were collected from cited literatures, and n in the legend is the number of obtained data.)

Moreover, pH regulation of brines is impractical before actual applications, thus comparison of effective pH ranges between adsorbents is of major significance. As presented in Figure 2.5e, the LiAl-LDHs, Li-IIPs, and resins exhibit the best Li extraction performance in common neutral brines. Whereas, LTO-LISs and LMO-LISs have the highest  $\text{Li}^+$  adsorption capacity in basic conditions owing to the  $\text{Li}^+/\text{H}^+$  exchange adsorption mechanism. Unfortunately, most brines are normally in a relatively steady neutral environment, suggesting that the additional alkali is necessary to be added to the brines prior to extraction using both LISs, which dramatically increases the cost of lithium extraction.

Based on the above results, performance comparison heatmap was plotted in Figure 2.6. Taking the all levels into account, LiAl-LDHs are currently the most mature lithium adsorbents for industrial applications. The major challenges for LiAl-LDHs remain to enhance the adsorption capacity and prevent  $\text{SO}_4^{2-}$  poisoning. Therefore, the chapter will subsequently focus on LiAl-LDHs for discussion and synthesis.



**Figure 2.6** Performance heatmap of LiAl-LDHs, LTO-LIS, TMO-LIS, Li-IIPs, and Resins.

## 2.4. Conclusions and perspectives

As technology advances, especially in lithium-ion batteries, the demand for lithium resources is soaring. Due to the endless lithium resources in the brine, lithium recovery from brines undoubtedly attracts more interest and desires more advanced selective Li extraction processes. Among various advanced techniques, adsorption is considered to be the most versatile technique for direct lithium recovery from brines owing to minimal pre-processing requirement, high lithium recovery and selectivity, cost-effective and environment-friendly advantages. Consequently, the researches on lithium adsorbents are significantly growing.

The lithium adsorbents involve inorganic metal-based adsorbents and organic adsorbents, the former comprising LiAl-LDHs, LTO-LISs, and LMO-LISs, while the latter including Li-IIPs and ion-exchange resins. Currently, the inorganic metal-based adsorbents present more promising and applicable in Li extraction, especially LiAl-LDHs. However, this does not mean that these adsorbents are capable of directly working for the  $\text{Li}^+$  recovery from brines. For LiAl-LDHs, though they have applied as the lithium extraction adsorbents on industrial- and commercial-scale applications, the relatively low adsorption capacity aspires to improve by structural modification. On the other hand, the long-term cycling stability is attacked by the ‘ $\text{SO}_4^{2-}$  poisoning’ effect.

With the development of industrial and commercial Li extraction, emerging challenges for Li extraction by adsorption methods have arisen: i) High grade brines with high  $\text{Li}^+$  concentration and low  $\text{Mg}^{2+}/\text{Li}^+$  ratio are rapidly decreasing, thus the LiAl-LDHs with effective Li extraction performance for low-quality brines should be the focus of future research; ii) To enhance the commercial competitiveness of enterprises, the  $\text{Li}^+$  adsorption kinetics of adsorbents should be improved, and LiAl-LDHs with high  $\text{Li}^+$  transfer rate and relevant adsorption tower need to be designed.

## 2.5. References

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## **Chapter 3. Doping engineering of lithium-aluminum layered double hydroxides for high-efficiency lithium extraction from salt lake brines**

### ***3.1. Introduction***

Lithium (Li), one of the most important strategic resources today, has many industrial applications, such as ceramics and glass, energy storage, nuclear fusion, pharmaceuticals and the well-known lithium-ion batteries (LIBs), which renders a skyrocket in the demand and market price of Li [1,2]. According to the statistics, most of the world's Li resources are found in salt lakes brines [3]. For China, even up to 80% of lithium resources are in salt lake brines [4]. Unfortunately, in addition to  $\text{Li}^+$ , a variety of competing cations in high concentrations are present in numerous brines, especially  $\text{Mg}^{2+}$  with similar properties to  $\text{Li}^+$  [5,6]. Therefore, it is imperative but challenging to develop efficient Li extraction technologies from the brines.

Hitherto, many extraction technologies for recovering  $\text{Li}^+$  from salt lakes brines have been researched, including solar evaporation, electrochemistry, precipitation, membrane separation, adsorption, etc. [7-9] Among them, adsorption method is considered a promising methodology for Li extraction due to easy operation, high selectivity to  $\text{Li}^+$ , and eco-friendliness, especially for applications in low-grade brines with ultrahigh  $\text{Mg}^{2+}:\text{Li}^+$  ratio [5,10]. Various types of adsorbents have been reported, in which inorganic metal-based lithium extraction adsorbents, namely manganese-based ion sieve (LMO), titanium-based ion sieve (LTO), and lithium-aluminum layered double hydroxides (LiAl-LDH), are the research hotspot in view of the innate merits [11]. For example, the LMO and LTO possess superior  $\text{Li}^+$  adsorption capacity and selectivity, while LiAl-LDH features stable adsorption performance and negligible elution damage with deionized water [12]. In practical application, LMO suffer from large dissolution losses during the desorption process, while the production cost of LTO are expensive [13]. Fortunately, LiAl-LDH are capable of overcoming the issues mentioned above and have become the only adsorbent material that can be used on commercial-scale applications in China [14,15]. However, LiAl-LDH have an innate limited  $\text{Li}^+$  theoretical adsorption capacity according to the formula of

[LiCl·2Al(OH)<sub>3</sub>·nH<sub>2</sub>O] [16,17]. Moreover, the actual adsorption capacity of LiAl-LDH (4 ~ 8 mg/g) is always much lower than theoretical capacity [15]. Therefore, improvement in the Li<sup>+</sup> adsorption performance of LiAl-LDH has become the keystone to promote the further development of the Li extraction industry.

To meet this preceding requirement, researchers carried out numerous works on the modification of LiAl-LDH [11,18,19]. Previous work on the interlayer regulation found that although expanding the layer spacing could enhance the Li<sup>+</sup> uptake of LiAl-LDH, it led to a decline in the Li<sup>+</sup> selectivity owing to the depressed interlayer confinement effect [19]. Wu and co-workers [20] revealed that the higher interlayer of water, the less the thermodynamic barriers, which facilitated Li<sup>+</sup> adsorption on LiAl-LDH, yet resulted in structural destabilization. Porous LiAl-LDH prepared by surfactants modification exhibited an increasing Li<sup>+</sup> adsorption capacity, but complex preparation process and the unstable material recycling capacity restrict their application [18]. The dopant modification with high electron density metals have also been utilized to retain structural and functional stability, whereas fail to enhance Li<sup>+</sup> adsorption capacity [21]. Apparently, a suitable strategy to improve the performance of LiAl-LDH for Li extraction is eager but unready. On the other hand, the mechanism of Li extraction by LiAl-LDH, i.e., the intercalation of Li<sup>+</sup> into the octahedral vacancies of Al(OH)<sub>3</sub> via weak hydrogen bonding and van der Waals forces ( $x\text{LiCl} + (1-x)\text{LiCl}\cdot 2\text{Al}(\text{OH})_3 + (n+1)\text{H}_2\text{O} \rightleftharpoons \text{LiCl}\cdot 2\text{Al}(\text{OH})_3\cdot n\text{H}_2\text{O}$ ), had been reported [14,22]. However, the whole process and steps of extraction are still unrevealed, whole hinders the further development of LiAl-LDH.

Indeed, doping engineering has been proven to be a simple yet effective strategy for improving physicochemical property of adsorbents, thereby facilitating adsorption [23]. By utilizing different dopants and levels of doping, adsorbents exhibit a highly flexible tunability in terms of surface electronegativity, stability, selectivity, and microstructures [24]. Herein, a low-valent metal doping-engineering strategy were presented to comprehensively improve the Li extraction performance of LiAl-LDH via simple one-pot co-precipitation method. Further, the three-steps process for Li extraction on LiAl-LDH was proposed. The results of experiments and theoretical calculations demonstrated that this doping-engineering strategy not only regulate the surface charge, specific surface area and hydrophilicity of LiAl-LDH, which increased the affinity for Li<sup>+</sup> and facilitated the transfer and insertion of lithium, but also introduced defects and accelerated the diffusion process of Li<sup>+</sup> in the internal bulk of

LiAl-LDH. Furthermore, the systematic investigations were performed to reveal the advance of doping-engineering strategy, where the samples after doping could effectively retain outstanding reusability and stability with significantly improved  $\text{Li}^+$  adsorption capacity and selectivity. This work delivered pivotal scientific significance and application value to develop efficient adsorption for the Li extraction from salt lakers brines.

### 3.2. Experimental section

#### 3.2.1. Material synthesis

**Materials:** All the analytical reagents used in experiments were obtained from Shanghai Aladdin Biochemical Technology Co., Ltd., including lithium chloride (LiCl), aluminum chloride hexahydrate ( $\text{AlCl}_3 \cdot 6\text{H}_2\text{O}$ ), zinc chloride ( $\text{ZnCl}_2$ ), magnesium chloride hexahydrate ( $\text{MgCl}_2 \cdot 6\text{H}_2\text{O}$ ), cupric chloride dihydrate ( $\text{CuCl}_2 \cdot 2\text{H}_2\text{O}$ ), nickel chloride hexahydrate ( $\text{NiCl}_2 \cdot 6\text{H}_2\text{O}$ ), cobalt chloride hexahydrate ( $\text{CoCl}_2 \cdot 6\text{H}_2\text{O}$ ), stannous chloride pentahydrate ( $\text{SnCl}_4 \cdot 5\text{H}_2\text{O}$ ), molybdenum chloride ( $\text{MoCl}_5$ ), lanthanum chloride heptahydrate ( $\text{LaCl}_3 \cdot 7\text{H}_2\text{O}$ ), calcium chloride ( $\text{CaCl}_2$ ), ferric chloride ( $\text{FeCl}_3$ ), antimony trichloride ( $\text{SbCl}_3$ ), and sodium hydroxide (NaOH).

The brine used in the experiments was the Lop Nor brine, and the compositions were provided in Table 3.1.

**Table 3.1** Composition of the Lop Nor brine.

Components	$\text{Li}^+$	$\text{Mg}^{2+}$	$\text{Na}^+$	$\text{K}^+$	$\text{Cl}^-$
Concentration (mg/L)	222	105276	1849	3827	2224000

**Synthesis of LiAl-LDHs with metal ions doping (LiMAI-LDHs):** LiMAI-LDHs were fabricated by a modified co-precipitation method, in which the reactions of metal ions doping and Li-insertion reaction were coupled. Typically, the aqueous solution with the Al/M/Li molar ratio of 19:1:10 (M represents the common divalent, trivalent, tetravalent, and pentavalent metal cations) was dropped into 8.0 mol/L NaOH solution, stirred at 75 °C together with detecting the pH of the mixture with a pH meter (Sartorius PB-10) until the its pH was 5 and then aged for 30 min. Finally, the LiAl-LDHs with metal ions doping (LiMAI-LDHs) were obtained after deionized water washing, filtration, and freeze-drying. In addition, to investigated the effect of metal ions doping amount, LiZnAl-LDHs with various Zn-doping amount were prepared via mixing  $\text{AlCl}_3$ ,  $\text{ZnCl}_2$  and LiCl with different molar ratio  $[\text{n}_{(\text{Al} + \text{M})}:\text{n}_{\text{Li}} = (100+0):50, (99+1):50,$

(95:5):50, (90:10):50, (80:20):50], and the produced materials were denoted as LiAl-LDH, LiZnAl-LDH-1%, LiZnAl-LDH-5%, LiZnAl-LDH-10%, and LiZnAl-LDH-20%, respectively, where 1-20% represent the molar content of  $Zn^{2+}$  in the raw material as a percentage of  $(Zn^{2+} + Al^{3+})$ .

### 3.2.2. Characterizations

The morphologies of samples were characterized using scanning electron microscopy (SEM, Zeiss Gemini 300, Germany) and transmission electron microscopy (TEM, JEM-JEOL-2100, Japan) equipped with energy dispersive spectroscopy (EDS) system. X-ray diffraction patterns were recorded using D/max RBX diffractometer (XRD, D8 ADVANCE X, Germany) with Cu K $\alpha$  radiation (40 kV, 100 mA). The N<sub>2</sub> adsorption-desorption measurements were measured by ASAP2460 aperture analyzer, and the specific area, porosity and pore size distributions were determined via Brunauer-Emmett-Teller method (BET). Raman spectroscopy was carried out using a Thermo scientific DXR3 Raman microscope with 532 nm laser excitation. Electron spin resonance (EPR) spectrum was obtained on a Bruker ER200-SRC spectrometer. Contact angle (CA) of sample was taken by micro-scopic contact angle meter (Kyowa Interface Science Co. Ltd., Japan). X-ray photoelectron spectroscopy (XPS) was taken with AXIS SUPRA spectrometer.

### 3.2.3. Lithium-ion extraction performance evaluation

All batch adsorption experiments were performed at room temperature in thermostatic water bath at 150 rpm with adsorbents (20 g/L) suspended in Lop Nor brine. The adsorption kinetics were conducted, and the pseudo-first-order, the pseudo-second-order and the intraparticle diffusion models were employed to fit the experimental data, respectively [25]. The adsorption isotherms were measured for 6 h. The experimental data were analyzed by the Langmuir isotherm and Freundlich isotherm models, respectively [26]. To evaluate the performance of adsorbents, supernatants were filtered at given intervals through 0.22  $\mu$ m filter membrane, and the concentration of Li<sup>+</sup> before and after adsorption were measured by filtering the atomic absorption spectrum (AAS). The adsorption capacity  $q_e$  (mg/g) was calculated by Equation 3.1:

$$q_e = (C_0 - C_e)V/m \quad (3.1)$$

where  $C_0$  (mg/L) and  $C_e$  (mg/L) are the initial and equilibrium concentrations of Li<sup>+</sup>,

respectively;  $V$  (L) represents the solution volume;  $m$  (g) is the mass of adsorbent. The desorption performance was investigated as well. Deionized water was used as eluent, and the liquid-solid ratio was 100 mL/g. The  $\text{Li}^+$  desorption capacity was determined by Equation 3.2:

$$q_{\text{dt}} = C_{\text{dt}} V / m \quad (3.2)$$

where  $q_{\text{dt}}$  (mg/g) and  $C_{\text{dt}}$  (mg/L) are the desorption capacity and concentration at time  $t$ , respectively.

The adsorption selectivity of samples to different metal cations in the brine was assessed by measuring the initial and equilibrium concentrations of each metal ion. The distribution coefficient  $K_{\text{d}}$  (mL/g) and separation coefficient  $\alpha_{\text{M}}^{\text{Li}}$  were determined according to Equation 3.3 and 3.4:

$$K_{\text{d}} = V(C_0 - C_e) / (mC_e) \quad (3.3)$$

$$\alpha_{\text{M}}^{\text{Li}} = K_{\text{d, Li}} / K_{\text{d, M}} \quad (3.4)$$

where M represents  $\text{K}^+$ ,  $\text{Na}^+$ , and  $\text{Mg}^{2+}$ .

Reusability and stability for Li extraction was also studied for practical applications. After a fast wash with ice water (adsorbent to water ratio of 1 g/10 mL) for removal of residual brine adhering to the separated adsorbent surface, the desorption process of saturated adsorbents was performed by shaking with 100 g/mL deionized water at 40 °C for 3 h, and then the regenerated adsorbents were used in the brine for next adsorption/desorption cycle. Moreover, the stability of adsorbents was revealed by monitoring the amounts of doped metal ion in desorption solutions.

### 3.2.4. Calculation details

All Density functional theory (DFT) calculations were performed with the Cambridge Sequential Total Energy Package (CASTEP) module or Dmol<sup>3</sup> module of the Materials Studio software. The exchange and correlation interactions were established by the Perdew-Burke-Ernzerhof (PBE) formulation with the generalized gradient approximation (GGA). The structure of LiAl-LDH with interlayer spacing of 9.7 Å was obtained from Materials Project (Materials ID: mp-643655). The cut-off energy was set to 430 eV and the k-point mesh with a size of  $1 \times 1 \times 1$  grid was used. For all structural optimization, atomic positions were fully relaxed (the convergence thresholds of energy  $< 2 \times 10^{-5}$  eV/atom, maximum displacement  $< 0.002$  Å, maximum force  $< 0.05$  eV/Å, respectively) [27]. Then, the adsorption energies ( $E_{\text{ad}}$ ) were

calculated by Equation 3.5:

$$E_{ad}=E_{\text{cluster/adsorbate}}-E_{\text{cluster}}-E_{\text{adsorbate}} \quad (3.5)$$

where  $E_{\text{cluster/adsorbate}}$  represents the total energy of Li adsorbed on the LiAl-LDH and LiZnAl-LDH;  $E_{\text{cluster}}$  is the energy of LiAl-LDH and LiZnAl-LDH;  $E_{\text{adsorbate}}$  stands for the energy of Li.

The density functional perturbation theory (DFPT) as implemented in CASTEP code were employed to calculate the entropies and zero-point energies. Further, the Gibbs free energies ( $G$ ) of Li-insertion reaction were obtained at 298.15 K and 1 bar using Equation 3.6 [28]:

$$G=E_{\text{DFT}}+E_{\text{ZPE}}-TS \quad (3.6)$$

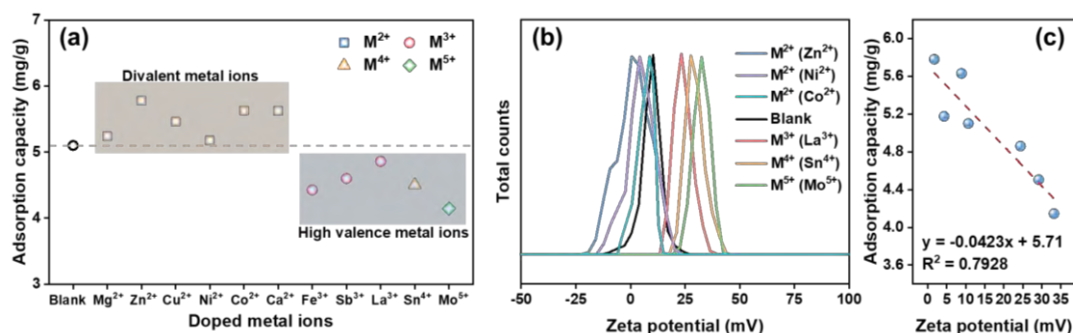
where  $E_{\text{DFT}}$  represents the DFT calculate DFT energy;  $E_{\text{ZPE}}$  and  $TS$  are the zero-point energy and the entropic contribution, respectively.

The energy barrier of  $\text{Li}^+$  diffusion within the samples were performed by searching their transition states. The transition state searching calculations were carried out by using linear and quadratic synchronous transit (LST/QST) method nudged elastic band (NEB) tools implemented in DMol<sup>3</sup> [29].

### 3.3. Results and discussion

#### 3.3.1. Optimization of doping strategy

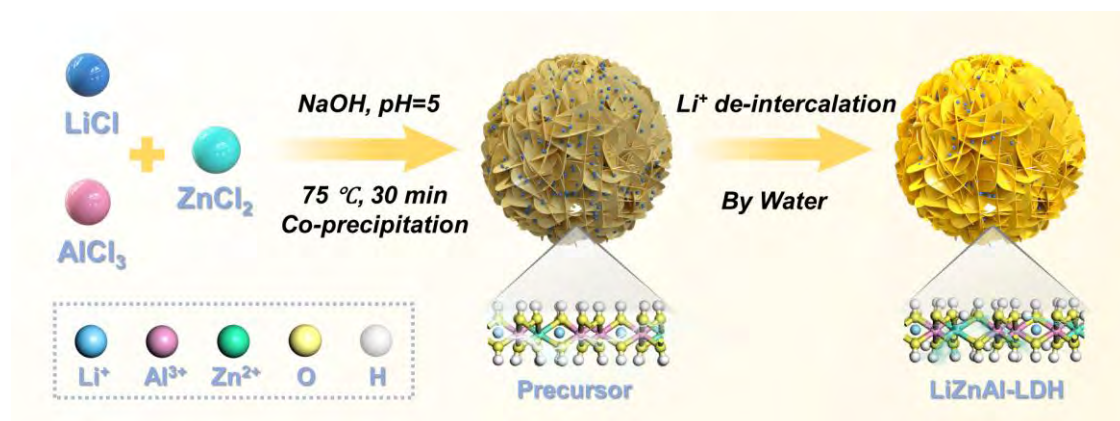
The effect of doping and optimal LiMAI-LDHs were first determined. As displayed in Figure 3.1a, various metal elements with different valence were doped into LiAl-LDH to prepare LiMAI-LDH, whose Li extraction kinetics were carried out as well. One could see that doping of divalent elements was able to improve the  $\text{Li}^+$  uptake, whereas the incorporation of higher valence elements had negative effect. The results might be related to the change in surface charge of LiMAI-LDHs. The positions of  $\text{Al}^{3+}$  are replaced by divalent metal ions can reduce the surface charge of aluminum hydroxide layered plate, facilitating the adsorption of  $\text{Li}^+$  [30]. Indeed, the surface charge exhibited a positive correlation with the adsorption capacity of LiMAI-LDHs to certain extent (Figure 3.1b). Value of  $R^2$ , however, is less than 0.8, suggesting the presence of other interaction mechanisms derived from doping engineering, which will be discussed below. Considering the best adsorption capacity of  $\text{Li}^+$ , the LiZnAl-LDHs was chosen the optimal doping element for emphatical investigation.



**Figure 3.1** (a) The adsorption capacity of Li<sup>+</sup> on LiAl-LDHs doped with various metal cations; (b) The surface zeta potential of LiAl-LDHs doped with various metal cations; (c) The relationship between surface zeta potential and adsorption capacity of Li<sup>+</sup>.

### 3.3.2. Fabrication and characterization of LiZnAl-LDH

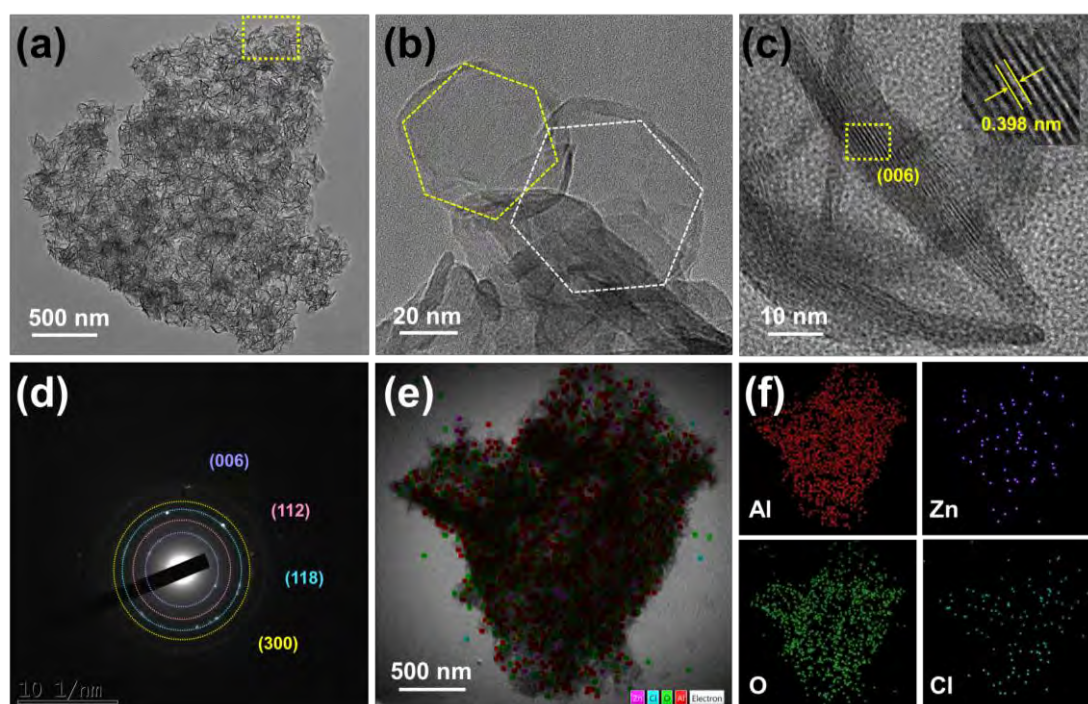
The in-situ Zn-doped LiAl-LDHs were synthesized via co-precipitation method (Figure 3.2). During the preparation of LiZnAl-LDH, the Zn-doping and Li-insertion reaction were coupled [31]. At the beginning of the reaction, ZnAl-LDHs were formed rather than Al(OH)<sub>3</sub> due to the more stable structure of the former [32,33]. Then, the intercalation reaction of Li<sup>+</sup> proceeded to form adsorbent precursors. Finally, the target LiZnAl-LDHs were prepared by washing and activating with deionized water.



**Figure 3.2** The schematic illustration of the fabrication strategy for LiZnAl-LDHs.

The microscopic morphologies LiZnAl-LDHs were observed. TEM images clearly uncovered the two-dimensional hexagonal nanosheet morphology of LiZnAl-LDH-5% with a size of 40-60 nm (Figure 3.3a-b). The high-resolution TEM (HRTEM) image of the LiZnAl-LDH-5% showed continuous lattice fringes and the determined lattice spacing was about 0.398 nm (Figure 3.3c), corresponding to the (006) crystal planes of LiAl-LDH. The four strong diffraction rings in the selected area electron

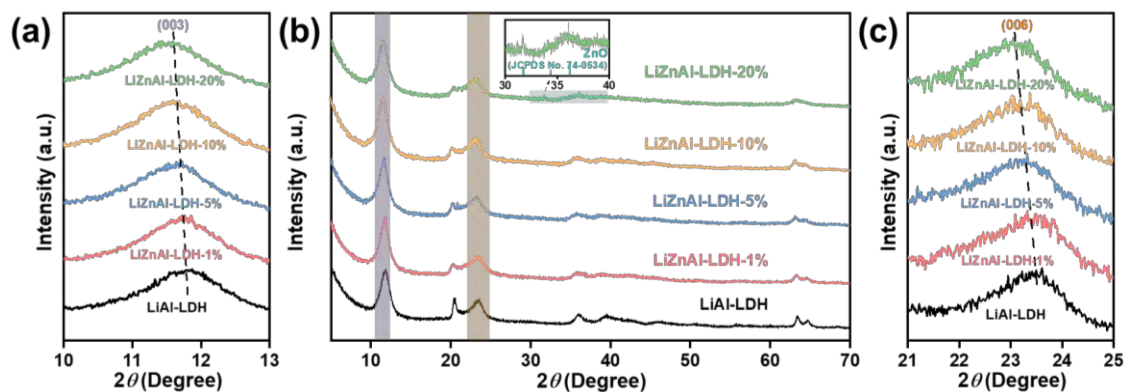
diffraction (SAED) pattern of LiZnAl-LDH-5% indexed to (006), (112), (118), and (300) crystal planes were observed (Figure 3.3d), confirming the LiAl-LDH crystal phase. Additionally, scanning transmission electron microscopy (STEM) coupled with energy-dispersive X-ray spectroscopy (EDS) elemental mapping of LiZnAl-LDH-5% demonstrated that Al, O, Cl, and Zn elements were homogeneously distributed throughout the whole sample (Figure 3.3e-f), where Zn element presented perfect dispersion with Al element, suggesting that Zn was doped into the octahedral voids of  $\text{Al}(\text{OH})_3$  [31,34].



**Figure 3.3** (a) TEM images, (b-c) HRTEM image, (d) SAED pattern and (e-f) STEM-EDS of LiZnAl-LDH-5%.

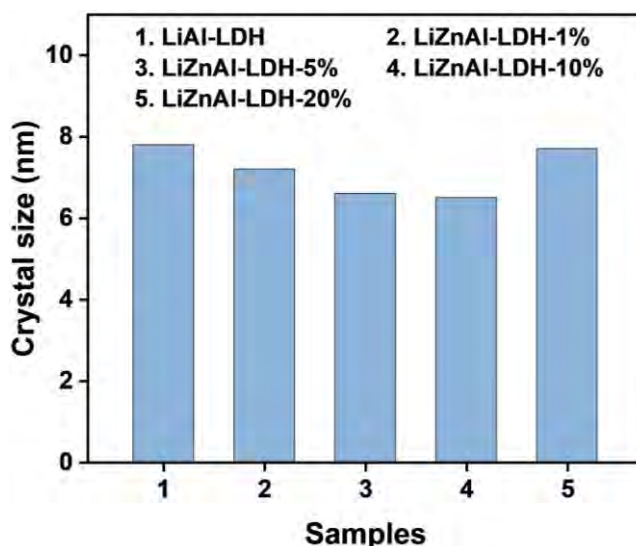
The XRD patterns of prepared adsorbents were shown in Figure 3.4a-c. It was found that the diffraction peaks belonging to  $\text{LiCl} \cdot 2\text{Al}(\text{OH})_3 \cdot n\text{H}_2\text{O}$  (JCPDS No. 31-0700) were observed in all samples, indicating that the crystalline products belong to LiAl-LDH (Figure 3.4b). Furthermore, the major crystal planes of (003) and (006) slightly shifted to the lower angle with the content of  $\text{Zn}^{2+}$  increasing (Figure 3.4a and c), confirming that  $\text{Zn}^{2+}$  (74 pm) with a larger ion radius than  $\text{Al}^{3+}$  (54 pm) was doped into the lattice of Al-O octahedrons in LiAl-LDH, resulting in crystal cell expansion according to Bragg's law ( $2d\sin\theta = n\lambda$ ) [35]. Also, these two diffraction peaks broadened with the incorporation of larger radius  $\text{Zn}^{2+}$  due to lattice distortion [36]. Besides, as the content of  $\text{Zn}^{2+}$  increased from 0% to 10%, no other impurity phases

were detected. Additional ZnO phase (JCPDS No. 74-0534), however, was determined in the XRD pattern of LiZnAl-LDH-20%. These phenomena illustrated that when the content of  $Zn^{2+}$  is less than 10%, the  $Zn^{2+}$  could be completely doped into the lattice of LiAl-LDH, while the excess  $Zn^{2+}$  could not be incorporated into the LiAl-LDH and existed in the form of oxide.



**Figure 3.4** XRD patterns of the LiAl-LDH and LiZnAl-LDHs.

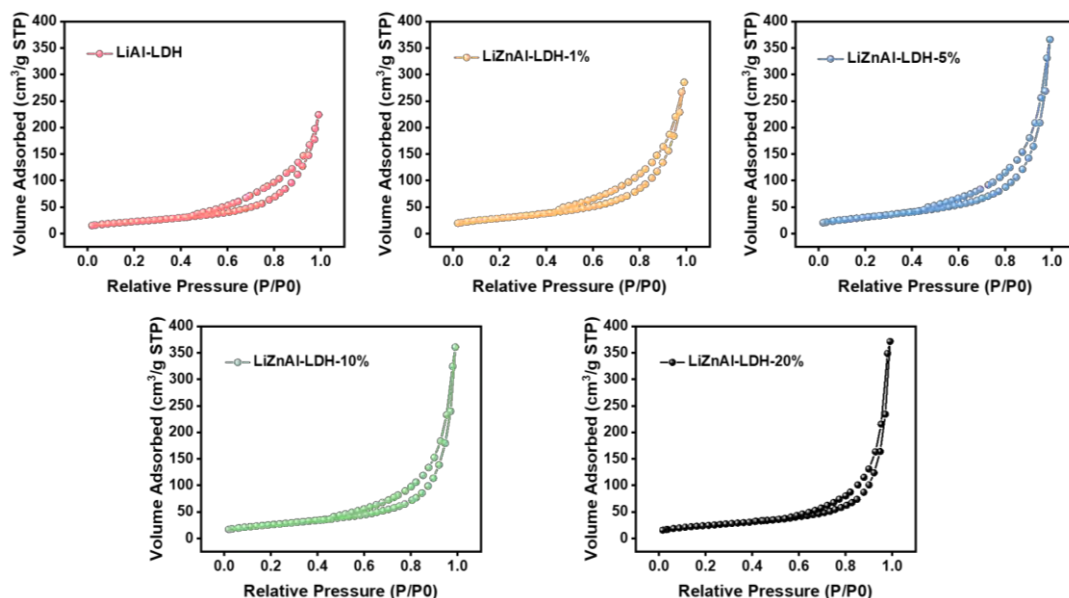
Based on the Debye-Scherrer formula,  $D = k\lambda / (FWHM \cdot \cos\theta)$  ( $D$  is crystal size,  $\lambda = 0.1541$  nm,  $k = 0.89$ , FWHM is the full width half maxima, and  $\theta$  is Bragg diffraction angle), the crystal sizes of all samples ( $D_{(003)}$ ) were calculated and presented decreasing  $D_{(003)}$  after Zn-doping (Figure 3.5), suggesting reduction of particle aggregation derived from doping engineering [2], which is conducive to shorten the transport path of  $Li^+$  within the particles and improve the specific surface area of samples [35,37].



**Figure 3.5** Crystal sizes of the LiAl-LDH and LiZnAl-LDHs based on Scherrer equation.

The improvement of LiZnAl-LDHs in textural properties could also be confirmed

by N<sub>2</sub> adsorption-desorption isotherms (Figure 3.6) and pore size analyses (Table 3.2). As observed, all samples showed type IV isotherms with a hysteresis of H3 type, revealing the mesoporous structures [25,38]. More importantly, with the doping of Zn<sup>2+</sup>, the BET specific surface area and pore volume of LiZnAl-LDHs increased conspicuously, which was conducive to the rapid transfer of Li<sup>+</sup> into the interface.

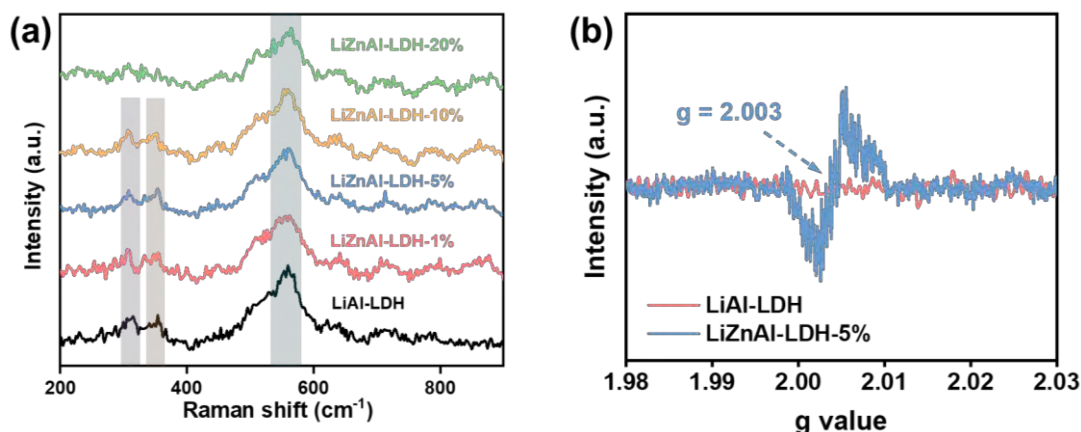


**Figure 3.6** N<sub>2</sub> adsorption-desorption isotherms of the LiAl-LDH and LiZnAl-LDHs.

**Table 3.2** The textural properties of the LiAl-LDH and LiZnAl-LDHs.

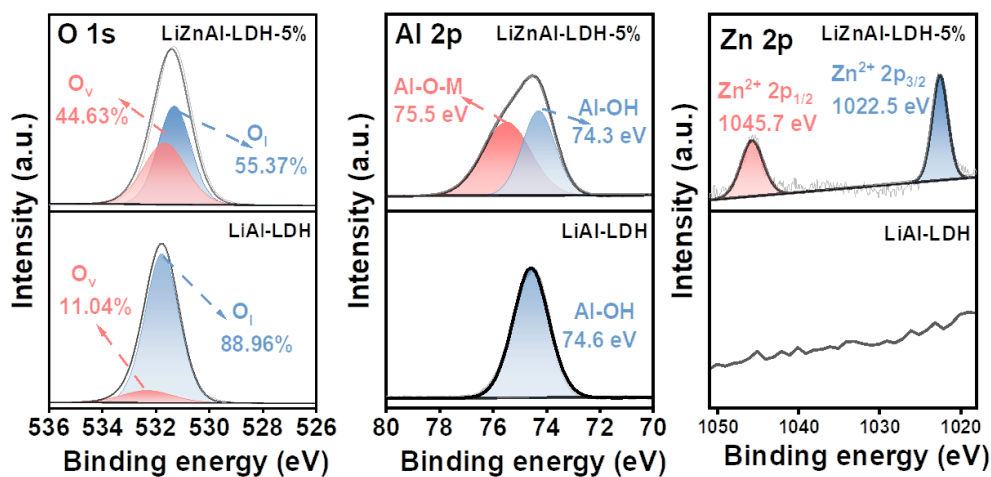
Samples	Specific surface area (m <sup>2</sup> /g)	Total pore volume (cm <sup>3</sup> /g)	Mean pore diameter (nm)
LiAl-LDH	105.6	0.4568	23.06
LiZnAl-LDH-1%	133.7	0.5075	18.51
LiZnAl-LDH-5%	166.4	0.5757	18.49
LiZnAl-LDH-10%	152.2	0.5765	18.55
LiZnAl-LDH-20%	133.4	0.4611	18.46

Raman spectra were employed to investigate the structural changes of samples (Figure 3.7a). Compared to the LiAl-LDH, several strong peaks assigned to the Al-O and Li-O stretching became broadened and weaker [39], that might be attributed to the effects of crystal distortion and surface defects (*e.g.*, oxygen vacancy) as a result of Zn<sup>2+</sup> incorporation [40]. The presence of surface oxygen vacancies was proved by EPR analyses (Figure 3.7b), in which the typical signal of oxygen vacancy was observed at  $g = 2.003$  in LiZnAl-LDH-5%.



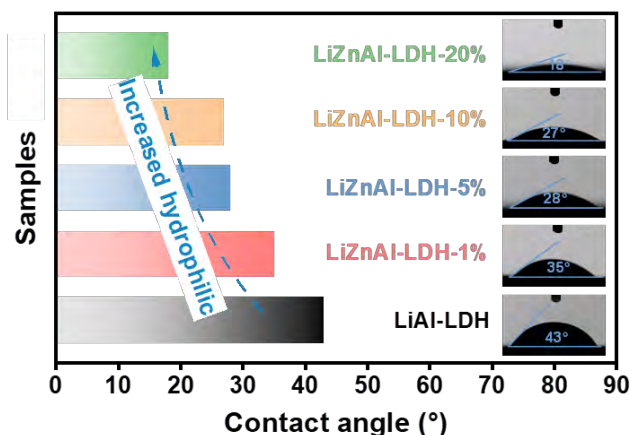
**Figure 3.7** (a) Raman spectra and (b) EPR analyses of the LiAl-LDH and LiZnAl-LDHs.

Further, XPS analyses were employed to investigate the effect of doping on the surface chemical state of LiZnAl-LDH-5%. It was found that some new peaks assigned to Al-O-Metal bond [41] and  $\text{Zn}^{2+}$  [34] appeared in Al 2p and Zn 2p spectra after Zn-doping, respectively, implying the presence of the doped  $\text{Zn}^{2+}$ . The O 1s spectra showed two major peaks at  $\sim 532.0$  and  $531.5$  eV (Figure 3.8), corresponding to oxygen vacancy ( $\text{O}_v$ ) and lattice oxygen ( $\text{O}_l$ ) species, respectively [42]. Notably, the content of  $\text{O}_v$  significantly increased for LiZnAl-LDH-5%, reconfirming the increase in oxygen vacancies, which was consistent with the results of EPR and Raman analyses.



**Figure 3.8** XPS spectra of the LiAl-LDH and LiZnAl-LDH-5%.

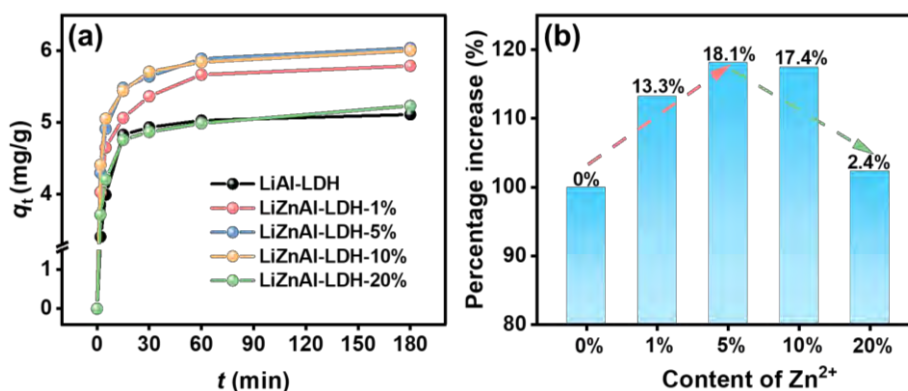
To better understand the difference in Li extraction before and after doping, the wetting ability was determined by contact angle measurement. As displayed in Figure 3.9, the contact angles of LiZnAl-LDHs decreased from  $43^\circ$  to  $18^\circ$  with the increasing  $\text{Zn}^{2+}$  dopant amount, indicating the enhanced hydrophilicity. Such feature ensured the easier transportation of  $\text{Li}^+$  [43].



**Figure 3.9** Contact angles of the LiAl-LDH and LiZnAl-LDHs.

### 3.3.3. Lithium-ion extraction performance

To evaluate the Li extraction performance of LiZnAl-LDH, the adsorption behaviors were investigated comprehensively. As shown in Figure 3.10, the  $\text{Li}^+$  adsorption capacities on LiZnAl-LDHs were enhanced with the doping of  $\text{Zn}^{2+}$ , which resulted from the stronger affinity surface and larger specific surface area. Therein, LiZnAl-LDH-5% exhibited the best  $\text{Li}^+$  uptake (6.1 mg/g within 1 h) with 18% improvement compared to the LiAl-LDH without Zn-doping. It was worth noting that although the Zn-doping had an obvious positive effect on the Li extraction, excessive amount would cause a sharp decline in  $\text{Li}^+$  uptake owing to the generation of ZnO impurities without  $\text{Li}^+$ -extraction activity in the samples.



**Figure 3.10** (a) The  $\text{Li}^+$  adsorption capacity and (b) increase of LiZnAl-LDHs with different  $\text{Zn}^{2+}$  doping amounts in brine.

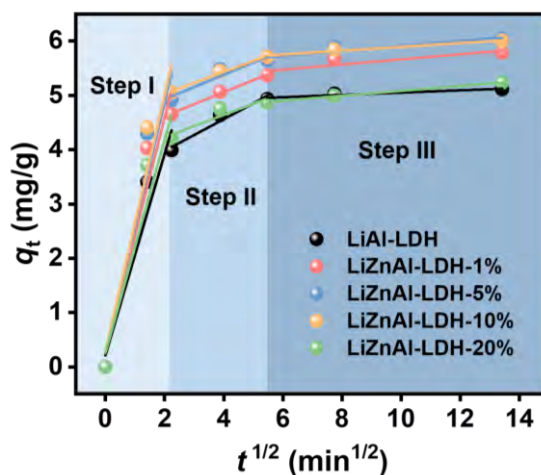
Further, the time-adsorption capacity data were analyzed for the kinetic characteristics. The results of the pseudo-first-order and the pseudo-second-order models were displayed in Table 3.3. One could see that the adsorption of  $\text{Li}^+$  on all samples was better fitted by the pseudo-second-order model, suggesting that

chemisorption is the control step of LiAl-LDH and LiZnAl-LDHs [44].

**Table 3.3** Parameters for the reactive kinetic models of  $\text{Li}^+$  on samples.

Samples	Pseudo-first order model			Pseudo-second order model		
	$k_1$ ( $\text{min}^{-1}$ )	$q_{e,\text{cal}}$ ( $\text{mg/g}$ )	$R^2$	$k_2$ ( $\text{g}/(\text{mg}\cdot\text{min})$ )	$q_{e,\text{cal}}$ ( $\text{mg/g}$ )	$R^2$
LiAl-LDH	0.0328	2.28	0.7342	0.1472	5.15	0.9999
LiZnAl-LDH-1%	0.0288	2.10	0.8621	0.1247	5.84	0.9998
LiZnAl-LDH-5%	0.0179	1.85	0.7694	0.1361	6.08	0.9999
LiZnAl-LDH-10%	0.0176	1.64	0.7383	0.1540	6.04	0.9999
LiZnAl-LDH-20%	0.0321	1.71	0.7614	0.1349	5.27	0.9997

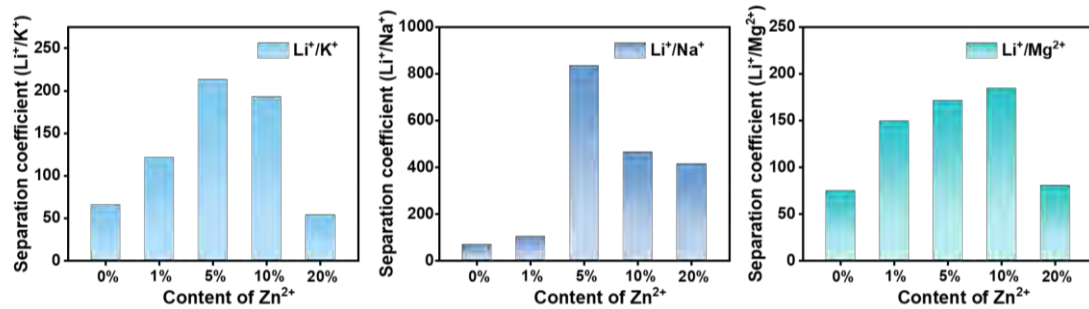
Moreover, the intraparticle diffusion model was used to examine the adsorption process. It could be found that all the Li extraction processes could be divided into three major steps (Figure 3.11), corresponding to (i) rapid transfer of  $\text{Li}^+$  from the brine solution to the interface of LiAl-LDH; (ii) dehydration of  $\text{Li}^+$  and insertion into the octahedral voids of LiAl-LDH; (iii) diffusion of  $\text{Li}^+$  into the interior of the LiAl-LDH bulk to release the external active sites [31]. In addition, LiZnAl-LDHs possess faster surface transfer rate and diffusion inside rate with higher diffusion rate constants, reconfirming that doping engineering can enhance the affinity of samples for  $\text{Li}^+$ .



**Figure 3.11** The intraparticle diffusion model for  $\text{Li}^+$  adsorption process of the LiAl-LDH and LiZnAl-LDHs.

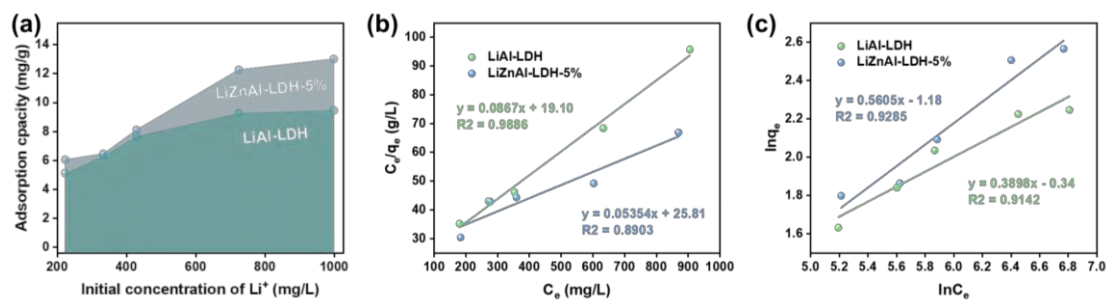
To speak of, the LiZnAl-LDHs presented significantly improved selectivity for  $\text{Li}^+$  from Figure 3.12. The main competing metal cations of Lop Nor brine involve  $\text{K}^+$ ,  $\text{Na}^+$ , and  $\text{Mg}^{2+}$ . Encouragingly, compared with the LiAl-LDH, the selectivity of  $\text{Li}^+/\text{K}^+$ ,

$\text{Li}^+/\text{Na}^+$ , and  $\text{Li}^+/\text{Mg}^{2+}$  of the LiZnAl-LDH-5% increased to ca. 3.3, ca. 12.3, and ca. 2.3 with separation factors as high as 213, 834, 171, respectively, which are well superior to those of the reported and commercialized lithium-aluminum layered double hydroxides. Such extraordinary selectivity was attributed to the high specific surface area and hydrophilicity of LiZnAl-LDH-5%, which exposed more adsorption sites and increased the number of sites for selective adsorption [45]. Considering the excellent adsorption capacity and selectivity of LiZnAl-LDH-5%, the 5% was chosen the optimal content of  $\text{Zn}^{2+}$  for the following tests.



**Figure 3.12** The comparison of the selectivity of LiZnAl-LDHs with different content of  $\text{Zn}^{2+}$  for (a)  $\text{Li}^+/\text{K}^+$ , (b)  $\text{Li}^+/\text{Na}^+$ , and (c)  $\text{Li}^+/\text{Mg}^{2+}$  in the brine.

To better assess the  $\text{Li}^+$  adsorption ability of LiZnAl-LDH-5%, the maximum adsorption ( $q_m$ ), a vital parameter in industrial applications, was determined by adsorption isotherm. As shown in Figure 3.13a, the  $q_e$  of adsorbents sharply increased and then reached a plateau (9.45 mg/g for LiAl-LDH, 13.10 mg/g for LiZnAl-LDH-5%) with the  $\text{Li}^+$  concentration of 750 mg/L. Furthermore, the Langmuir and Freundlich models were applied to elucidate the adsorption process. From Figure 3.13b-c, the Langmuir model fitted better with LiAl-LDH, whereas the Freundlich model could describe better the adsorption on LiZnAl-LDH-5%, revealing a potential change in the adsorption mechanism from monolayer adsorption to multilayer adsorption after Zn-doping [44].



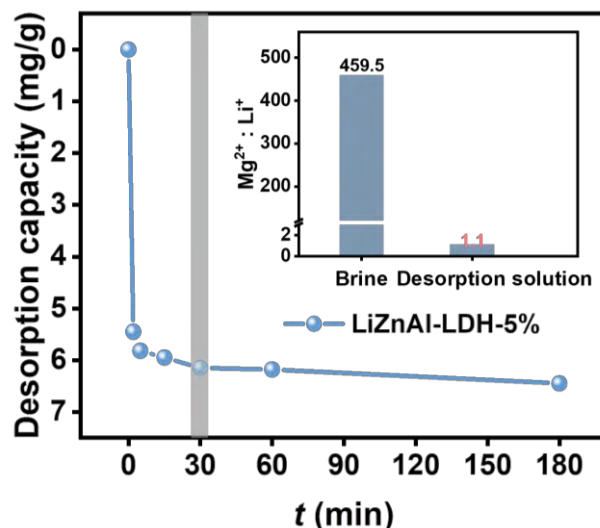
**Figure 3.13** (a) The adsorption capacity of  $\text{Li}^+$  with different initial concentration on

the LiAl-LDH and LiZnAl-LDH-5%. (b) Langmuir and (c) Freundlich models of  $\text{Li}^+$  on pristine LiAl-LDH and LiZnAl-LDH-5%.

Washing process with deionized water was adopted to desorb ions in saturated adsorbents after initial Li extraction procedure. The desorption solution was mainly composed of  $\text{Li}^+$  and  $\text{Mg}^{2+}$  with sporadic amounts of  $\text{K}^+$  and  $\text{Na}^+$ . Importantly, the  $\text{Mg}^{2+}/\text{Li}^+$  mass ratios sharply decreased from 459.5 in raw brine to 1.1 in desorption solution, which is greatly lower than the 1.8 in that of pristine LiAl-LDH (Table 3.4). Moreover, the desorption kinetics and cation ( $\text{Li}^+$ ,  $\text{K}^+$ ,  $\text{Na}^+$  and  $\text{Mg}^{2+}$ ) concentrations of elution solutions were presented in Figure 3.14. It could be seen that LiZnAl-LDH-5% had a fast  $\text{Li}^+$  desorption rate with 30 min. Thus, LiZnAl-LDH-5% is a promising adsorbent for  $\text{Li}^+$  recovery from brine with ultrahigh  $\text{Mg}^{2+}/\text{Li}^+$  mass ratios.

**Table 3.4** The cation concentrations of adsorbents elution solutions.

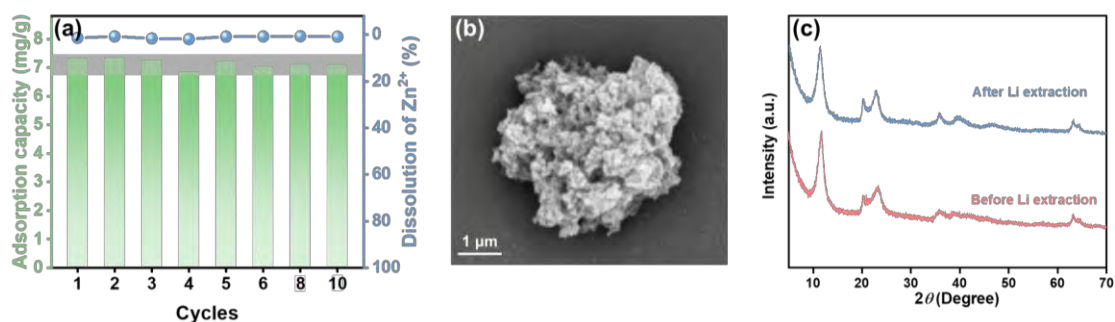
Samples	$\text{Li}^+$ (mg/L)	$\text{Mg}^{2+}$ (mg/L)	$\text{Na}^+$ (mg/L)	$\text{K}^+$ (mg/L)
LiAl-LDH	79.3	143.885	11.28	6.865
LiZnAl-LDH-5%	66.95	74.905	4.18	3.415



**Figure 3.14** The  $\text{Li}^+$  desorption capacity of LiZnAl-LDH-5%. Inset is the  $\text{Mg}^{2+}/\text{Li}^+$  mass ratios in brine and desorption solution.

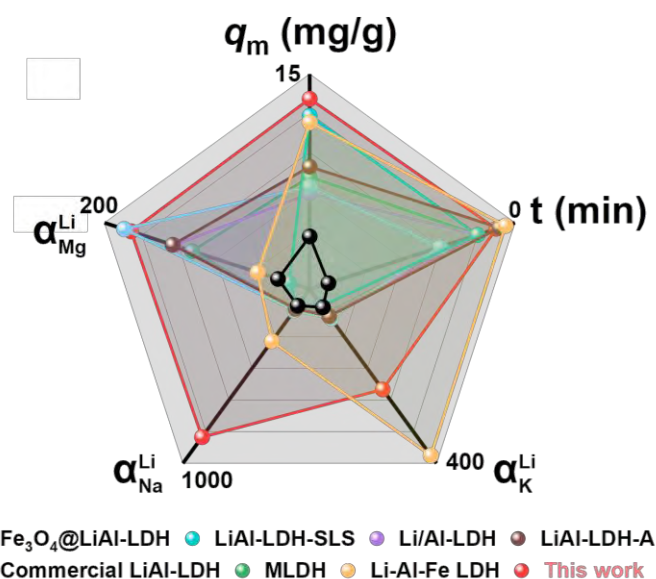
Also, the LiZnAl-LDH-5% exhibited long-term stability with a neglected  $\text{Zn}^{2+}$  loss (Figure 3.15a). Specifically, the adsorption capacity of LiZnAl-LDH-5% maintained almost unchanged of 7.0 mg/g in 10 cycles and showed almost no loss of  $\text{Zn}^{2+}$  in each subsequent cycle. From Figure 3.15b-c, the SEM image and XRD pattern after  $\text{Li}^+$

adsorption showed neglected changes as well. These results indicated the good reusability and stability of LiZnAl-LDH-5% when applied in Li extraction from brines.



**Figure 3.15** (a) The reusability and stability of LiZnAl-LDH-5%. (b) The SEM image of LiZnAl-LDH-5% after lithium extraction. (c) XRD patterns of LiZnAl-LDH-5% before and after lithium extraction.

At the same time, in comparison with previously reported lithium-aluminum layered double hydroxides (Figure 3.16), the Li extraction performance of LiZnAl-LDH-5% from brines, including  $q_m$ , adsorption kinetics, the selectivity of Li<sup>+</sup>/K<sup>+</sup>, Li<sup>+</sup>/Na<sup>+</sup> and Li<sup>+</sup>/Mg<sup>2+</sup>, is extraordinarily excellent.

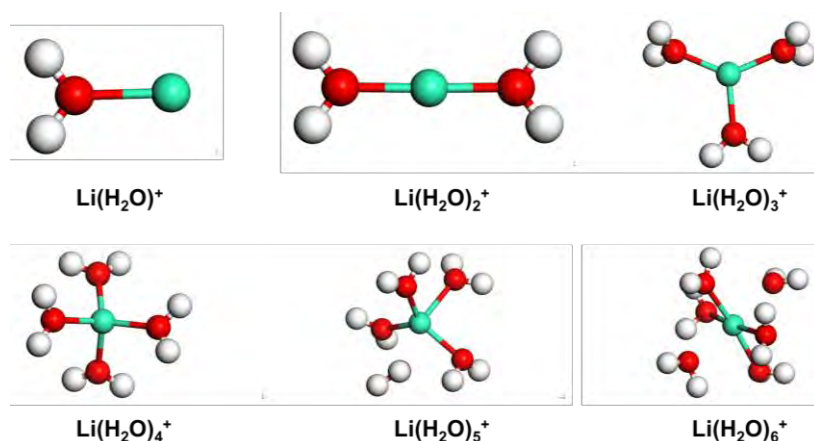


**Figure 3.16** Comparison of Li extraction performance of different lithium-aluminum layered double hydroxides.

### 3.3.4. Mechanisms of enhanced performance for lithium extraction by Zn-doping

The preceding experiments demonstrated that LiZnAl-LDHs have a better Li extraction compared to pristine LiAl-LDH. The role of Zn-doping, however, is still unclear. Computational simulations were conducted to illustrate the mechanisms of

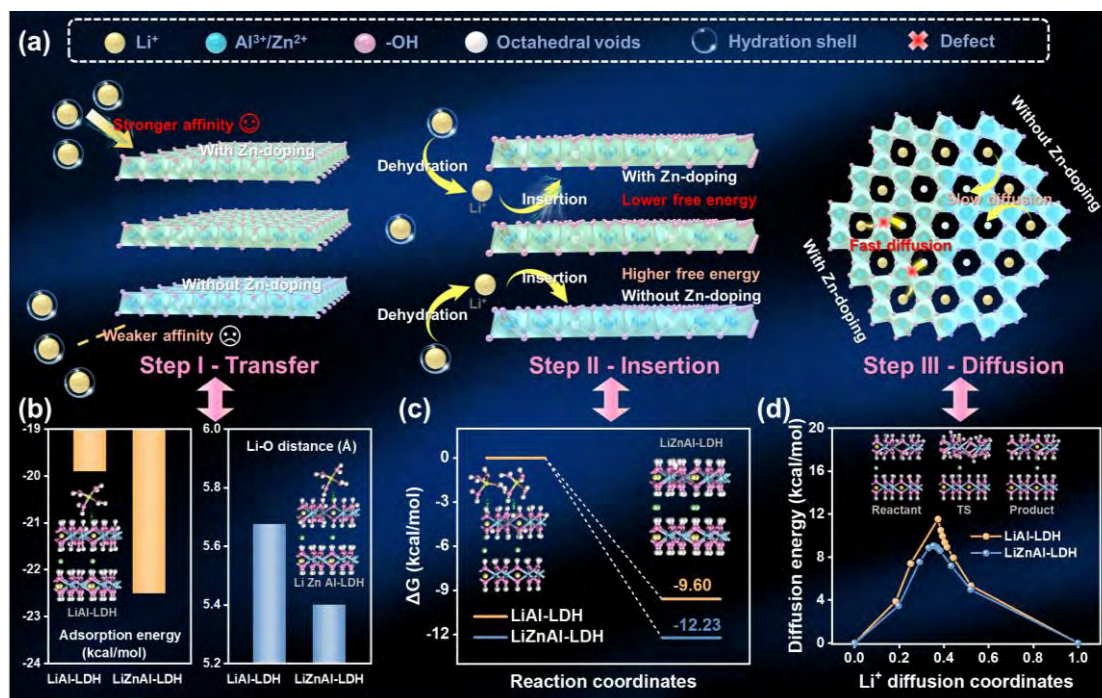
improved adsorption performance of LiZnAl-LDHs for  $\text{Li}^+$ . Generally, metal ions tend to bind to water molecules to form stable hydrated metal ion structures. For lithium-ion, four-coordinated structure  $[\text{Li}(\text{H}_2\text{O})_4]^+$  is deemed to be the favorable hydration clusters in the aqueous phase [31], which was also certified by the results of calculations (Figure 3.17). Thus, the adsorption processes of  $\text{Li}(\text{H}_2\text{O})_4^+$  on samples before and after Zn-doping were researched in detail.



**Figure 3.17** Optimal configuration of hydrated lithium ions.

During the transfer step, only the typical adsorption sites at the tip of the octahedral voids were considered owing to the “ion sieve effect” of LiAl-LDHs. Then, the adsorption energies ( $E_{\text{ad}}$ ) of  $\text{Li}(\text{H}_2\text{O})_4^+$  on LiZnAl-LDHs and pristine LiAl-LDH were simulated in Fig (Figure 3.18b), respectively, in which the LiZnAl-LDHs possessed more negative  $E_{\text{ad}}$  (-22.51 kcal/mol) than LiAl-LDH without Zn-doping (-19.90 kcal/mol). Meanwhile, the Li-O distance of the former (5.401 Å) was apparently shorter compared with the latter. These results indicated that doping engineering delivered a stronger  $\text{Li}^+$  affinity to the LiZnAl-LDHs, enabling easier transfer of  $\text{Li}(\text{H}_2\text{O})_4^+$  from the brine solution to the surface of LiZnAl-LDHs, which was consistent with the results of intraparticle diffusion model analyses [25]. The improvement in transfer might be due to lower surface charge, higher specific surface area and more hydrophilic surface of sample after Zn-doping. Further, the  $\text{Li}^+$  transferred and adsorbed on the surface is ready for the following insertion reaction step. With the help of more negative  $E_{\text{ads}}$ , the  $\text{Li}(\text{H}_2\text{O})_4^+$  was more easily dehydrated and inserted into the lithium vacancies of LiZnAl-LDH, which could be manifested by the lower Gibbs free energy ( $\Delta G$ ) of the insertion reaction (Figure 3.18c). In the final step (diffusion), the  $\text{Li}^+$  inserted was ready to diffuse into the bulk of LiAl-LDH to release the external active sites. Thus, the

diffusion pathways of  $\text{Li}^+$  between two adjacent octahedral voids were simulated. It could be seen that the diffusion energy barrier for  $\text{Li}^+$  within pristine  $\text{LiAl-LDH}$  was calculated to be 11.53 kcal/mol (Figure 3.18d). After Zn-doping, the  $\text{Li}^+$  diffusion process within  $\text{LiZnAl-LDH}$ s was accelerated with lower diffusion energy, which might result from the presence of defects [46].



**Figure 3.18** (a) Three-steps schematic representation of Li extraction on pristine  $\text{LiAl-LDH}$  and  $\text{LiZnAl-LDH}$ . (b) Theoretical calculation analysis: The adsorption energy of  $\text{Li}(\text{H}_2\text{O})_4^+$  on pristine  $\text{LiAl-LDH}$  and  $\text{LiZnAl-LDH}$ s surface; (c) The Gibbs free energy of Li-insertion reaction on pristine  $\text{LiAl-LDH}$  and  $\text{LiZnAl-LDH}$ s; (d) The diffusion energy barrier of  $\text{Li}^+$  within pristine  $\text{LiAl-LDH}$  and  $\text{LiZnAl-LDH}$ s.

Based on above analyses, it could be deduced that the doping engineering can deliver a superior Li extraction performance to  $\text{LiAl-LDH}$  by facilitating the transfer of  $\text{Li}(\text{H}_2\text{O})_4^+$ , reducing the free energy of Li-insertion reaction, and accelerating the solid-phase diffusion of  $\text{Li}^+$ . Eventually, the prepared  $\text{LiZnAl-LDH}$ s presented unprecedented potential as  $\text{Li}^+$  adsorbent.

### 3.4. Conclusions

In summary, the doping engineering of  $\text{LiZnAl-LDH}$ s were achieved via one-pot co-precipitation method, which can make up the unsatisfactory performance of  $\text{LiAl-LDH}$ s commercial adsorbents for Li extraction. Benefited from the Zn-doping, the

enhanced specific surface area, hydrophilic as well as surface attraction for  $\text{Li}^+$ , and the generation of intrinsic defects comprehensively improved the Li extraction performance. That is,  $q_m$  is up to 13.10 mg/g, and  $\alpha_{\text{K}^+}^{\text{Li}^+}$ ,  $\alpha_{\text{Na}^+}^{\text{Li}^+}$  and  $\alpha_{\text{Mg}^{2+}}^{\text{Li}^+}$  for Lop Nor brine are as high as 213, 834, 171, respectively, which are far superior to the reported and commercialized LiAl-LDHs. Furthermore, combining experiments and theoretical calculations, a three-steps process for Li extraction on LiAl-LDHs was proposed. Importantly, after the doping engineering, the LiZnAl-LDH exhibits the more favorable three-steps processes with more negative adsorption energy and Gibbs free energy for  $\text{Li}^+$  transfer and insertion, and lower  $\text{Li}^+$  diffusion energy barrier. Overall, this work provides a prospective strategy for promote the development of the Li extraction industry on a larger scale.

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## Chapter 4. Steering interlayer interaction of lithium-aluminum layered double hydroxide beads for stable lithium extraction from sulfate-type brines

### 4.1. Introduction

Lithium, one of the most valuable energy metals, has been widely applied in numerous areas, particularly in lithium-ion batteries (LIBs) [1-4]. To ensure the sustainable development of LIBs market, it is imperative to extract lithium from brines due to high lithium reserves (60% of the global total) and low environmental impact, yet hampered by competing ions with high concentrations, such as  $Mg^{2+}$  [5-7]. Adsorption has a reputation for lithium extraction from brines with ultrahigh  $Mg^{2+}/Li^+$  ratios owing to low cost, superior  $Li^+$  selectivity and performance [8-10]. Up to date, lithium-aluminum layered double hydroxide (LiAl-LDH) are the most successful industrialized adsorbents for recovering  $Li^+$  from brines because of stable adsorption performance and easy elution with deionized water [11,12]. Nevertheless, the applications of LiAl-LDH focus on  $Cl^-$ -type brines, less on  $SO_4^{2-}$ -type brines, another common lithium-bearing brines in nature, as a result of deactivation caused by the abatement of adsorption capacity during long-term process [13-15].

The essential reason for the deactivation of LiAl-LDH in  $SO_4^{2-}$ -type brines is the intercalation of  $SO_4^{2-}$  into interlayers, which hinders the  $Li^+$  desorption and reduces subsequent  $Li^+$  adsorption. The generic formula of LiAl-LDH can be expressed as  $LiX \cdot mAl(OH)_3 \cdot nH_2O$ , where X represents the interlayer anions, which connect to the laminates by interactions, like electrostatic interactions [16-18]. The  $Li^+$  adsorption-desorption process of LiAl-LDH can be described by  $LiX \cdot mAl(OH)_3 \cdot nH_2O + H_2O \rightleftharpoons xLiX + (1-x)LiX \cdot mAl(OH)_3 + (n+1) H_2O$ , in which  $Li^+$  ( $\sim 0.68 \text{ \AA}$ ) can insert into octahedral cavities of  $Al(OH)_3$  ( $0.70 \text{ \AA}$ ) through size and memory effect [19-21]. Interlayer anions would simultaneously intercalate or deintercalate to maintain the electroneutrality of LiAl-LDH during the  $Li^+$  adsorption or desorption process [8,22]. Notably, LDHs possess anion exchange property with the order of  $PO_4^{3-} > CO_3^{2-} > SO_4^{2-} > OH^- > Cl^-$ , and the species, radius, and content of interlayer anions affect the structures and physiochemical properties of LDHs [23,24]. Tarasov et al. [25] found

that the desorption rate of  $\text{Li}^+$  on LiAl-LDH relies on the interlayer anion via in-situ XRD analysis, where  $\text{Li}^+$  would spontaneously release in water with  $\text{Cl}^-$ , and the deintercalation of  $\text{Li}^+$  would only complete 40% with  $\text{SO}_4^{2-}$ , causing the decreasing adsorption sites for  $\text{Li}^+$ . The stronger stability of LiAl-LDH intercalated with  $\text{SO}_4^{2-}$  (LiAl-LDH-S) than that with  $\text{Cl}^-$  (LiAl-LDH-Cl) was also confirmed by electronic analyses [26]. At the atomic level, due to the electrostatic attraction between guest  $\text{SO}_4^{2-}$  and host laminates is stronger compared with  $\text{Cl}^-$ , the intercalation of  $\text{Li}_2\text{SO}_4$  requires lower energy barrier, but higher energy barrier for deintercalation [27]. Hence,  $\text{SO}_4^{2-}$  in brines tend to replace interlayer  $\text{Cl}^-$  by ion exchange, obstructing the  $\text{Li}^+$  desorption, thus reducing the re-adsorption capacity of LiAl-LDH.

Currently, limited efforts have been carried out by researchers to address this dilemma. For example, the desorption of intercalated  $\text{Li}^+$  and  $\text{SO}_4^{2-}$  on LiAl-LDH would be improved by increasing temperature and eluent consumption [28]. Worryingly, the structures of LiAl-LDH readily collapse and transfer to gibbsite without Li extraction activity under such conditions [13,29,30]. The evasive strategy of removing  $\text{SO}_4^{2-}$  by nanofiltration and resin ion exchange prior to Li extraction avoided the  $\text{SO}_4^{2-}$  intercalation in LiAl-LDH, but operational costs and complexity skyrocketed [31]. Moreover, these methods failed to essentially solve dilemma. The efforts to overcome the deactivation of LiAl-LDH in Li extraction from  $\text{SO}_4^{2-}$ -type brines are still needed.

Compared to monovalent  $\text{Cl}^-$ , divalent  $\text{SO}_4^{2-}$  show higher ionic potentials (charge/radius, a critical parameter to describe the electric field intensity) [32], which provides spur for modification of LiAl-LDH. Based on the Coulomb's law, it is reasonable to speculate that the introduction of few negatively charged anions with highly ionic potentials to replace partial  $\text{Cl}^-$  in the interlayer of LiAl-LDH would induce a higher electrostatic repulsion with  $\text{SO}_4^{2-}$ , hindering the intercalation of  $\text{SO}_4^{2-}$ , and thus promising a solution to the feasibility of lithium extraction from  $\text{SO}_4^{2-}$ -type brines. To speak of, the excessive desorption of LiAl-LDH is also solved by regulating the intercalation amount of highly negatively charged anions to precisely anchor the amount of  $\text{Li}^+$  required to maintain structural stability in the host layer, without impacting the deintercalation of LiCl adsorbed in LiAl-LDH, killing two birds with one stone. Herein, a novel strategy of steering interlayer interaction by replacing part of the  $\text{Cl}^-$  in the interlayer of LiAl-LDH with  $\text{PO}_4^{3-}$  (LiAl-LDH-P) was proposed to realize long-term recycling of LiAl-LDH in  $\text{SO}_4^{2-}$ -type brines. As a proof of concept, a mechanically robust LiAl-LDH-P bead (BLDH-P) was constructed to evaluate the

advancement of the resulting adsorbent in static and dynamic Li extraction in Lop Nur salt lake brine, the largest sulfate-type brine in the world. The adsorption, desorption, re-adsorption performance and property for preventing  $\text{SO}_4^{2-}$  intercalation of BLDH-P were comprehensively performed. Density functional theory (DFT) calculations were used to reveal the mechanisms of the steering interlayer interaction as well. This work provides a solution for sustainable lithium extraction from  $\text{SO}_4^{2-}$ -type brines and offers insights into the design of promising LDHs.

## 4.2. Experimental section

### 4.2.1. Reagents and materials

Lithium chloride (LiCl), aluminum chloride hexahydrate ( $\text{AlCl}_3 \cdot 6\text{H}_2\text{O}$ ), sodium dodecahydrate phosphate ( $\text{Na}_3\text{PO}_4 \cdot 12\text{H}_2\text{O}$ ), sodium hydroxide (NaOH), polyvinyl chloride (PVC), N, N-dimethylformamide (DMF), and polyacrylonitrile (PAN) were purchased from Aladdin Co., Ltd. All reagents are analytical grade without further purification.

The brine used in the experiments was obtained from Lop Nor Salt Lake Brine, a typical sulfate-type brine. The detailed compositions were summarized in Table 4.1.

**Table 4.1** Properties of Lop Nor brine before and after static extraction.

$\text{Li}^+$ (mg/L)	$\text{Mg}^{2+}$ (mg/L)	$\text{Na}^+$ (mg/L)	$\text{K}^+$ (mg/L)	$\text{SO}_4^{2-}$ (mg/L)	$\text{Cl}^-$ (mg/L)	pH
223.2	106045	3284.8	3725.6	37600	222400	5.04

### 4.2.2. Preparation of BLDH-P

Lithium-aluminum layered double hydroxide intercalated with phosphate ions (LiAl-LDH-P) were obtained by a modified co-precipitation method with reference to our previous research [19]. Furthermore, the  $\text{PO}_4^{3-}$  intercalated LiAl-LDH beads (BLDH-P) were prepared via inverse solvent phase conversion method.

Specifically, the solution with the  $\text{AlCl}_3$ :LiCl molar ratio of 2:1 was added into mixture solution of NaOH (8mol/L) and  $\text{Na}_3\text{PO}_4$ , stirred until the pH of mixed solution was 6, and then aged at 80 °C for 30 min to achieve the LiAl-LDH-P powder. Considering the balance between adsorption capacity and desorption ability, an adequate concentration of  $\text{PO}_4^{3-}$  (0.05 mol/L) was selected. Next, the  $\text{PO}_4^{3-}$  intercalated LiAl-LDH beads (BLDH-P) was prepared via inverse solvent phase conversion method, in which LiAl-LDH-P powder was mixed with PAN/PVC in wight ratio of 8:2 using

DMF as solvent to product adsorption-binder slurry, and then the slurry was dropped into deionized water using the injector to form adsorbent beads called BLDH-P-x (x represents the weight ratio of PAN in the binder,  $x = 0, 20\%, 40\%, 50\%$ , and  $60\%$ ). For comparison,  $\text{Cl}^-$  intercalated LiAl-LDH beads (BLDH-Cl) were also prepared by similar procedure except for the preparation of LiAl-LDH-Cl without  $\text{Na}_3\text{PO}_4$ .

#### **4.2.3. Characterizations**

The morphological structure and the elemental distribution of materials were observed by scanning electron microscopy (SEM, Phenom-Pro XL, China) equipped with energy distributions (EDS) system. To analyzed the materials phase structure, the X-ray diffraction (XRD) patterns were measured by the powder X-ray diffractometer (D8 ADVANCE X, Germany) with  $\text{Cu K } \alpha$  radiation (40 kV, 100 mA). The surface functional groups of materials were determined using the Fourier transform infrared spectrometer (FTIR, 6700, Nicolet, USA). The  $\text{N}_2$  adsorption-desorption measurements were performed by ASAP2460 aperture analyzer (Micromeritics, USA) to analyze the surface specific area, porosity and pore size of materials. The microscopic contact angle meter (Kyowa Interface Science Co. Ltd., Japan) was employed to obtain the contact angle (CA) of materials. The concentrations of anions and cations were measured by the anion chromatograph (Dionex Aquion, Thermo Scientific, USA) and the atomic absorption spectrum (AAS, G8434A, Japan). The chemical oxygen demand (COD) of dissolution was measured by the dichromate method based on the Standard of the People's Re public of China for Environmental Protection (GB 11914-89).

#### **4.2.4. Lithium-ion extraction**

Lithium extraction experiments were all performed in Lop Nor brine. Static experiments were conducted at room temperature in thermostatic water bath at 150 rpm (20 g/L), while dynamic experiments in a fixed bed with an inner diameter of 2.4 cm and a height of 30 cm. Adsorption kinetics were performed, and the pseudo-first-order, pseudo-second-order kinetic model, and the intraparticle diffusion models were used to analyzed experimental data, respectively [33]. Adsorption isotherms were carried out for 36 h, and the Langmuir and Freundlich models were employed to fit experimental data, respectively [19]. The desorption experiments were carried out by using deionized water with the solid/liquid of 1 g/50 mL as the eluent, stirred at 150 rpm for 8 h at 25 °C. Considering the residual brine adhered to the surface of adsorbents, a rapid washing through ice water (1 g/5 mL) was performed before the desorption procedure. The

adsorption capacity ( $q_t$ , mg/g) and desorption capacity ( $q_d$ , mg/g) were calculated by Equation 4.1-4.2:

$$q_t = (C_0 - C_t)V/m \quad (4.1)$$

$$q_d = C_d V/m \quad (4.2)$$

where  $C_0$ ,  $C_t$ , and  $C_d$  (mg/L) represent initial, residual, and desorption concentration, respectively.  $V$  (L) is the volume of brine, and  $m$  (g) indicates the mass of adsorbent.

The  $\text{Li}^+$  adsorption selectivity was evaluated by the distribution coefficient  $K_d$  (mL/g) and separation coefficient  $\alpha_{\text{Li M}}$ , which were determined by Equation 4.3-4.4:

$$K_d = V(C_0 - C_e)/(mC_e) \quad (4.3)$$

$$\alpha_{\text{M}}^{\text{Li}} = K_{d, \text{Li}}/K_{d, \text{M}} \quad (4.4)$$

where M represents other cations.

#### 4.2.5. Theoretical calculations

The Gaussian 09 software was used to calculate the electrostatic potential (ESP) distributions described using basis set of 6-31+G(d), and the results were analyzed by GaussView 5.0 [34]. The binding energies between anions and energy barriers of anions diffusion were performed by Materials Studio software (MS 8.1, Accelrys, San Diego, CA). The exchange-correlation interactions were established by the generalized gradient approximation of Perdew-Burke-Ernzerhof (GGA-PBE). The structures of LiAl-LDH-P and LiAl-LDH-Cl with interlayer spacing of 7.45 Å and 7.67 Å was constructed by modifying the structure obtained from Materials Project (Materials ID: mp-643655), respectively. The cut-off energy was set to 580 eV and the k-point mesh with a size of  $3 \times 1 \times 1$  grid was used. The convergence criteria for displacement, energy, and force were 0.002 Å,  $2 \times 10^{-5}$  eV/atom, and 0.05 eV/Å, respectively. The binding energy ( $E_b$ ) were calculated by Equation 4.5:

$$E_b = E_{A/B} - E_A - E_B \quad (4.5)$$

where  $E_{A/B}$  represents the total energy of A and B bonded system;  $E_A$  and  $E_B$  were the energies of individual A and B, respectively.

Further, the Gibbs free energies ( $G$ ) as followed Equation 4.6. The energy barrier of anions diffusion within the LiAl-LDH were carried out via transition states searching, which were conducted by linear and quadratic synchronous transit (LST/QST) method nudged elastic band (NEB) tools implemented in DMol<sup>3</sup> [35,36].

$$G = E_{\text{DFT}} + E_{\text{ZPE}} - TS \quad (4.6)$$

where  $E_{\text{DFT}}$  indicates the total energy calculated through density functional theory (DFT);  $E_{\text{ZPE}}$  and  $TS$  represent the zero-point energy and the entropic contribution, respectively.

### 4.3. Results and discussion

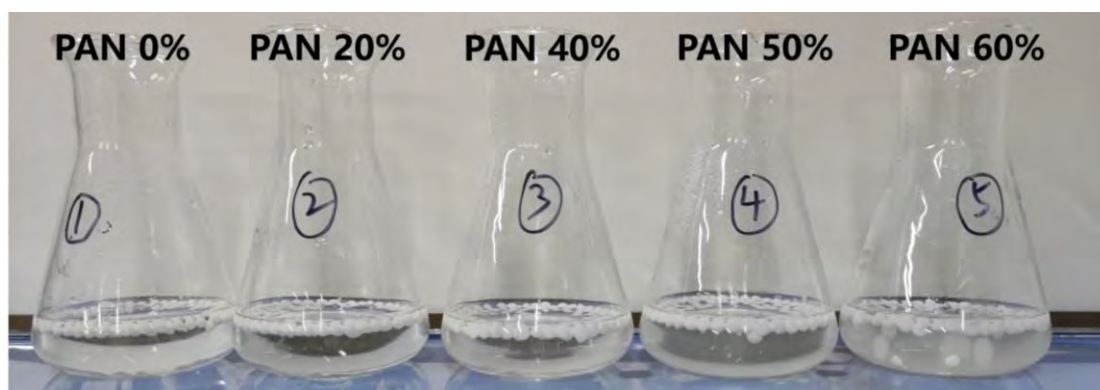
#### 4.3.1. Construction and optimization of LiAl-LDH beads

Considering the readily available and high mechanical properties, the polyvinyl chloride (PVC) can be an ideal binder for the large-scale production adsorbent beads [37]. Nevertheless, the diffusion process of  $\text{Li}^+$  from brine to adsorbent surface is always impeded due to the hydrophobic instinct of PVC, which might be addressed by combination of hydrophilic polymer blend, such as polyacrylonitrile (PAN). Hence, the phosphate ions intercalated lithium-aluminum layered double hydroxide beads (BLDH-P) were prepared by co-precipitation followed by antisolvent method using PVC and PAN as the hybrid binders (Figure 4.1).



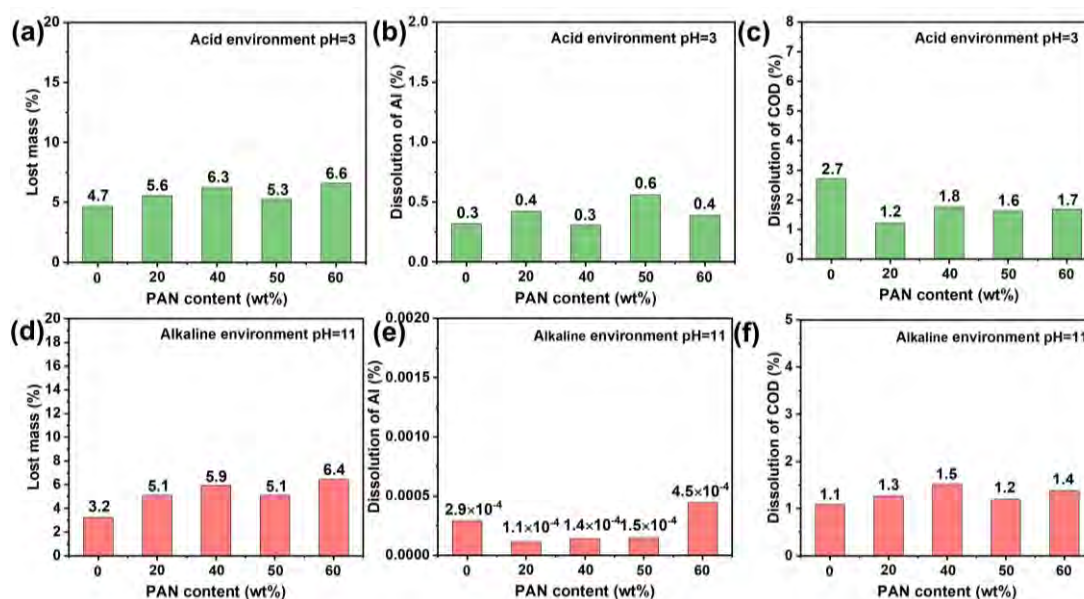
**Figure 4.1** Schematic illustration of the fabrication strategy for BLDH-P beads.

The resultant BLDH-P beads appeared while with the diameters of 2.5-4.0 mm. The compatibility of both binders was optimized through determining the lithium extraction performance and stability of BLDH-P with various PVC/PAN ratios. As illustrated in the Figure 4.2, most BLDH-P mixtures were transparent except for the BLDH-P-60% after 24h of vigorous shaking in the brine. Such phenomena suggested that BLDH-P beads with suitable contents (i.e., PAN/PVC=0-50%) presented well stability.



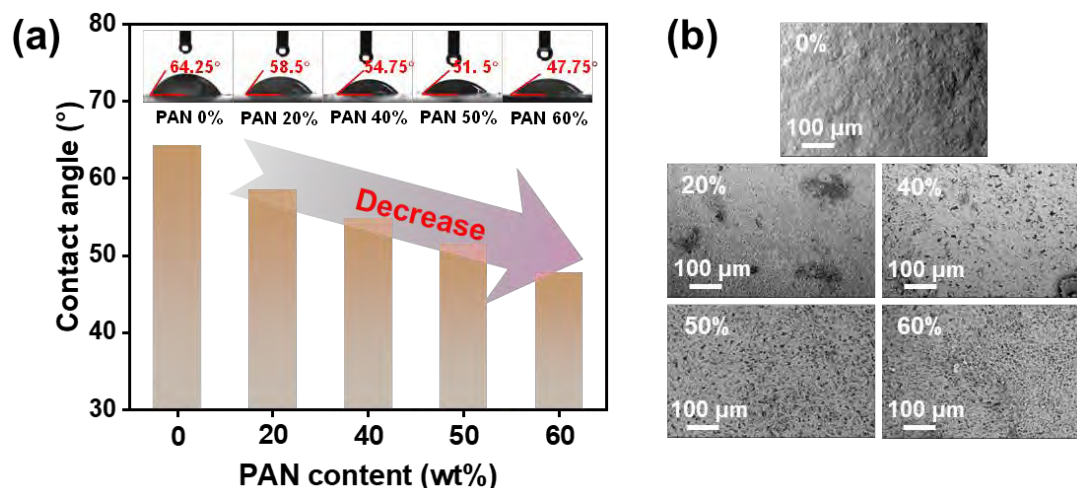
**Figure 4.2** Optical photographs of the BLDH-P with various PVC/PAN ratios after 24h of vigorous shaking in brine.

The stability of adsorbents was confirmed by the dissolution results of BLDH-P beads in strong acid (pH=3) and alkali (pH=11) solutions. From Figure 4.3, it can be found that the mass losses, dissolution amounts of  $Al^{3+}$  and dissolution COD of BLDH-P were negligible levels except for a few samples with high PAN content.



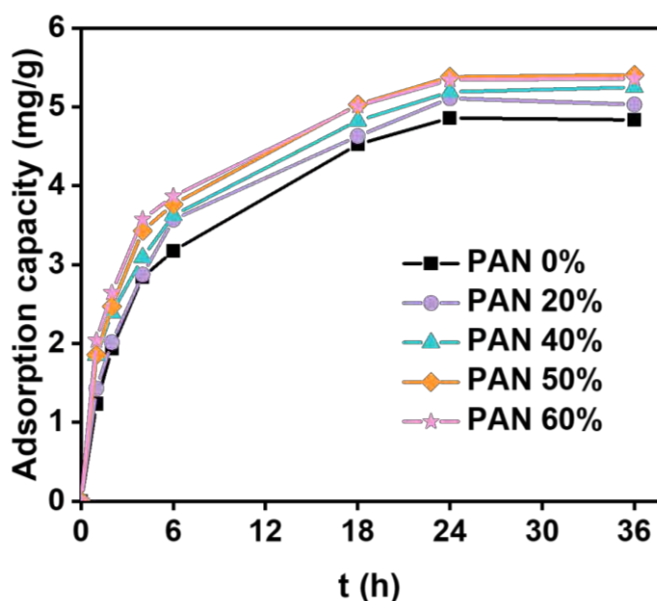
**Figure 4.3** Mass losses, dissolution amounts of  $Al^{3+}$  and dissolution COD of BLDH-P beads with various PVC/PAN ratios in strong acid and alkali solutions.

Moreover, the effect of PVC/PAN ratios on wettability and surface structures was investigated to reveal the Li extraction potential of BLDH-P. As shown in Figure 4.4a, the contact angles of BLDH-P decreased from  $64.25^\circ$  to  $47.75^\circ$  with the increasing PAN content. Meanwhile, the pore number and roughness of BLDH-P surfaces increased with the addition of PAN (Figure 4.4c). These results indicated the improved water permeability and hydrophilicity, favoring  $Li^+$  diffusion and transfer on adsorbent beads.



**Figure 4.4** (a) Contact angles, and (b) SEM images of BLDH-P beads with various PVC/PAN ratios.

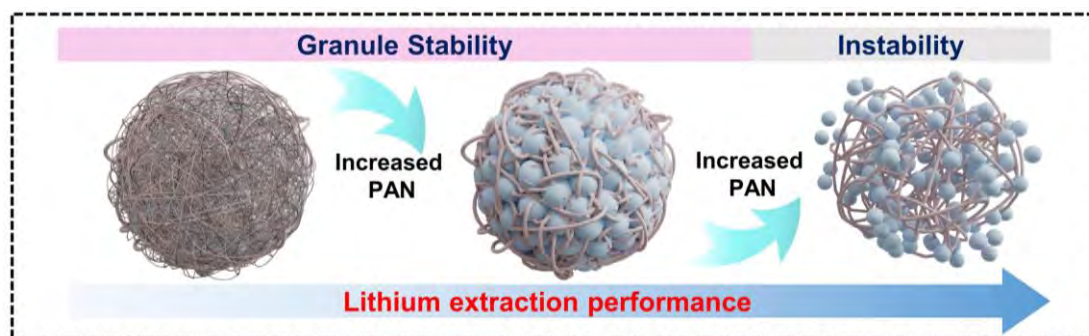
As expected, as the PAN content increased, BLDH-P exhibited a gradual grow in the  $\text{Li}^+$  adsorption capacity in Lop Nor brine (Figure 4.5). Notably, the capacity of BLDH-P-50% was similar to that of BLDH-P-60%, which might result from the instable structure at high PAN content.



**Figure 4.5**  $\text{Li}^+$  adsorption capacities of BLDH-P beads with various PVC/PAN ratios.

In light of the above discussions, the full effect of PVC/PAN ratios was unveiled and schematically illustrated in Figure 4.6, where the Li extraction performance enhanced with the increasing PAN content, and the BLDH-P beads were capable of maintaining stable structure at appropriate PAN content, however, were instable at high content. BLDH-P-50% (abbreviated BLDH-P) was selected as the optimal lithium

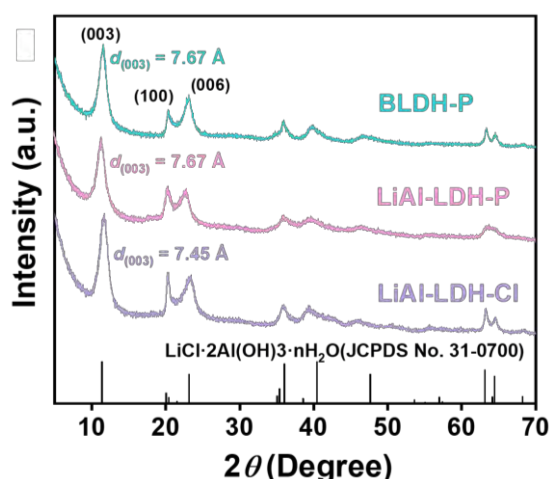
adsorbent for following investigation as well.



**Figure 4.6** Schematic illustration of effect of PVC/PAN ratios on BLDH-P beads.

#### 4.3.2. Characterization of LiAl-LDH beads intercalated with $PO_4^{3-}$

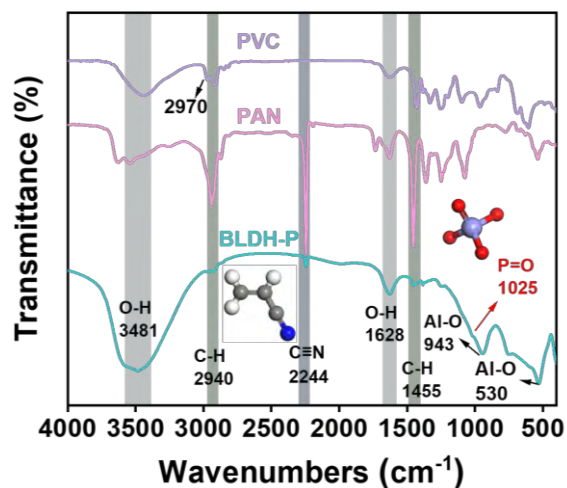
Micro-characterization and physicochemical properties of BLDH-P beads was systematically carried out. The X-ray diffraction (XRD) patterns in Figure 4.7 showed that all the characteristic diffraction peaks of LiAl-LDH-Cl and LiAl-LDH-P powder were well indexed into the standard card of the  $LiCl \cdot 2Al(OH)_3 \cdot nH_2O$  (JCPDS No. 31-0700), indicating that crystalline products belong to LiAl-LDH. It was worth noting that compared to the LiAl-LDH-Cl, the crystal plane of (003) of LiAl-LDH-P mildly shifted to the lower angle accompanied by the increased interlayer spacing ( $d_{(003)}$ ), suggesting intercalation of  $PO_4^{3-}$  with larger ion radius than  $Cl^-$  into the interlayer, resulting in the enlarged interlamellar space [38]. After the granulation process, BLDH-P showed a similar XRD pattern to LiAl-LDH-P powder, indicating that binders were adequately mixed and crystal structure of resultant bead was unaffected.



**Figure 4.7** XRD patterns of LiAl-LDH-Cl powder, LiAl-LDH-P powder and BLDH-P bead.

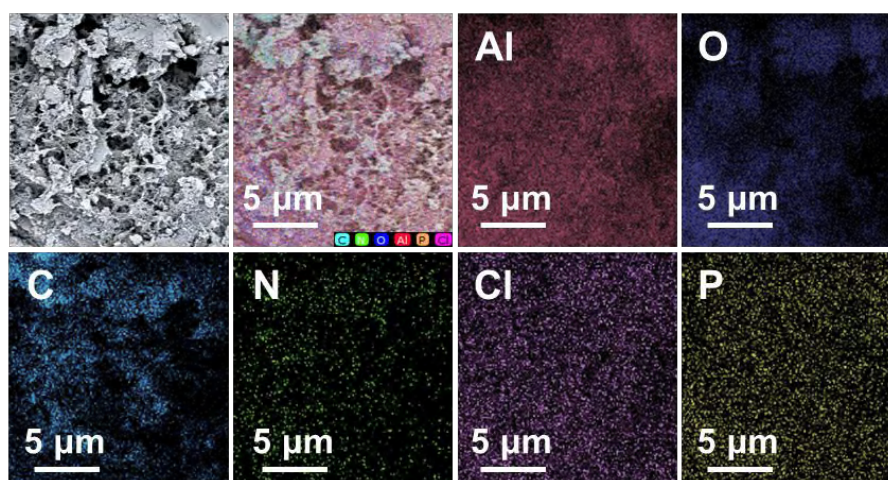
Further, the Fourier transform infrared (FT-IR) spectra of samples were exhibited

in Figure 4.8, where beside P=O ( $1025\text{ cm}^{-1}$ ), Al-O ( $530$  and  $943\text{ cm}^{-1}$ ), and O-H assigned to  $\text{PO}_4^{3-}$  and LDH [19,39], respectively, BLDH-P showed both PVC- and PAN- (including C≡N, C-H) related functional groups [40], proving the successful preparation of BLDH-P beads.



**Figure 4.8** FT-IR spectra of PVC, PAN and BLDH-P bead.

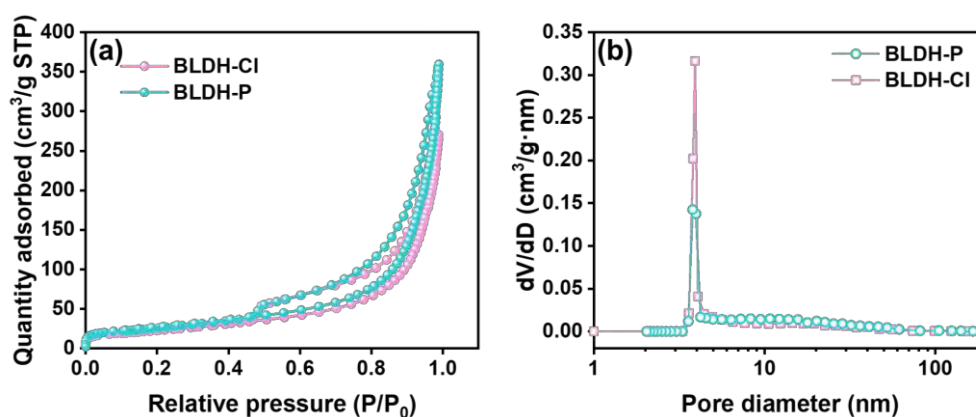
Scanning electron microscope (SEM) image and energy dispersive spectroscopy (EDS) mapping images of BLDH-P also confirmed the coexistence of LiAl-LDH-P, PVC and PAN in BLDH-P, in which Al, O, P, C, N, Cl elements homogeneously distributed throughout internal structure of beads (Figure 4.9). From the SEM image, BLDH-P consisted of organic 3D net-framework with numerous mesopores and embedded LiAl-LDH-P powders. Such structure ensured excellent stability and multiple  $\text{Li}^+$  diffusion channels, facilitating the Li extraction from brines.



**Figure 4.9** SEM images and EDS mapping images of BLDH-P internal.

The textural properties of adsorbents were investigated by  $\text{N}_2$  adsorption-

desorption isotherms in detail (Figure 4.10a). Obviously, both BLDH-P and BLDH-Cl showed type IV isotherms with a hysteresis of H3 type, demonstrating the mesoporous structure [41], which was substantiated by the results of pore size analyses (Table 4.2 and Figure 4.10b). Importantly, the BET specific surface area (SSA) and pore volume of BLDH-P were markedly higher than these of BLDH-Cl, being conducive to the  $\text{Li}^+$  diffusion and adsorption.

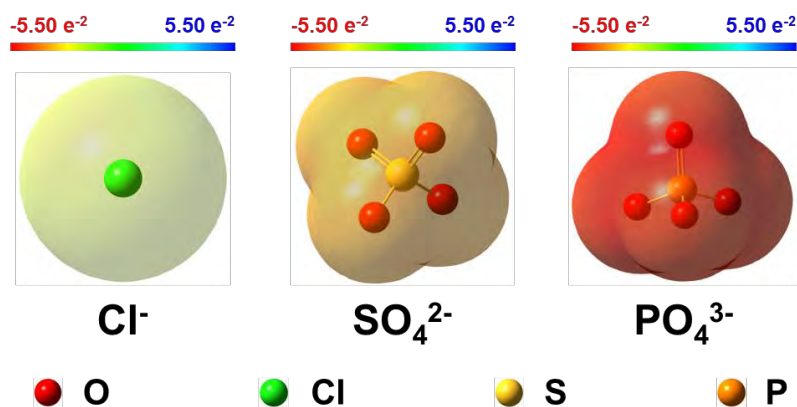


**Figure 4.10** (a) Nitrogen adsorption-desorption isotherms, and (b) pore size distributions of BLDH-Cl and BLDH-P bead.

**Table 4.2** The textural properties of BLDH-P and BLDH-Cl.

Samples	Specific surface area ( $\text{m}^2 \cdot \text{g}^{-1}$ )	Total pore volume ( $\text{cm}^3 \cdot \text{g}^{-1}$ )	Mean pore diameter (nm)
BLDH-Cl	105.6	0.4568	18.49
BLDH-P	146.00	1.0487	15.23

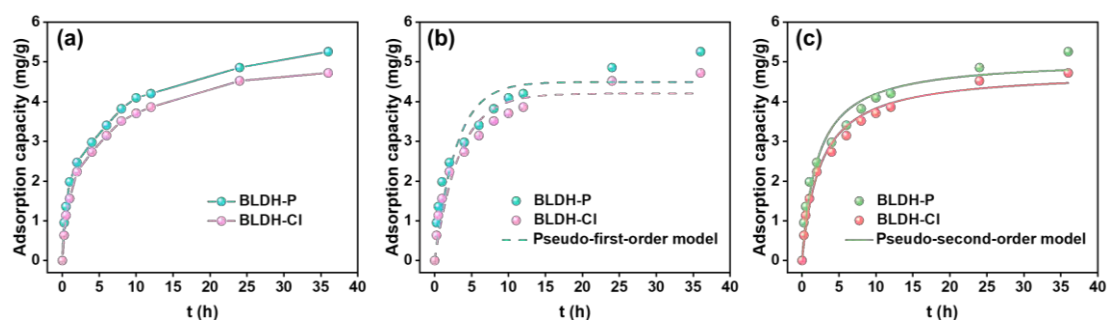
To estimate the potential of BLDH-P for preventing intercalation of  $\text{SO}_4^{2-}$ , the  $\text{Cl}^-$ ,  $\text{SO}_4^{2-}$  and  $\text{PO}_4^{3-}$  were employed as models and density functional theory (DFT) calculations of electrostatic potential (ESP) distributions were conducted. As shown in Figure 4.11, the entire frames of all anions presented negative charges, and as the anion charge raised, the region with negative electrostatic potential was more concentrated (redder in color). Specifically, although both  $\text{Cl}^-$  and  $\text{PO}_4^{3-}$  had negative ESP, the latter exhibited more negative electrostatic potential, which might induce the stronger electrostatic repulsion between interlayered anions and  $\text{SO}_4^{2-}$  in brines [42], thus hindering the intercalation of  $\text{SO}_4^{2-}$ , and facilitating the long-term extraction of  $\text{Li}^+$  from sulfate-type brines by LiAl-LDH.



**Figure 4.11** ESP distributions of  $\text{Cl}^-$ ,  $\text{SO}_4^{2-}$ ,  $\text{PO}_4^{3-}$  and their solvation energies.

### 4.3.3. Lithium extraction performance in sulfate-type brines

**Static lithium extraction:** To determine the suitability of BLDH-P in sulfate-type brines, the multiple cycle static Li extraction experiments with adsorption, desorption and re-adsorption were carried out in Lop Nor brine. As shown in Figure 4.12a, the adsorption capacities of both BLDH-P and BLDH-Cl rapidly increased in the first 8 h, then followed by slow adsorption rates until reaching equilibrium within 36 h. It was worth noting that BLDH-P exhibited a higher  $\text{Li}^+$  adsorption capacity (5.26 mg/g) than BLDH-Cl (4.72 mg/g), which might be attributed to the higher SSA and interlayer spacing, promoting the  $\text{Li}^+$  transfer and diffusion in adsorbent bead [43]. Moreover, the kinetic characteristics of extraction processes were investigated (Figure 4.12b-c and Table 4.3), where both adsorption kinetics fitted well the pseudo-second-order kinetic model according to the analysis of correlation coefficient ( $R^2$ ), indicating that the chemical adsorption was the dominated during extraction processes [44,45]. In addition, the higher rate constant ( $k_2$ ) proved the stronger driven force of BLDH-P for Li extraction than BLDH-Cl.

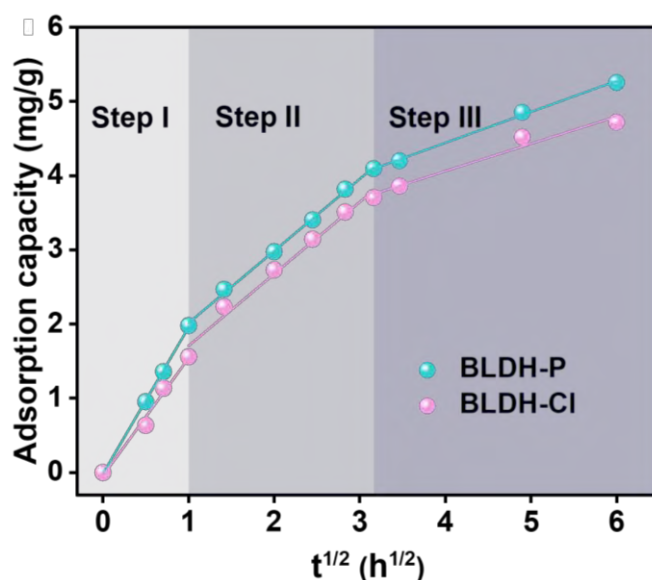


**Figure 4.12** (a) Adsorption kinetics of  $\text{Li}^+$  on BLDH-P and BLDH-Cl during the adsorption process. (b) The pseudo-first-order and (c) pseudo-second-order kinetic models of the BLDH-P and BLDH-Cl.

**Table 4.3** Kinetic model parameters of BLDH-P and BLDH-Cl.

Samples	Pseudo-first-order			Pseudo-second-order		
	$q_e$ (mg/g)	$k_1$ ( $\text{min}^{-1}$ )	$R^2$	$q_e$ (mg/g)	$k_2$ ( $\text{g}/(\text{mg}\cdot\text{min})$ )	$R^2$
BLDH-P	4.49	0.35	0.9088	5.07	0.094	0.9658
BLDH-Cl	4.20	0.30	0.9415	4.77	0.084	0.9831

The intraparticle diffusion model were further used to analyzed the adsorption process (Figure 4.13). The Li extraction on adsorbents could be divided into three major steps, involving fast  $\text{Li}^+$  surface adsorption from brine to the adsorbents interface,  $\text{Li}^+$  transfer into octahedral voids of  $\text{LiAl-LDH}$ , and  $\text{Li}^+$  internal diffusion [46]. To speak of, all three steps of BLDH-P showed faster rates than these of BLDH-Cl (Table 4.4), in consistence with the results of kinetics.



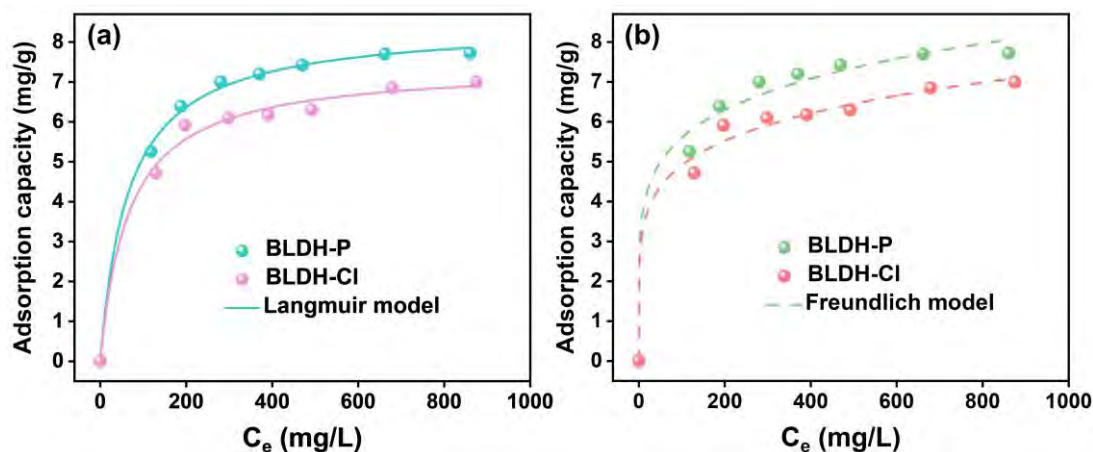
**Figure 4.13** The intraparticle diffusion model of  $\text{Li}^+$  on BLDH-P and BLDH-Cl during the adsorption process.

**Table 4.4** The intraparticle diffusion model calculated parameters for the adsorption of  $\text{Li}^+$  on samples.

Samples	$k_{p1}$	$C_1$	$R^2_1$	$k_{p2}$	$C_2$	$R^2_2$	$k_{p3}$	$C_3$	$R^2_3$
BLDH-P	1.97	-0.01	0.9990	0.97	1.05	0.9978	0.42	2.77	0.9963
BLDH-Cl	1.58	-0.04	0.9794	0.96	0.74	0.9803	0.37	2.59	0.9496

To in-depth investigate the Li extraction performance, adsorption isotherms were also estimated (Figure 4.14 and Table 4.5). One can see that adsorption processes of

both adsorbents agree better with the Langmuir model, suggesting that Li extraction was close to monolayer adsorption [47]. The theoretical maximum uptake from Langmuir model was as high as 8.46 mg/g.

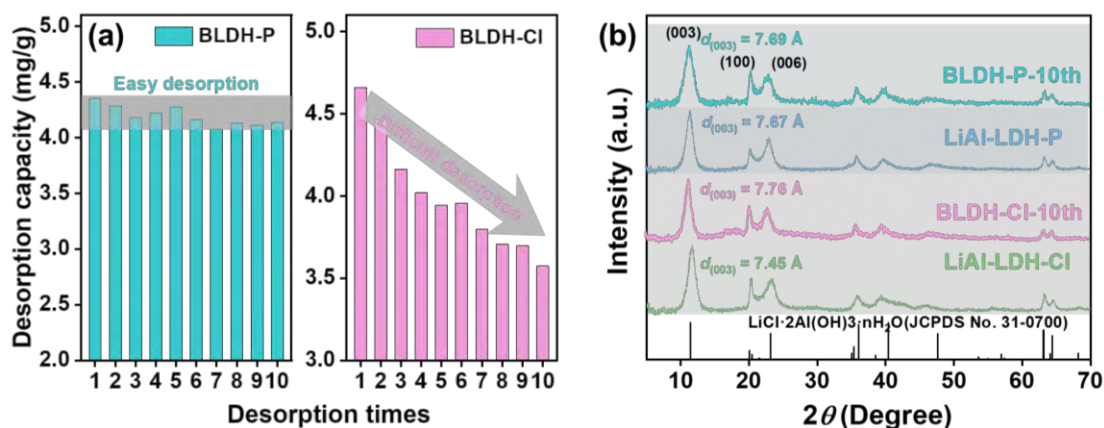


**Figure 4.14** (a) Langmuir and (b) Freundlich isotherm models of BLDH-P and BLDH-Cl.

**Table 4.5** Adsorption isotherm models parameters of BLDH-P and BLDH-Cl.

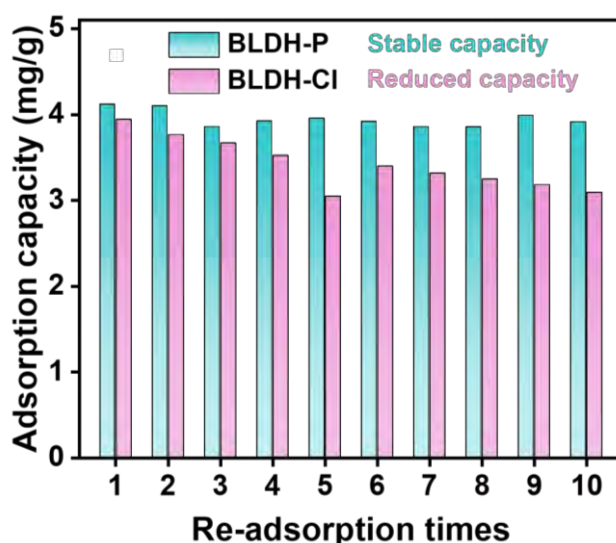
Samples	Langmuir			Freundlich		
	$q_m$ (mg/g)	$K_L$ (L/mg)	$R^2$	$K_F$ (mg/g) (L/mg) <sup>1/n</sup>	$n_F$	$R^2$
BLDH-P	8.46	0.0152	0.9926	2.58	5.93	0.9878
BLDH-Cl	7.42	0.0150	0.9913	2.25	5.91	0.9890

Next, the continuous desorption procedure was performed. Encouragingly, the desorption capacity of BLDH-P maintained stable level throughout ten desorption times (Figure 4.15a), revealing that the desorption is relatively easy for BLDH-P. In contrast, BLDH-Cl presented a gradual decrease in the desorption capacity. Based on previous research, such phenomena might derive from the accumulation of  $\text{SO}_4^{2-}$ , which had a strong electrostatic attraction with positively charged laminates in interlayer of LiAl-LDH, causing the difficulty of  $\text{SO}_4^{2-}$  and  $\text{Li}^+$  desorption [13]. The accumulation of  $\text{SO}_4^{2-}$  was proved by the results of XRD patterns (Figure 4.15b), where the  $d_{(003)}$  of BLDH-Cl enlarged from 7.45 Å to 7.65 Å after ten adsorption-desorption cycles, indicating the intercalation of  $\text{SO}_4^{2-}$  from the brine into BLDH-Cl [27]. While the structure of BLDH-P remained virtually unchanged for ten cycles, in agreement with the results of desorption capacity, suggesting that BLDH-P might repel  $\text{SO}_4^{2-}$  via interlayered  $\text{PO}_4^{3-}$ .



**Figure 4.15** (a) Desorption capacities of BLDH-P and BLDH-Cl during ten desorption cycles. (b) The XRD patterns of LiAl-LDH-Cl powder, BLDH-Cl and BLDH-P after ten adsorption-desorption cycles.

In order to evaluate the long-term suitability of BLDH-P, the continuous re-adsorption procedure was also conducted in Lop Nor brine (Figure 4.16). As expected, the uptake of desorbed BLDH-P still maintained a high level ( $\sim 4.1$  mg/g) in ten re-adsorption cycles, while the re-adsorption capacity of BLDH-Cl showed a reduced Li extraction performance, which was in line with the results of desorption process. Owing to the strong interaction between  $\text{SO}_4^{2-}$  and LiAl-LDH laminates,  $\text{Li}^+$  can be anchored into the octahedral voids during the desorption process, leading that the limited adsorption sites were released, hindering the  $\text{Li}^+$  re-adsorption. Intriguingly, intercalated  $\text{PO}_4^{3-}$  can inhibit the intercalation of  $\text{SO}_4^{2-}$  into interlayer of LiAl-LDH, endowing BLDH-P with stable capacity.



**Figure 4.16** Adsorption capacities of BLDH-P and BLDH-Cl during ten cycles.

The selectivity of lithium adsorbent is crucial for Li extraction and recovery from salt lake brines, consisting of ultrahigh concentration  $K^+$ ,  $Na^+$ , and  $Mg^{2+}$ . Figure 4.17 showed that BLDH-P realized the higher  $Li^+$  selectivity compared with BLDH-Cl, and the separation factors of  $Li^+/K^+$ ,  $Li^+/Na^+$ , and  $Li^+/Mg^{2+}$  reached 39.84, 48.14, and 144.87, demonstrating the extraordinary practical applicability of BLDH-P.

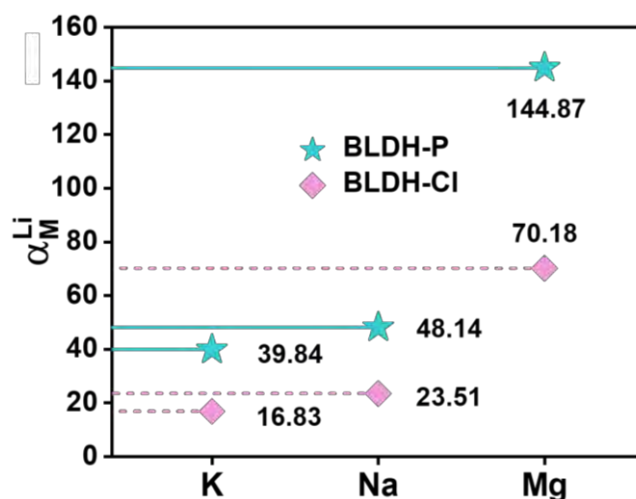


Figure 4.17 The selectivity of BLDH-P and BLDH-Cl.

**Continuous column extraction:** To assess the application prospect of BLDH-P in  $SO_4^{2-}$ -type brine, a facile fixed bed column adsorption device was developed. A continuous flow of Lop Nor brine through a column packed with BLDH-Cl or BLDH-P beads, as shown in Figure 4.18a. The results of  $Li^+$  breakthrough curves presented a stable and long-term process of 12.4 bed volume (BV) for BLDH-P, which was well superior than that of BLDH-Cl (9.0 BV) (Figure 4.18b). At the same time, the total  $Li^+$  adsorption capacity of BLDH-P was as high as 3.96 mg/g (Figure 4.18c).

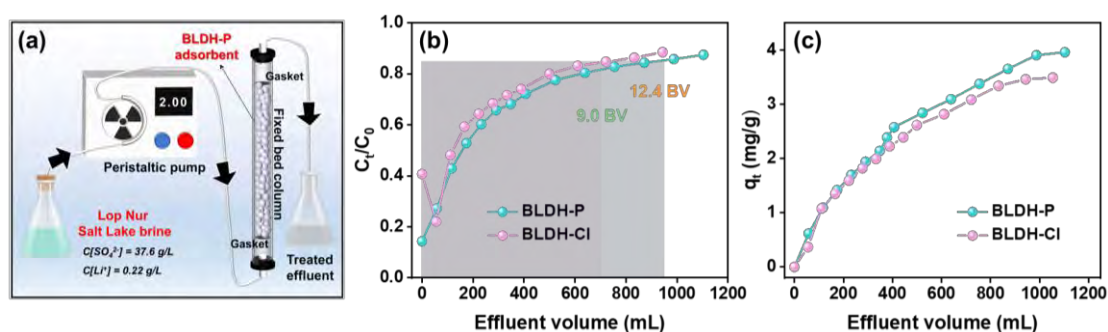
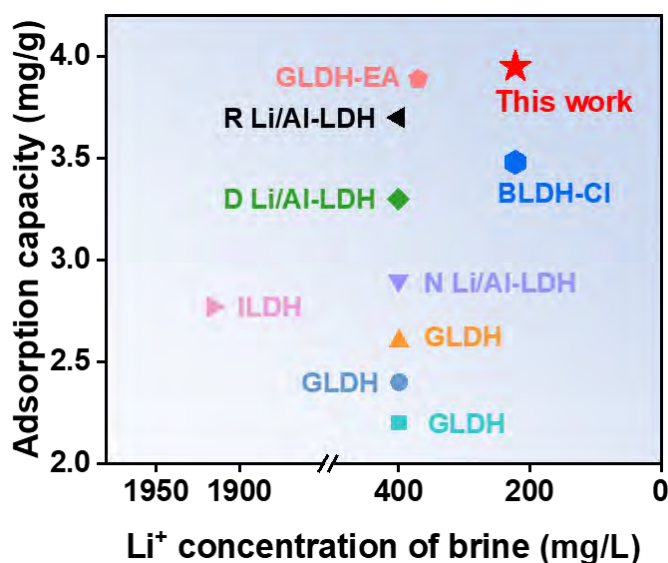


Figure 4.18 (a) Schematic illustration of the fixed bed column device. (b) The  $Li^+$  breakthrough curves and (c) the  $Li^+$  adsorption curves of BLDH-Cl and BLDH-P.

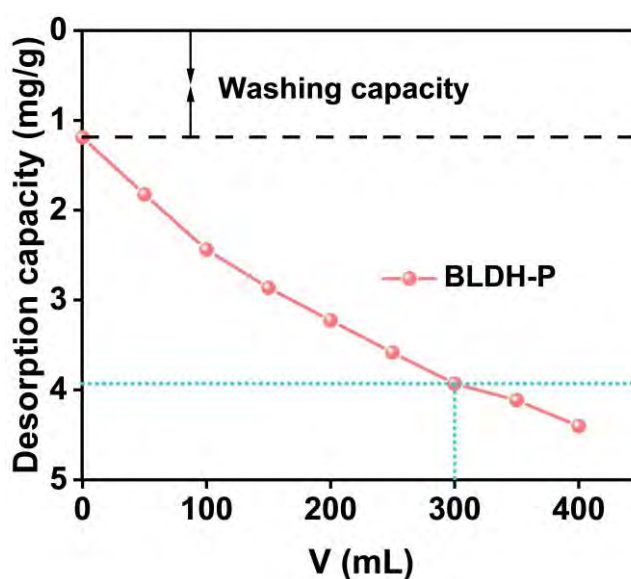
Such exceptional dynamic uptake in brine with low  $Li^+$  concentration exceeded

most of the granulated LiAl-LDH adsorbents previously reported (Figure 4.19), demonstrating the extraordinary lithium extraction performance and strong adsorption drive.



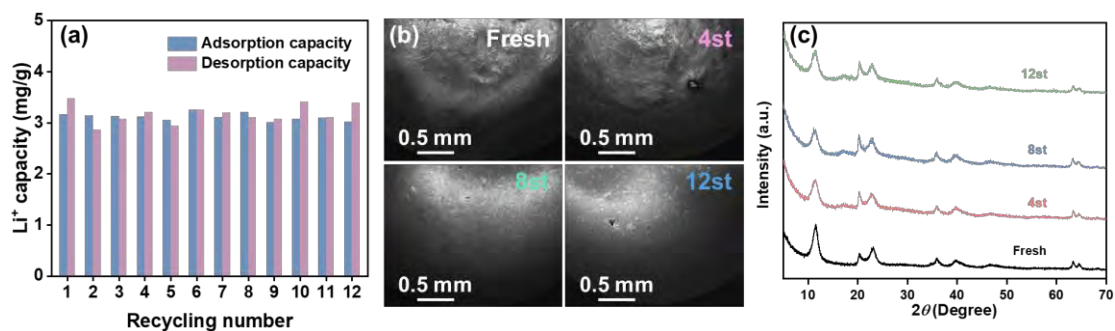
**Figure 4.19** Comparison of  $\text{Li}^+$  dynamic extraction properties of different LiAl-LDHs.

Moreover, considering the crucial significance of the adsorbents' reusability for large-scale application in practical Li extraction from brines, the consecutive dynamic  $\text{Li}^+$  adsorption and desorption cycles were performed. Based on the results of dynamic adsorption (Figure 4.18b) and desorption (Figure 4.20), the volume of pumped brine was set to 1200 mL, and the volume of deionized water was set to 300 mL.



**Figure 4.20** The dynamic desorption capacity of BLDH-P in fixed bed.

As exhibited in Figure 4.21a, the both dynamic adsorption capacity and desorption capacity maintained stable levels during 12 cycling process. Meanwhile, the surface of BLDH-P exhibited no cracks and the structure remained unchanged during the entire continuous extraction process (Figure 4.21b-c), suggesting the excellent reusability and advancement of BLDH-P.

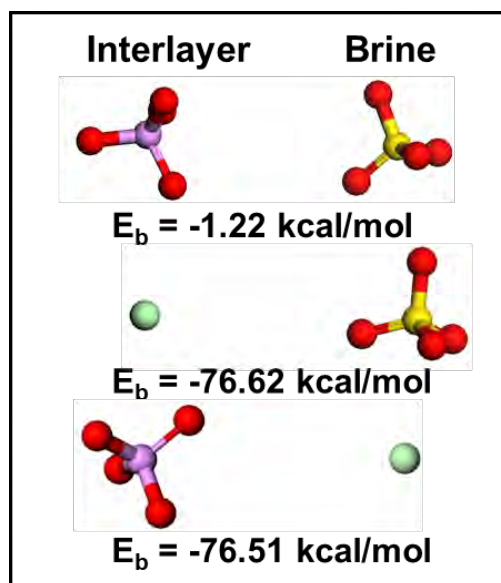


**Figure 4.21** (a) The dynamic adsorption-desorption cycling adsorption performance of BLDH-P. (b) SEM images and (c) XRD patterns of BLDH-P after different cycling numbers

#### 4.3.4. Mechanisms of stable extraction in sulfate-type brines

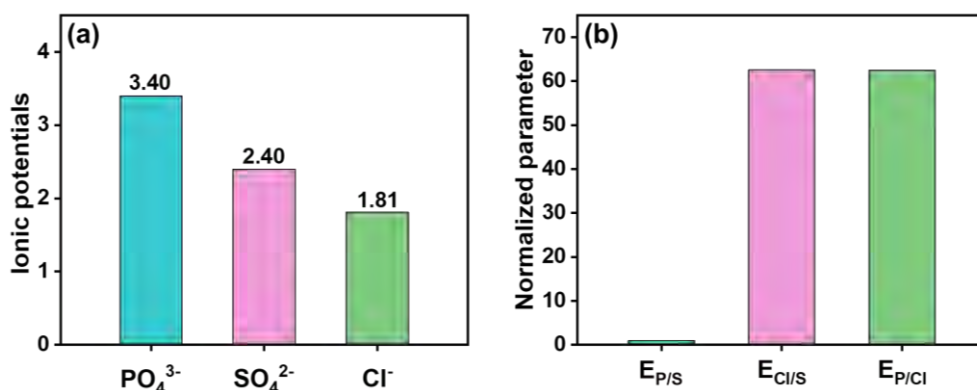
The preceding experiments have stated that BLDH-P bead possesses the property for preventing intercalation of  $\text{SO}_4^{2-}$  into LiAl-LDH interlayer, which results from the stronger electrostatic repulsion between  $\text{PO}_4^{3-}$  and  $\text{SO}_4^{2-}$ . The insights into the interaction mechanisms, however, still remain unclear. To this end, the DFT calculations were carried out to simulate the ions specific interactions and the processes of LiCl and  $\text{Li}_2\text{SO}_4$  capture by LiAl-LDH intercalated with  $\text{PO}_4^{3-}$  or  $\text{Cl}^-$ . The electrostatic interaction might obviously affect the interaction between interlayered anions (i.e.,  $\text{PO}_4^{3-}$  or  $\text{Cl}^-$ ) and  $\text{SO}_4^{2-}$  in brines, further impacting the intercalation behaviors of  $\text{SO}_4^{2-}$ . Herein, the binding energy ( $E_b$ ) was used to evaluate the insertion resistance of  $\text{SO}_4^{2-}$  into the interlayer of LiAl-LDH, where the higher  $E_b$ , the stronger interaction, the easier insertion of anion in brines [48]. As shown in the Figure 4.22, the  $E_b$  between  $\text{Cl}^-$  and  $\text{SO}_4^{2-}$  ( $E_{\text{Cl/S}}$ ) was as high as -76.62 kcal/mol, while the  $E_b$  between  $\text{PO}_4^{3-}$  and  $\text{SO}_4^{2-}$  ( $E_{\text{P/S}}$ ) was only -1.22 kcal/mol. Such calculation results indicated that common  $\text{Cl}^-$  tends to combine with  $\text{SO}_4^{2-}$ , inducing more  $\text{SO}_4^{2-}$  inserting into the interlayer of LiAl-LDH-Cl. Nevertheless, it is difficult for  $\text{SO}_4^{2-}$  to bind with  $\text{PO}_4^{3-}$  according to the low  $E_{\text{P/S}}$ . At the same time, it can be found that the  $E_b$  between  $\text{PO}_4^{3-}$  and  $\text{Cl}^-$  ( $E_{\text{P/Cl}}$ ) increased to -76.51 kcal/mol, which suggested that Li extraction by LiAl-LDH-P favors being accompanied by the intercalation of  $\text{Cl}^-$  to balance the charge

instead of  $\text{SO}_4^{2-}$  in sulfate-type brine.



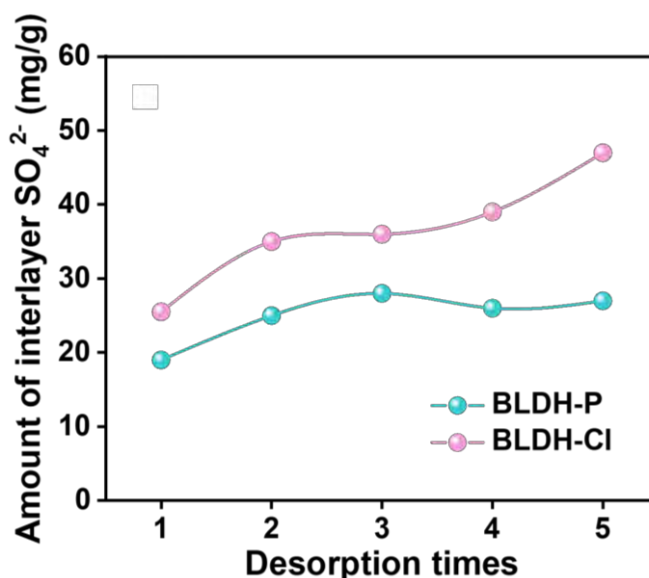
**Figure 4.22** The optimized anion structure and binding energy between anions.

Although the highly negative electric field of  $\text{PO}_4^{3-}$  could induce electrostatic repulsion for both  $\text{Cl}^-$  and  $\text{SO}_4^{2-}$ , the former presented the smaller ionic potential (1.81) than that of the latter (2.40) (Figure 4.23a), demonstrating the lower electrostatic repulsion [49]. Additionally, the interlayer of LiAl-LDH-P consisted of  $\text{PO}_4^{3-}$  and  $\text{Cl}^-$ , that is, the adsorbent had a specific affinity for  $\text{Cl}^-$  due to memory effect [3]. Thus, LiAl-LDH-P featured a selective electrostatic interaction, allowing the  $\text{Cl}^-$  to overcome the electrostatic repulsion to achieve a smooth intercalation process. To better visualize the intercalation disparity, a normalized parameter of  $\text{NP} = E_b / E_{p/s}$  was defined. The results of the  $E_{\text{Cl/S}}$  NP indicated that the selectivity of  $\text{SO}_4^{2-}/\text{Cl}^-$  insertion into LiAl-LDH-P was the 62.57 (Figure 4.23b).



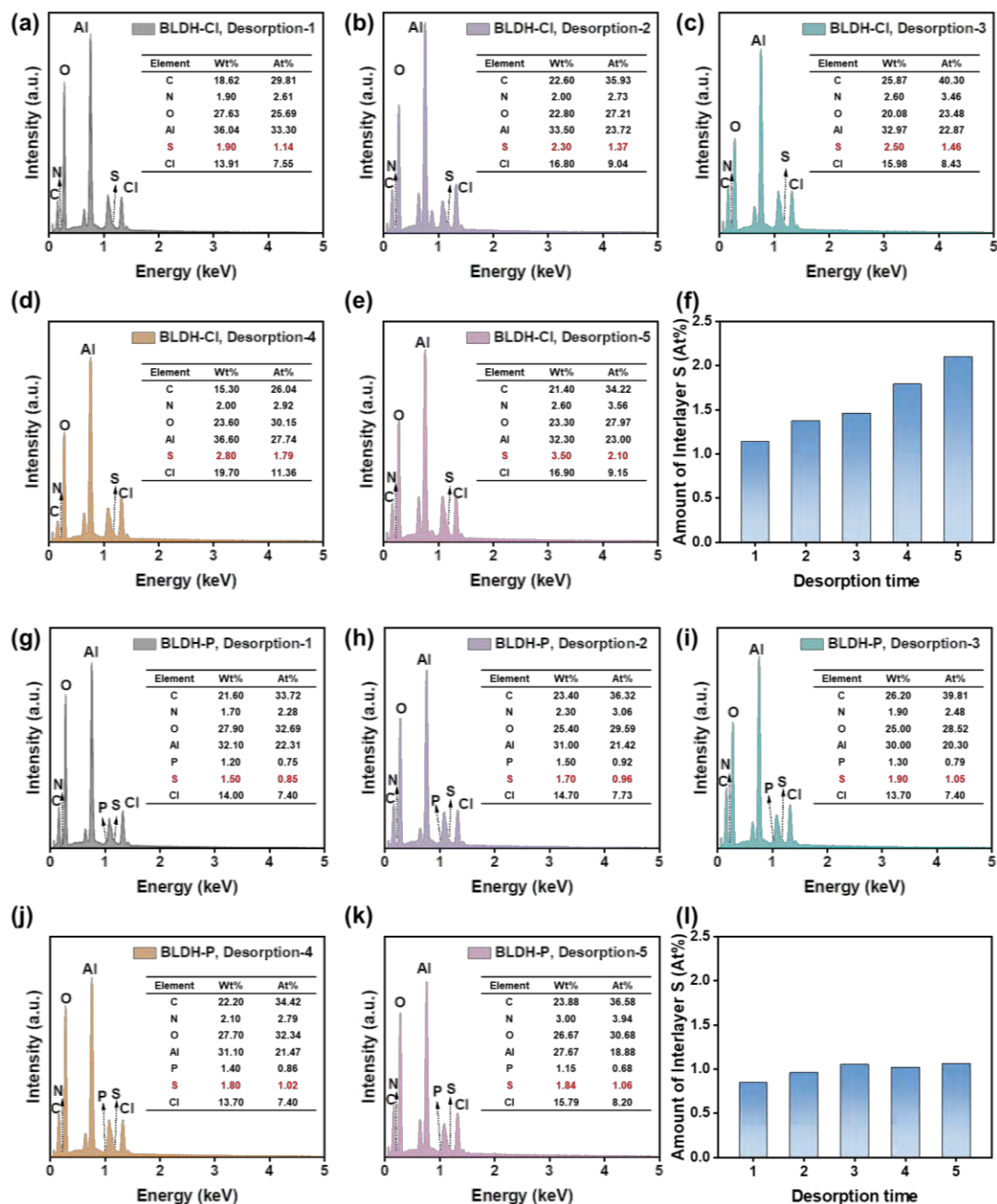
**Figure 4.23** (a) Ionic potentials of different anions. (b) Quantitative diagram of anion interaction disparity.

Furthermore, interlayer  $\text{SO}_4^{2-}$  contents of BLDH-P and BLDH-Cl were determined as well (Figure 4.24). There was an upward trend in amount of interlayer  $\text{SO}_4^{2-}$  within BLDH-Cl after successive adsorption-desorption cycles. Whereas, the interlayer  $\text{SO}_4^{2-}$  amount of BLDH-P retained a low plateau, which might be due to the residual brine adhering to the bead, proving that  $\text{PO}_4^{3-}$  were capable of repelling  $\text{SO}_4^{2-}$  via stronger electrostatic repulsion.



**Figure 4.24** Amounts of interlayer  $\text{SO}_4^{2-}$  of BLDH-P and BLDH-Cl during five desorption cycles.

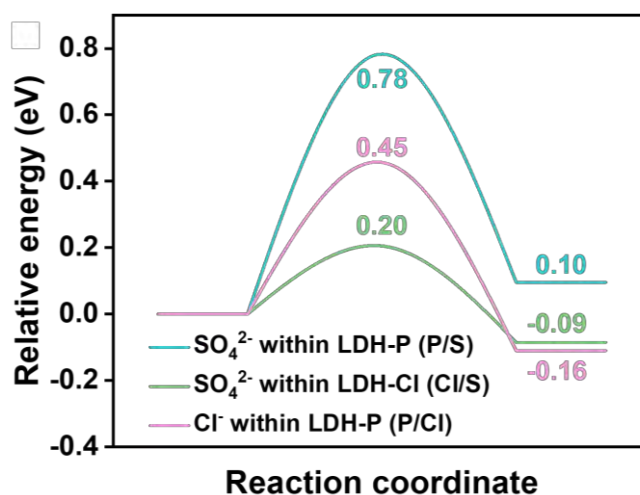
The EDS spectra of adsorbents after various desorption times realized similar trend in  $\text{SO}_4^{2-}$  amount as well (Figure 4.25). The facts that the low and stable  $\text{SO}_4^{2-}$  amount of BLDH-P provided solid proof for function of steering interlayer interaction strategy, i.e., prevention of  $\text{SO}_4^{2-}$  intercalation, in favor of the  $\text{Li}^+$  and  $\text{Cl}^-$  re-adsorption in sulfate-type brines.



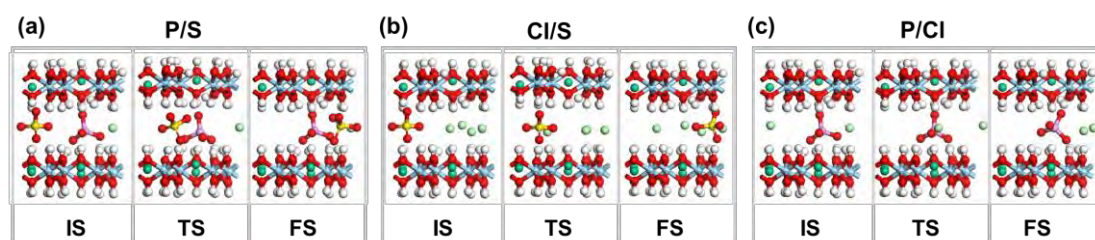
**Figure 4.25** (a-e) The EDS spectra of BLDH-Cl after various desorption times. (f) The amount of S element in BLDH-Cl from the results of EDS spectra. (g-k) The EDS spectra of BLDH-P after various desorption times. (l) The amount of S element in BLDH-P from the results of EDS spectra.

Considering that the insertion of brine anions and their diffusion into LiAl-LDH are not only affected by the interaction between ions, but also by the diffusion paths and the spatial confinement of interlayer nanostructures, the calculation of diffusion energy barriers of  $\text{Cl}^-$  and  $\text{SO}_4^{2-}$  within LiAl-LDH-P or LiAl-LDH-Cl (Figure 4.26) was performed. It can be found that the energy barrier of  $\text{SO}_4^{2-}$  within common LiAl-LDH-

Cl was only 0.20 eV, indicating that there is low resistance for  $\text{SO}_4^{2-}$  diffusion, in consistence with the result of previous research [27]. Encouragingly, such energy barrier in LiAl-LDH-P intercalated with phosphate ions increased to 0.78 eV, corroborating the difficult diffusion of  $\text{SO}_4^{2-}$  within LiAl-LDH-P [36]. Comparing with  $\text{SO}_4^{2-}$ , the diffusion activation energy of  $\text{Cl}^-$  within LiAl-LDH-P was 0.45 eV, suggesting that for LiAl-LDH-P in brine with high concentration  $\text{SO}_4^{2-}$  and  $\text{Cl}^-$ , the  $\text{Cl}^-$  readily inserts into the interlayer and diffusion instead of  $\text{SO}_4^{2-}$ , preventing the reduction of  $\text{Li}^+$  adsorption capacity derived from the tough desorption. Figure 4.27 exhibited the structures of initial state (IS), transition state (TS) and final state (FS) configurations for anion diffusion reaction within adsorbents.



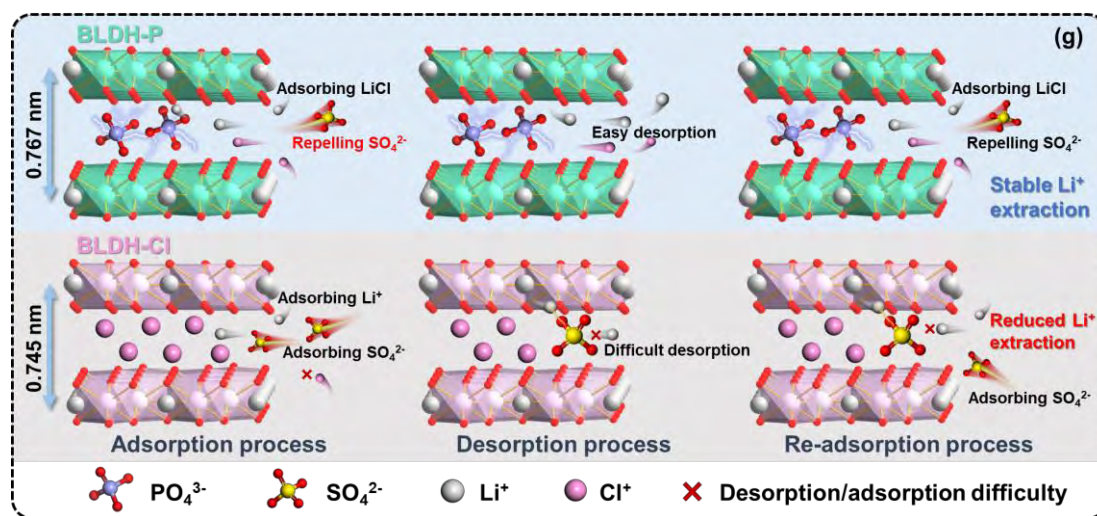
**Figure 4.26** Relative energies for the diffusion of  $\text{SO}_4^{2-}$  and  $\text{Cl}^-$  within LiAl-LDH-P or LiAl-LDH-Cl.



**Figure 4.27** Optimized structures of initial state, transition state and final state configurations for  $\text{SO}_4^{2-}/\text{Cl}^-$  diffusion reaction within LiAl-LDH-P or LiAl-LDH-Cl.

Based on the above data and discussion, the functional mechanisms of  $\text{PO}_4^{3-}$  intercalation steering interlayer interaction strategy were schematically illustrated in Figure 4.28. Benefiting from the expansion of the interlayer spacing and the inhibition of  $\text{SO}_4^{2-}$  intercalation due to enhanced electrostatic repulsion as well as raised the

diffusion energy barrier within interlayers, BLDH-P was imparted with long-lasting excellent  $\text{Li}^+$  adsorption capacity and selectivity in brines with ultrahigh concentrations of impurity cations and  $\text{SO}_4^{2-}$ .



**Figure 4.28** Schematic illustration of adsorption, desorption and re-adsorption processes of BLDH-P and BLDH-Cl.

#### 4.4. Conclusions

In summary, a steering interlayer interaction strategy was proposed to improve the feasibility of  $\text{LiAl-LDH-Cl}$  in lithium extraction from  $\text{SO}_4^{2-}$ -type brines. The prepared BLDH-P beads intercalated with phosphate ions showed well mechanical properties and outstanding Li extraction performance. Specifically, the static and dynamic  $\text{Li}^+$  adsorption capacity of BLDH-P reached 5.26 mg/g and 3.96 mg/g in Lop Nor brine, with high separation factors of 39.84, 48.14, and 144.87 for  $\text{Li}^+/\text{K}^+$ ,  $\text{Li}^+/\text{Na}^+$ , and  $\text{Li}^+/\text{Mg}^{2+}$ , respectively, outperforming the reported and commercialized  $\text{LiAl-LDH}$ . Moreover, BLDH-P were endowed with property for preventing  $\text{SO}_4^{2-}$  intercalation through strong electrostatic repulsion between interlayer  $\text{PO}_4^{3-}$  and  $\text{SO}_4^{2-}$  in brine, which was proved by DFT calculation. Unlike BLDH-Cl, BLDH-P therefore presented the stable desorption and re-adsorption ability and low amount of interlayer  $\text{SO}_4^{2-}$  in continuous desorption and re-adsorption procedure. As expected, BLDH-P demonstrated the excellent stability and reusability during 12 cycles of column extraction, revealing the application prospect. Overall, this work not only provides an efficient strategy for solving the actual dilemma of  $\text{LiAl-LDH}$  in long-term Li extraction from  $\text{SO}_4^{2-}$ -type brines, but also inspires the development and design of state-of-the-art LDHs.

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## Chapter 5. Constructing multiple functional domains of lithium aluminum layered double hydroxides for sustainable lithium extraction in sulfate-type brines

### 5.1. Introduction

Lithium (Li) is a critical element for the clean energy transition, for which the global demand is growing exponentially [1-3]. The sustainable supply of Li is, therefore, particularly urgent [4,5]. Currently, commercial Li is exclusively from high-grade Li ores and continental brines, with the latter being more abundant than the former [6,7]. The conventional evaporitic process used to concentrate and extract Li from continental brines is time-consuming, land-intensive, and negatively impacts local ecosystems [6,8-11]. What's more, the entrainment loss of Li readily occurs with the precipitation of co-dissolved elements (such as Na and K) during the evaporation process, causing Li yield of less than 40% of the overall, which entails a great waste of resources [12,13]. Moreover, the dramatic competing effects originated from the numerous impurity ions (especially  $Mg^{2+}$ ) usually requires to be surmounted to extract Li even from concentrated brines [14,15]. Thus, to secure the Li supply, it is required to explore more efficient avenues and expand accessible brine resources for lithium extraction.

Adsorption has widely applied to perform direct lithium extraction (DLE) from brines due to simple process and low energy consumption [16,17]. In particular, lithium-aluminum layered double hydroxides (LiAl-LDHs) are the most successful adsorbents for industrialized Li extraction owing to their unique octahedral cavity structure ( $\sim 1.4 \text{ \AA}$ ) matching the  $Li^+$  diameter and desorption without dissolution loss [18,19]. LiAl-LDHs are a class of two-dimensional laminated materials whose chemical formula is  $LiX \cdot 2Al(OH)_3 \cdot nH_2O$  [20]. During the Li extraction procedure,  $Li^+$  selectively intercalates into octahedral vacancies of  $Al(OH)_3$  to form positively charged host layers, accompanied by the charge-balancing anions (*i.e.*, X) and water molecules entering the interlayer [21,22]. In the case of Li recovery, the  $Li^+$  in the octahedral units and interlayer anions are readily deintercalated using water [18,23]. To date, LiAl-LDHs are only used in Cl<sup>-</sup>-type brines, which are limited in number. The industrialized Li extraction of LiAl-LDHs in  $SO_4^{2-}$ -type brines that are the second most significant

type of brines in the world, remains to be achieved, which suffers from the ‘SO<sub>4</sub><sup>2-</sup> poisoning’ effect. Specifically, SO<sub>4</sub><sup>2-</sup> readily intercalates into the interlayer of LiAl-LDHs, while it is challenging to be desorbed to release Li<sup>+</sup> adsorption sites due to the strong interlayer binding interaction, inducing the gradually reduced Li<sup>+</sup> adsorption capacity of LiAl-LDHs [24,25]. Such poisoning effect seriously hampers application diversification of LiAl-LDHs. To this end, the innovation and design of state-of-art LiAl-LDHs for sustainable Li extraction from SO<sub>4</sub><sup>2-</sup>-type brines are imperative.

The strategy of steering interlayer interaction by PO<sub>4</sub><sup>3-</sup> has been proposed to realize lithium extraction of LiAl-LDHs from SO<sub>4</sub><sup>2-</sup>-type brines, while PO<sub>4</sub><sup>3-</sup> may be gradually replaced by other anions during long-term cycling. What’s more, it is also difficult to avoid progressive poisoning due to gradual diffusion of SO<sub>4</sub><sup>2-</sup> into the LiAl-LDHs by regulating only the interlayer interactions. Herein, a novel organic modification strategy of constructing multiple functional domains of LiAl-LDHs using polyacrylamide (PAM) was proposed for sustainable lithium extraction in SO<sub>4</sub><sup>2-</sup>-type brines. Leveraging the enriched hydroxyl groups on the interface and ion exchange feature of LiAl-LDHs, part of the PAM was connected to the surface by hydrogen bonds, and the rest was intercalated into the LiAl-LDH interlayer to form multiple SO<sub>4</sub><sup>2-</sup> repelling domains. Benefiting from the rational design, the LiAl-LDHs modified with PAM (LiAl-LDH/PAM) offered excellent Li<sup>+</sup> selectivity, extraordinary anti-sulfate poisoning property, and the adsorption capacity of up to 13.25 mg g<sup>-1</sup> in the real SO<sub>4</sub><sup>2-</sup>-type brine. The strategy significantly enables the feasibility of long-term Li extraction by LiAl-LDHs from SO<sub>4</sub><sup>2-</sup>-type brines, significantly expanding the availability of Li resources.

## 5.2. Experimental section

### 5.2.1. Reagents and materials

Lithium chloride (LiCl), aluminum chloride hexahydrate (AlCl<sub>3</sub>·6H<sub>2</sub>O), sodium hydroxide (NaOH), and polyacrylamide (PAM) were purchased from Shanghai Aladdin Biochemical Technology Co., Ltd. All reagents are analytical grade.

The brine used in the experiments is the real Lop Nor Salt-Lake brine, the largest SO<sub>4</sub><sup>2-</sup>-type brine in the world. The detailed compositions were summarized in Table 5.1.

**Table 5.1** Properties of Lop Nor brine before and after static extraction.

Li <sup>+</sup> (g/L)	Mg <sup>2+</sup> (g/L)	K <sup>+</sup> (g/L)	Na <sup>+</sup> (g/L)	Cl <sup>-</sup> (g/L)	SO <sub>4</sub> <sup>2-</sup> (g/L)
0.2222	97.015	2.549	2.899	222.400	37.600

### 5.2.2. Preparation of LiAl-LDH-PAM

A two-step co-precipitation-activation modification method to ensure the negligible influence on the structure of LiAl-LDHs from the PAM introduction. First, LiAl-LDH precursors were prepared using the common co-precipitation method. Briefly, a mixed solution containing LiCl and  $\text{AlCl}_3 \cdot 6\text{H}_2\text{O}$  was dropped into a NaOH solution ( $8 \text{ mol L}^{-1}$ ) until the pH of the mixture was below 5. The resultant precipitates were dried and collected to obtain LiAl-LDH precursors. For inserting PAM without structural damage, a one-step activation-modification method was proposed. Specifically, the PAM solution with 0.1% concentration were prepared, and LiAl-LDH precursors were added to the above solutions (liquid-solid ratio of  $100 \text{ mL g}^{-1}$ ). After shaking in an air bath at  $40 \text{ }^\circ\text{C}$  for 2 h, centrifugation and freeze-drying were performed to complete the desorption-activation and organic modification processes simultaneously. The as-obtained samples were abbreviated as LiAl-LDH/PAM.

For comparison, the pristine LiAl-LDH were also prepared using the same method but with deionized water for desorption-activation.

### 5.2.3. Characterizations

Transmission electron microscope (TEM, JEM-JEOL-2100) equipped with energy dispersive spectroscopy (EDS) system was used to characterize the morphological structures of the samples. X-ray diffraction patterns were recorded using a Bruker diffractometer (XRD, Empyrean) with  $\text{Cu K}\alpha$  irradiation (40 kV, 100 mA). The surface potentials of the samples were tested using a zeta potential analyzer (Malvern Zetasizer Nano ZS90 zeta). Raman spectra were performed using a LabRAM Odyssey Raman microscope in 532 nm laser excitation. X-ray photoelectron spectra (XPS) were determined by a Thermo Scientific K-Alpha spectrometer.

### 5.2.4. Lithium-ion extraction

All batch adsorption experiments carried out in a water temperature-controlled shaker at room temperature. To determine the  $\text{Li}^+$  uptake, LiAl-LDHs were added into various real brines for 3 h, in which the liquid-solid ratio was  $50 \text{ mL g}^{-1}$ . The adsorption capacity  $q$  ( $\text{mg g}^{-1}$ ) was calculated by the Equation 5.1:

$$q = (C_0 - C_t)V/m \quad (5.1)$$

where  $C_0$  ( $\text{mg L}^{-1}$ ) and  $C_t$  ( $\text{mg L}^{-1}$ ) are the initial and residual ion concentrations, respectively;  $V$  (L) is the solution volume;  $m$  (g) refers the mass of LiAl-LDHs.

The desorption procedure involved two processes, that is, the rapid washing using a little ice deionized water for removing the residual brine on the sample surface and  $\text{Li}^+$  deintercalation using deionized water with a liquid-solid ratio of  $100 \text{ mL g}^{-1}$  at  $40^\circ\text{C}$  for 2h. The desorption capacity was determined by the Equation 5.2:

$$q = C_{\text{dt}}V/m \quad (5.2)$$

where  $q$  ( $\text{mg g}^{-1}$ ) and  $C_{\text{dt}}$  ( $\text{mg L}^{-1}$ ) represent the desorption capacity and concentration.

The distribution coefficient  $K_d$  ( $\text{mL g}^{-1}$ ) and separation coefficient  $\alpha_M^{\text{Li}}$  were determined to assess the adsorption selectivity of samples to different cations in brines according to the Equation 5.3-5.4:

$$K_d = V(C_0 - C_e)/(mC_e) \quad (5.3)$$

$$\alpha_M^{\text{Li}} = K_{d, \text{Li}}/K_{d, \text{M}} \quad (5.4)$$

where M represents cations in brines, involving  $\text{K}^+$ ,  $\text{Na}^+$ , and  $\text{Mg}^{2+}$ .

The adsorption-desorption cycling experiments were conducted in Lop Nur Salt-Lake brine, where the liquid-solid ratio remained consistent with those in batch adsorption and desorption experiments.

### 5.2.5. Theoretical calculations

All density functional theory (DFT) calculations were performed through the Materials Studio 8.0 software. The exchange-correlation interactions were described by the generalized gradient approximation of Perdew-Burke-Ernzerhof (GGA-PBE) for structural optimization to minimize the energy. The cut-off energy was set to  $570.0 \text{ eV}$ , and the convergence criteria for displacement, energy, and force were  $0.001 \text{ \AA}$ ,  $1 \times 10^{-5} \text{ eV/atom}$ , and  $0.03 \text{ eV/\AA}$ , respectively. Considering to the actual system, the transport pathway of  $\text{SO}_4^{2-}$  was divided into migration over interface and diffusion over interlayer of LiAl-LDHs. The relative energy barrier of  $\text{SO}_4^{2-}$  transport was calculated from the difference between the energy at the optimal adsorption site and the energy at specified position. Similarly, binding energies ( $E_b$ ) between ions and PAM were calculated by:

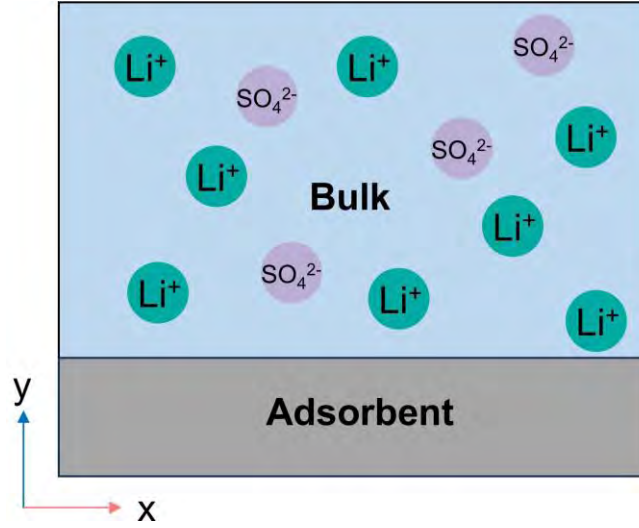
$$E_b = E_{A/B} - E_A - E_B \quad (5.5)$$

where  $E_{A/B}$  is the total energy of A and B bonded system;  $E_A$  and  $E_B$  indicate the energies of individual A and B, respectively.

### 5.2.6. Numerical simulation

Numerical simulation was performed by using finite element package COMSOL

(version 5.6) Multiphysics. A simplified two-dimensional model was constructed to carry out the calculations (Figure 5.1), where the top represents the bulk phase of  $\text{Li}_2\text{SO}_4$  solution, and the bottom rectangle with a length of  $5\ \mu\text{m}$  and a width of  $1\ \mu\text{m}$  represents the layered LiAl-LDH adsorbent.



**Figure 5.1** Two-dimension model of LiAl-LDHs and bulk phase of  $\text{Li}_2\text{SO}_4$ .

“Transport of Diluted Species (tds)” and “Static Electricity (es)” modules were used to simulate the ions diffusion on the LiAl-LDH interface, and the mesh is controlled by the physical field to ensure accuracy. The Poisson-Nernst-Planck (PNP) model is consisted of the Poisson equation and a set of convective diffusion equations, the former determining the electrostatic potential caused by the moving ions and fixed charges, while the latter represents the ion diffusion induced by the solution concentration gradient and the electric field, as shown in Equations 5.6-5.8:

$$\nabla^2 \varphi = -\frac{F}{\varepsilon} \sum_i z_i c_i \quad (5.6)$$

$$J_i = D_i (\nabla c_i + \frac{z_i F c_i}{RT} \nabla \varphi) \quad (5.7)$$

$$\nabla \cdot J_i = 0 \quad (5.8)$$

where,  $\varphi$  (V) is the potential of the adsorbent;  $\varepsilon$  (F/m) refers dielectric constant;  $c_i$  ( $\text{mol m}^{-3}$ ),  $z_i$ , and  $D_i$  ( $\text{m}^2 \text{ s}^{-1}$ ) are the ion concentration, valence number, and diffusion coefficient of ion  $i$ , respectively;  $J_i$  ( $\text{mol m}^{-2} \text{ s}^{-1}$ ) is the ionic flux;  $F$  ( $\text{C mol}^{-1}$ ) represents Faraday constant;  $R$  ( $\text{J} \cdot \text{mol}^{-1} \text{ K}^{-1}$ ) and  $T$  (K) are the gas constant and absolute temperature, respectively. The  $\varphi$  is obtained as:

$$\nabla \cdot (-\varepsilon \nabla \varphi) = \sigma \quad (5.9)$$

where  $\sigma$  ( $\text{C m}^{-2}$ ) is the surface charge density, which be calculated based on the equation:

$$\sigma = \frac{\varepsilon\varepsilon_0\xi}{\lambda_D} \quad (5.10)$$

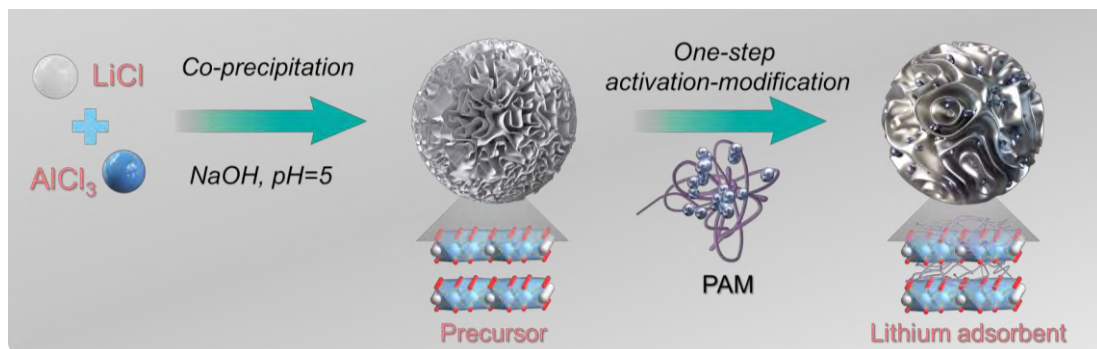
$$\lambda_D = \sqrt{\frac{(\varepsilon\varepsilon_0RT)}{(2n_{bulk}z^2F^2)}} \quad (5.11)$$

where  $\varepsilon_0$  (F/m) is vacuum dielectric constant and  $\xi$  (mV) is the zeta potential;  $\lambda_D$  represents the Debye length;  $n_{bulk}$  ( $\text{mol m}^{-3}$ ) indicates the concentration of bulk solution. Based on the determined results of zeta potential, the calculated values of pristine LiAl-LDH and LiAl-LDH/PAM are  $6.50 \times 10^{-3} \text{ C m}^{-2}$  and  $-4.17 \times 10^{-3} \text{ C m}^{-2}$ , respectively.

### 5.3. Results and discussion

#### 5.3.1. Synthesis and characterization

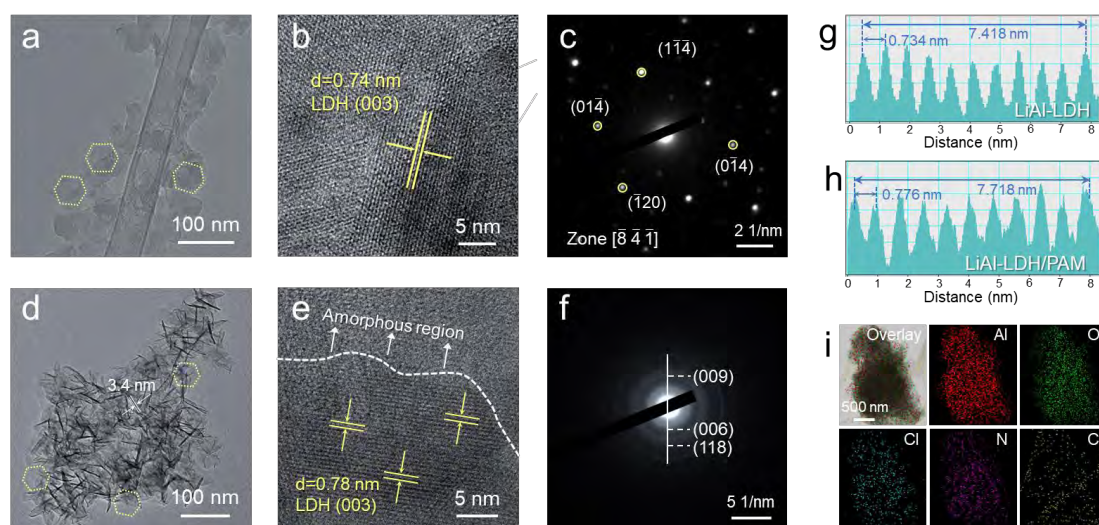
First, LiAl-LDH/PAM was prepared to evaluate the effects of the PAM on continuous Li recovery from sulfate-type brines. To speak of, the standard one-step co-precipitation method was not employed, based on the understanding of the properties of the structure of LiAl-LDHs, to shield that PAM impact the polarity and ionic concentration of the precursor slurry, which in turn affects the crystalline nucleation of Li/Al salts [18]. In contrast, a two-step co-precipitation-activation modification method was proposed to ensure the negligible influence on the structure of LiAl-LDHs from the PAM introduction, allowing a solid assessment on the feasibility of the strategy of constructing multiple functional domains. Specifically, the typical LiAl-LDH precursor was first prepared by co-precipitation of Li/Al salts, and then the precursor was mixed with the solution containing modifiers for simultaneous activation and modification to obtain LiAl-LDH/PAM (Figure 2a).



**Figure 5.2** Schematic illustration of the LiAl-LDH modified with PAM.

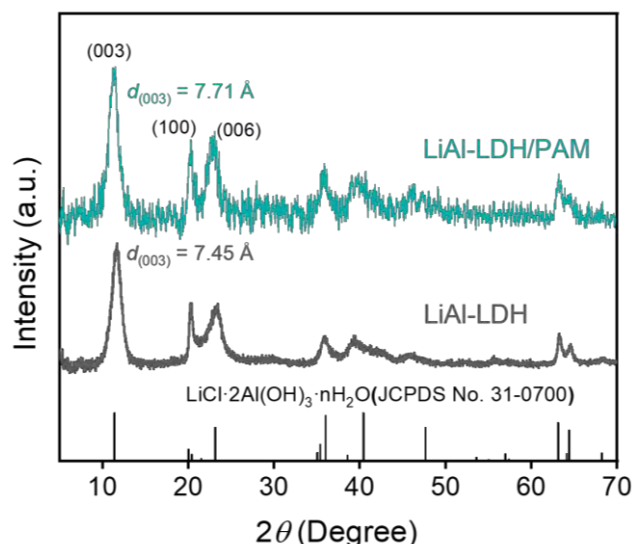
Transmission electron microscopy (TEM) images presented the hexagonal morphologies of LiAl-LDH nanosheets with diameters of  $\sim 80$  nm (Figure 5.3a,d). The high-resolution TEM (HRTEM) image and corresponding selected area electron

diffraction (SAED) pattern indicated that the single crystal nature of the pristine LiAl-LDH. The lattice fringes measured 0.74 nm, consistent with the (003) plane of the LiAl-LDH (JCPDS No. 31-0700) (Figure 5.3b). The SAED pattern exhibited hexagonally arranged diffraction spots, which revealed a hydrocalcite-like crystal structure (Figure 5.3c)[26]. In contrast to the pristine LiAl-LDH, the modified LiAl-LDH/PAM exhibited an interaggregate and densely curled structure owing to the introducing flexible polymers (Figure 5.3d). The distinguishable amorphous regions in the HRTEM image of LiAl-LDH/PAM demonstrated the tight bonding of the PAM to the LiAl-LDH (Figure 5.3e). SAED patterns presented diffuse halo electron diffraction rings indexed to the (009), (006), and (118) planes of the LiAl-LDH, revealing that partial polymer bonded to the adsorbent surfaces, reducing the phase crystallinity (Figure 5.3f)[27]. Notably, the layered structure of LiAl-LDH is retained after PAM modification but increase from original 0.734 nm to 0.776 nm according to the atom distance profiles in Figure 5.3g-h. Moreover, the elemental mapping images reveal the homogeneity of the LiAl-LDH/PAM structures (Figure 5.3i).



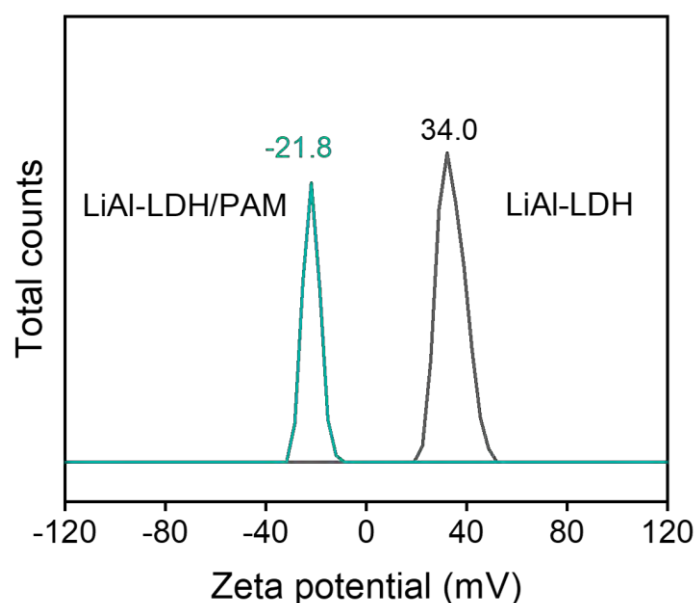
**Figure 5.3** (a) TEM image, (b) HRTEM image, (c) SAED pattern of the pristine LiAl-LDH (d) TEM image, (e) HRTEM image, (f) SAED pattern of the LiAl-LDH/PAM. (g) Atom distance profiles from lattice fringes of (003) plane of (g) the pristine LiAl-LDH and (h) the LiAl-LDH/PAM. (i) Mapping images of the LiAl-LDH/PAM.

X-ray diffraction (XRD) patterns further demonstrated the successful preparation of LiAl-LDH/PAM with decreased crystallinity and expanded interlayer spacing from 7.45 Å to 7.71 Å (Figure 5.4), in well agreement with the TEM analysis, where the diffraction peak of (003) plane (JCPDS#31-0700) became border and lower accompanying with a shift toward low  $2\theta$  after modification.



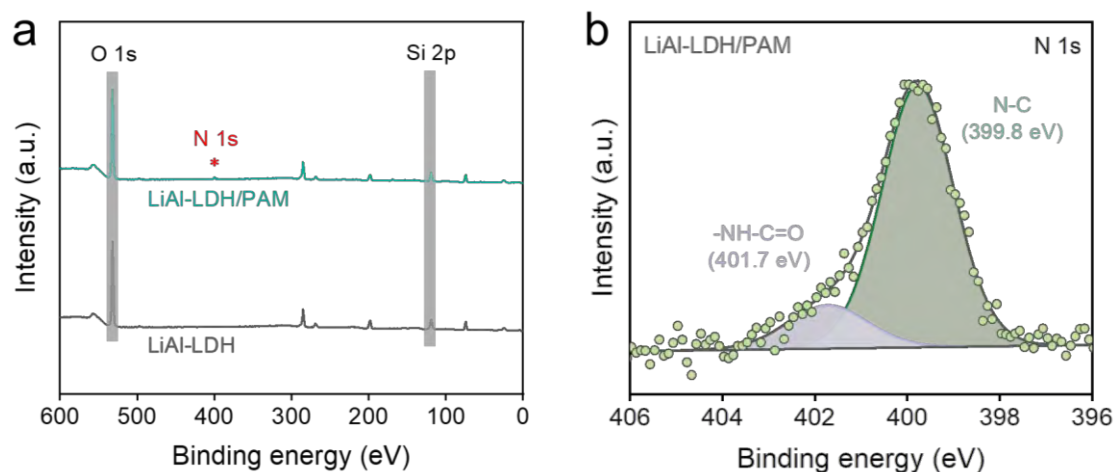
**Figure 5.4** XRD patterns of the pristine LiAl-LDH and LiAl-LDH/PAM.

Such modification tuned the zeta potential of LiAl-LDH/PAM from positive to negative due to the polar functional groups with rich lone pair electrons in the PAM, indicating the presence of PAM on the surface of LiAl-LDH/PAM, which can yield a strong attraction for  $\text{Li}^+$  while repulsion for  $\text{SO}_4^{2-}$  (Figure 5.5).



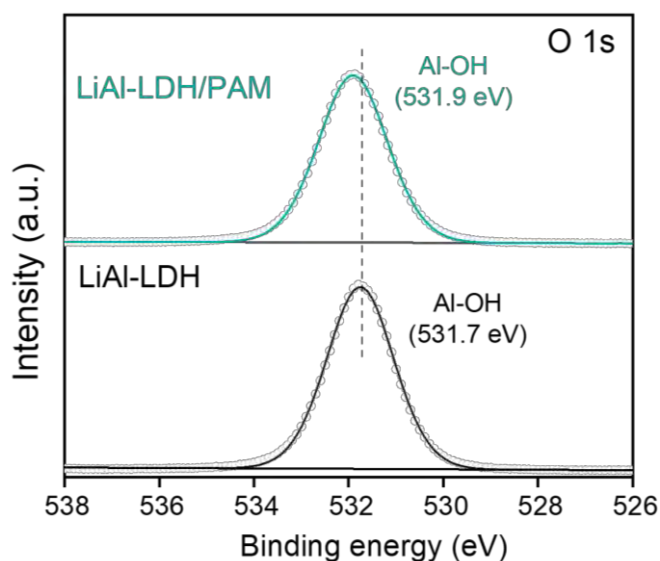
**Figure 5.5** Zeta potentials of the pristine LiAl-LDH and LiAl-LDH/PAM.

Moreover, X-ray photoelectron spectroscopy (XPS) of LiAl-LDH/PAM after modification appeared new N 1s peak (Figure 5.6a). XPS spectrum for the characteristic elemental N 1s core level indicated the existence of PAM with groups of  $-\text{CONH}_2$  on the surface of the LiAl-LDH/PAM (Figure 5.6b).



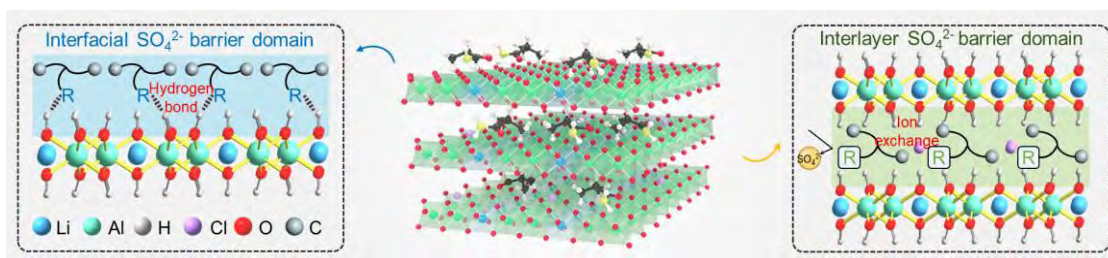
**Figure 5.6** (a) XPS survey spectra of the pristine LiAl-LDH and LiAl-LDH/PAM. (b) XPS spectrum for the N 1s core level of the LiAl-LDH/PAM.

Furthermore, as for the XPS spectrum of O 1s core level of the LiAl-LDH/PAM, the peak of Al-OH occurred a significant blue shift (). This implied that the electrons around O atoms on Al-OH transferred to the H atoms on  $-\text{CONH}_2$  groups of the PAM, and hydrogen bonds were formed between the PAM and the LiAl-LDH [28].



**Figure 5.7** XPS spectra of O 1s core level of the pristine LiAl-LDH and LiAl-LDH/PAM.

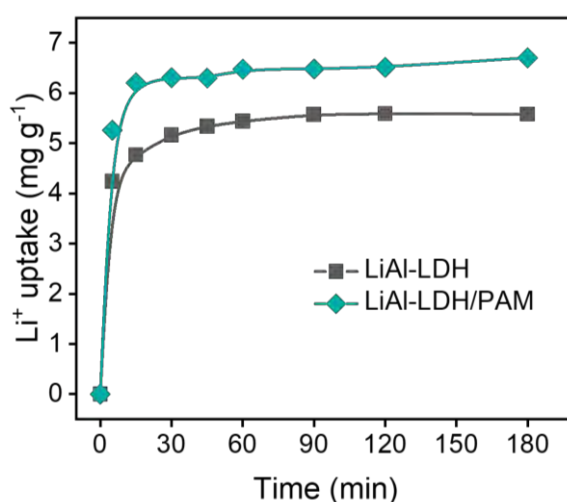
Briefly, LiAl-LDH/PAM were successfully prepared by two-step co-precipitation-activation modification method, in which part of the PAM was connected to the surface by hydrogen bonds to create, and the rest was intercalated into the LiAl-LDH interlayer via ion exchange to form multiple  $\text{SO}_4^{2-}$  repelling domains, which facilitate sustainable lithium extraction from  $\text{SO}_4^{2-}$ -type brines (Figure 3g).



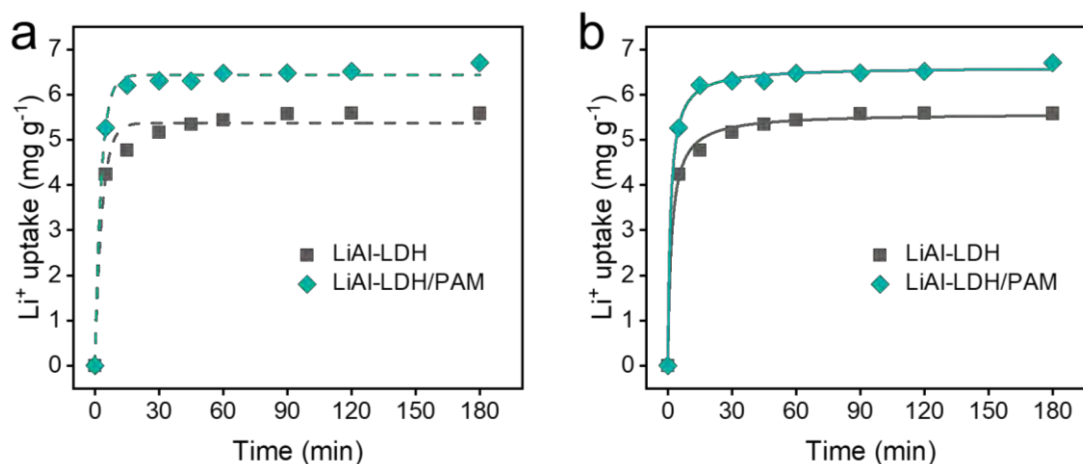
**Figure 5.8** Schematic of multiple functional domains of LiAl-LDH/PAM and interactions between LiAl-LDH and polymer building blocks.

### 5.3.2. Lithium extraction performance

The as-obtained LiAl-LDH/PAM were used in real Lop Nor Salt-Lake brine, the largest  $\text{SO}_4^{2-}$ -type brine in the world, to evaluate the practical feasibility of the proposed strategy. The kinetics experiments displayed that the pristine LiAl-LDH reached equilibrium in 60 min, while LiAl-LDH/PAM could extract lithium faster within 30 min (Figure 5.9). Moreover, the LiAl-LDH/PAM showed a significantly increased  $\text{Li}^+$  adsorption capacity ( $6.71 \text{ mg g}^{-1}$ ) compared to the pristine LiAl-LDH ( $5.57 \text{ mg g}^{-1}$ ). The improved extraction performance might be attributed to the higher lithium affinity of LiAl-LDH/PAM due to the positive surface potential (Figure 5.5). Further, the adsorption kinetic modeling analysis revealed the chemisorption-dominated Li extraction processes of the pristine LiAl-LDH and LiAl-LDH/PAM (Figure 5.10 and Table 5.2) [20].



**Figure 5.9**  $\text{Li}^+$  adsorption kinetics of the pristine LiAl-LDH and LiAl-LDH/PAM in Lop Nor brine.

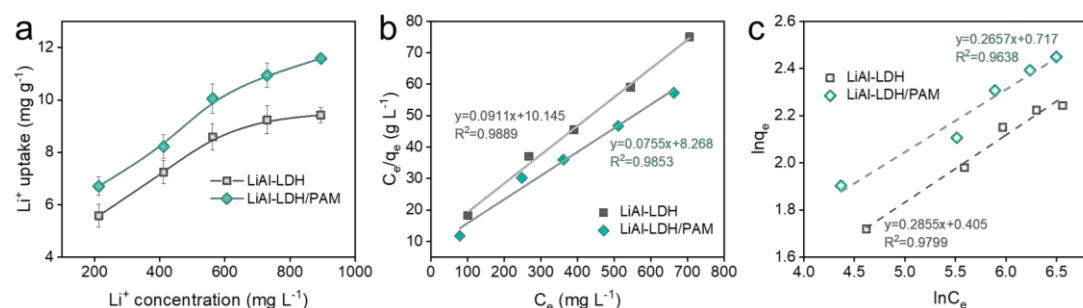


**Figure 5.10** (a) Pseudo-first-order and (b) pseudo-second-order kinetic models of  $\text{Li}^+$  adsorption on the pristine LiAl-LDH and LiAl-LDH/PAM in Lop Nor brine.

**Table 5.2** Adsorption kinetic model parameters of the pristine LiAl-LDH and LiAl-LDH/PAM.

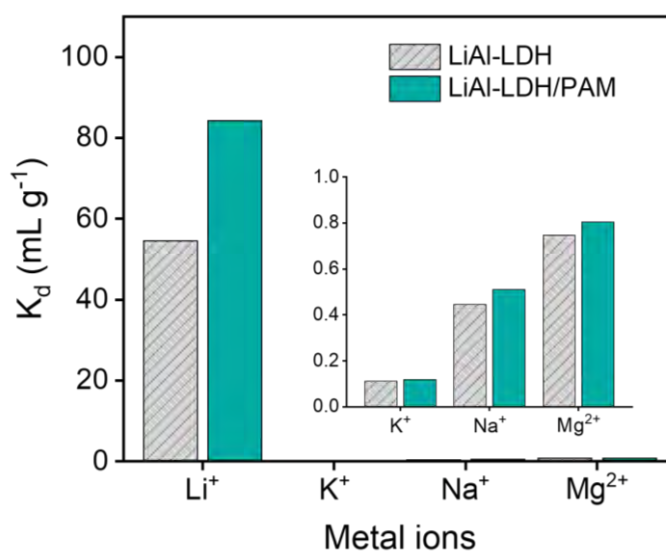
Samples	Pseudo-first-order			Pseudo-second-order		
	$q_e$ (mg/g)	$k_1$ ( $\text{min}^{-1}$ )	$R^2$	$q_e$ (mg/g)	$k_2$ ( $\text{g}/(\text{mg}\cdot\text{min})$ )	$R^2$
LiAl-LDH	5.37	0.2974	0.9787	5.58	0.0792	0.9957
LiAl-LDH/PAM	6.43	0.3368	0.9951	6.61	0.1201	0.9984

Furthermore, the isotherm experiments provided solid support for the strategy, as the  $\text{Li}^+$  adsorption capacity of the LiAl-LDH/PAM exceeded that of pristine LiAl-LDH at the full range of  $\text{Li}^+$  concentration tested (Figure 5.11a). The analysis of isotherm models presented that  $\text{Li}^+$  uptake was a homogeneous adsorption process, suggesting the uniform distribution of PAM on the LiAl-LDH/PAM (Figure 5.11b-c) [29].



**Figure 5.11** (a) The adsorption capacity of  $\text{Li}^+$  on the pristine LiAl-LDH and LiAl-LDH/PAM in Lop Nor brine with different  $\text{Li}^+$  concentration. (b) Langmuir and (c) Freundlich models of  $\text{Li}^+$  on the pristine LiAl-LDH and LiAl-LDH/PAM.

As well, the selectivity was investigated in detail. As shown in Figure 5.12, the dispersion coefficient ( $K_d$ ) values of the pristine LiAl-LDH and LiAl-LDH/PAM for  $\text{Li}^+$  were larger than 50, while those for the other main coexisting metal ions below 1, indicating the well selectivity, which originated from the memory effect and size screening effect [21]. Further, the separation factors ( $\alpha$ ) of  $\text{Li}^+/\text{Mg}^{2+}$ ,  $\text{Li}^+/\text{Na}^+$  and  $\text{Li}^+/\text{K}^+$  were determined. The LiAl-LDH/PAM (104.65) presented significant higher  $\alpha_{\text{Li}/\text{Mg}}$  than pristine LiAl-LDH (72.99). The selectivity of LiAl-LDH/PAM for  $\text{Li}^+/\text{Na}^+$  and  $\text{Li}^+/\text{K}^+$ , on the other hand, was higher than that for  $\text{Li}^+/\text{Mg}^{2+}$ , because of the weaker binding of functional groups to  $\text{Na}^+$  and  $\text{K}^+$  than  $\text{Mg}^{2+}$ , as well as the apparently larger ionic sizes of  $\text{Na}^+$  (2.76 Å) and  $\text{K}^+$  (2.04 Å) [30].



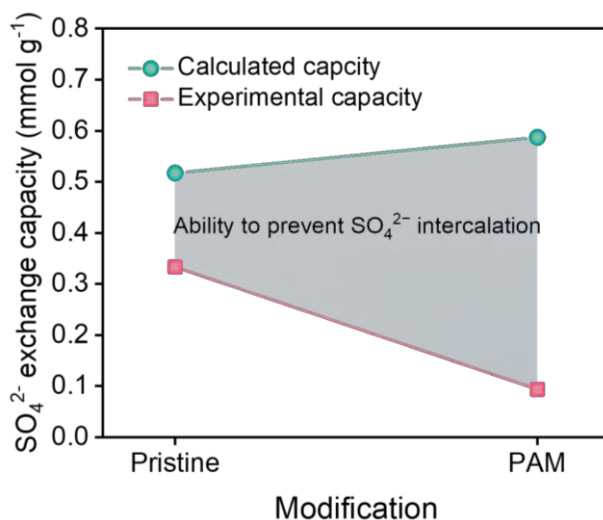
**Figure 5.12** Dispersion coefficient ( $K_d$ ) values of the pristine LiAl-LDH and LiAl-LDH/PAM in Lop Nor brine.

Overall, benefited from the proposed strategy of constructing multiple functional domains, the LiAl-LDH/PAM modified with the PAM presented excellent lithium extraction performance from  $\text{SO}_4^{2-}$ -type brines, including the adsorption rate, adsorption capacity, and  $\text{Li}^+$  selectivity, unveiling the sophistication of the strategy.

### 5.3.3. Anti-sulfate ion poisoning performance

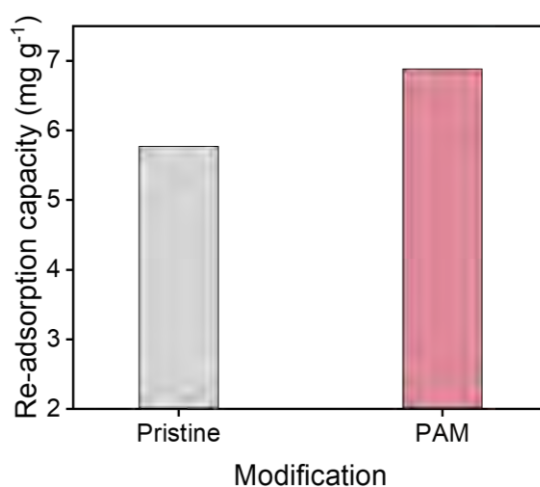
To evaluate the effect of the proposed strategy on the anti-sulfate ion poisoning performance that is considered as the ‘Achilles heel’ of the LiAl-LDHs, the  $\text{SO}_4^{2-}$  exchange capacity during the Li extraction procedure in Lop Nor brine was carried out. As shown in Figure 5.13, the exchange capacity of the pristine LiAl-LDH was 0.33 mmol g<sup>-1</sup>, indicating that its susceptibility to sulfate ion poisoning. Encouragingly, the

exchange capacities of LiAl-LDH/PAM greatly decreased, which revealed the advancement of the proposed strategy against sulfate ion poisoning.



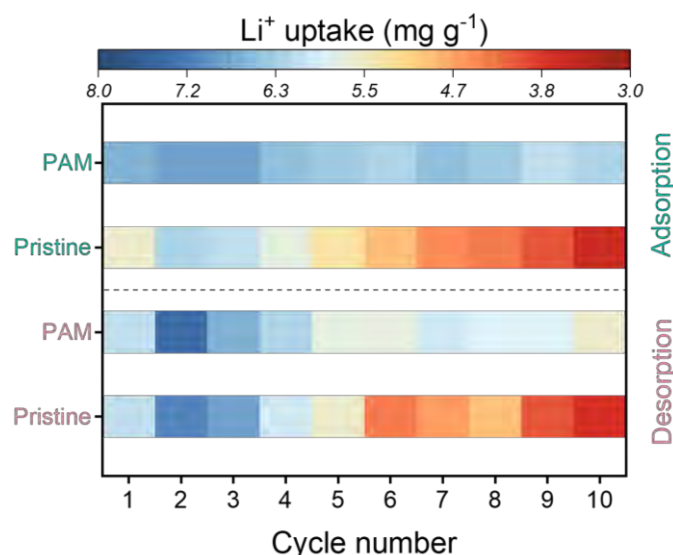
**Figure 5.13** The  $\text{SO}_4^{2-}$  exchange capacities of the pristine LiAl-LDH and LiAl-LDH/PAM.

Further, the re-adsorption experiments were conducted, and the  $\text{Li}^+$  re-adsorption capacities slightly reduced or constant (Figure 5.14). It is declared that the single re-adsorption capacity of LiAl-LDHs in certain  $\text{SO}_4^{2-}$ -type brines with sufficient ionic strength might be high, during long-term desorption-adsorption cycles, however, the replacement of interlayer  $\text{Cl}^-$  by  $\text{SO}_4^{2-}$  accumulates and gradually suppresses the desorption and re-adsorption of  $\text{Li}^+$ , leading to the unsatisfactory long-term Li extraction of from  $\text{SO}_4^{2-}$ -type brines by LiAl-LDHs. To this end, 10 desorption-adsorption cycle experiments were performed.



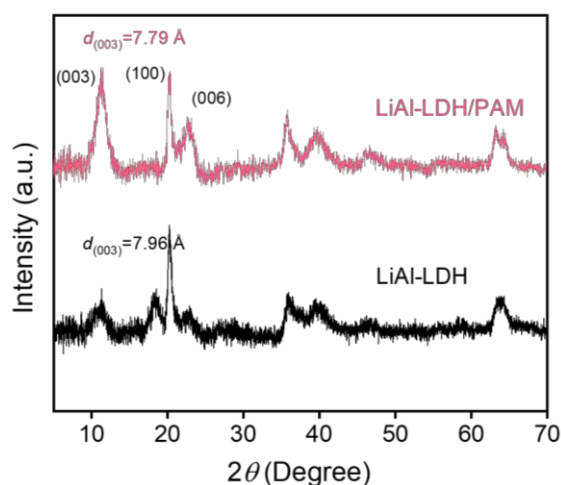
**Figure 5.14**  $\text{Li}^+$  re-adsorption capacity of the pristine LiAl-LDH and LiAl-LDH/PAM in Lop Nor brine.

To trail the accumulation of  $\text{SO}_4^{2-}$  in the interlayer, 10 desorption-adsorption cycle experiments were carried out (Figure 5.15). The reduction in uptake was remarkably different. As for the pristine LiAl-LDH, the adsorption and desorption capacity reduced by over 40%, demonstrating severe poisoning. In contrast, these for LiAl-LDH/PAM were reduced from  $\sim 6.7$  mg/g to  $\sim 6.3$  mg/g, proving the enhanced anti-sulfate ion poisoning performance.



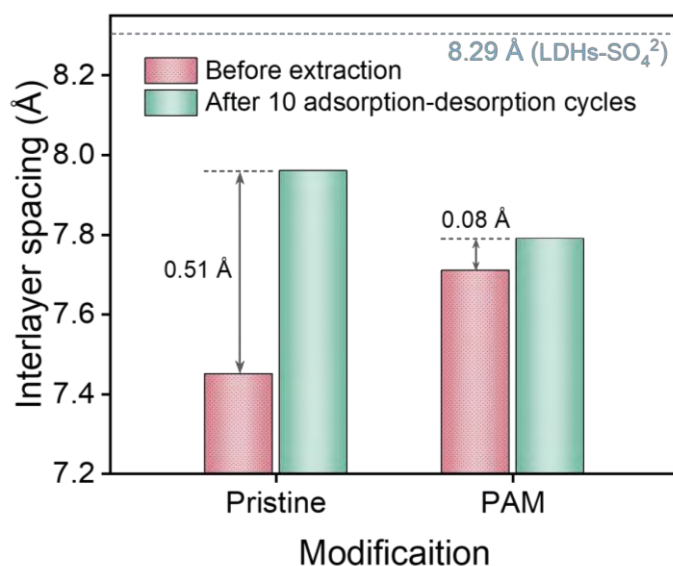
**Figure 5.15**  $\text{Li}^+$  uptakes of the pristine LiAl-LDH and LiAl-LDH/PAM during the adsorption-desorption cycling experiments.

After ten adsorption-desorption cycles, the XRD measurements of all the pristine LiAl-LDH and LiAl-LDH/PAM were carried out. Compared to the XRD peaks before extraction, peaks of pristine LiAl-LDH were broadened and weakened after 10 cycles, suggesting decreased crystallinity and poor stability in  $\text{SO}_4^{2-}$ -type brines (Figure 5.16).



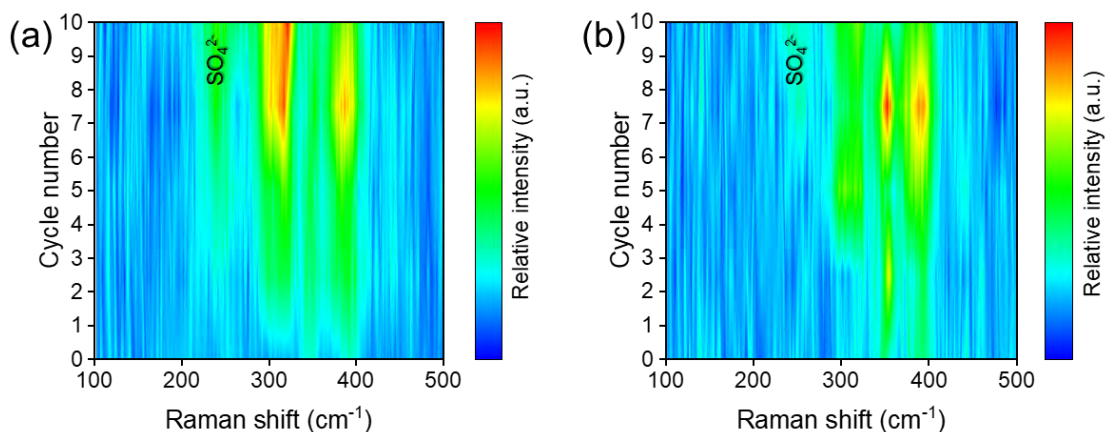
**Figure 5.16** XRD patterns of pristine LiAl-LDH and LiAl-LDH/PAM after ten adsorption-desorption cycles.

Moreover, statistical analysis of the (003) plane unveiled the level of  $\text{SO}_4^{2-}$  intercalation into LiAl-LDH adsorbents (Figure 5.17). The interlayer spacing of pristine LiAl-LDH increased from 7.45 Å to 7.96 Å with an increase of 0.51 Å during cycling, indicating the severe intercalation of  $\text{SO}_4^{2-}$ . While the (003) plane spacing of LiAl-LDH/PAM were below 7.8 Å with an increase of 0.08 Å, validating the significant improvement in the anti-sulfate ion poisoning property of LiAl-LDH/PAM.



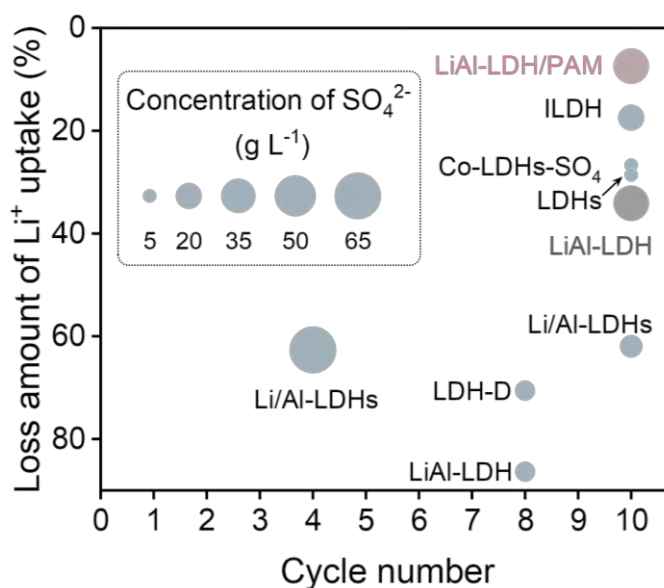
**Figure 5.17** The interlayer spacing of LiAl-LDHs before and after 10 adsorption-desorption cycling experiments.

Furthermore, Raman spectroscopy was also applied to track the structural evolution of pristine LiAl-LDH and LiAl-LDH/PAM (Figure 5.18). As for pristine sample, two peaks corresponding to the typical LiAl-LDHs vibration were observed at around 348 and 392  $\text{cm}^{-1}$  during the whole desorption-adsorption cycle process (Figure 5.18a) [31]. With the continuous cycle, the Al-O vibration peak corresponding to  $\text{Al}(\text{OH})_3$  generated at  $\sim 320 \text{ cm}^{-1}$ , suggesting that certain LiAl-LDH sites had been poisoned, resulting in their inability to trap  $\text{Li}^+$  to form a layered double hydroxide structure [23]. At the same time, a new mode corresponding to  $\text{SO}_4^{2-}$  (near 252  $\text{cm}^{-1}$ ) was found in the structure [32], demonstrating that the pristine LiAl-LDH was poisoned with sulfate ions at the early stage of the continuous Li extraction cycle. On the contrary, LiAl-LDH/PAM gradually presented low-intensity sulfate ion signals only at the final stage of the cycling process (Figure 5.18b), which reconfirmed its excellent resistance to sulfate poisoning.



**Figure 5.18** Contour plots of Raman spectra of (a) pristine LiAl-LDH and (b) LiAl-LDH/PAM during 10 adsorption-desorption cycling experiments.

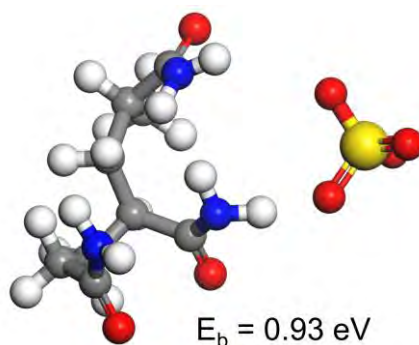
Encouraged by the above results, the anti-sulfate poisoning properties of the prepared LiAl-LDH/PAM was compared with the reported LiAl-LDH-based adsorbents. The excellent stability and regeneration ability of the adsorbents are always desired, and thus the promising LiAl-LDHs are required to have larger bubble diameters and be in the upper right region of Figure 5.19. A brief glance at this region revealed that LiAl-LDH/PAM exhibits the best anti-sulfate poisoning performance, namely, the long-term stable Li extraction at higher sulfate ion concentrations with only a slight decrease in uptake. Apparently, the proposed strategy enabled the LiAl-LDH to be highly feasible for continuous Li extraction from  $\text{SO}_4^{2-}$ -type brines.



**Figure 5.19** Comparison of the anti-sulfate ion poisoning performance between proposed LiAl-LDHs and reported LiAl-LDH-based adsorbents in  $\text{SO}_4^{2-}$ -type brines.

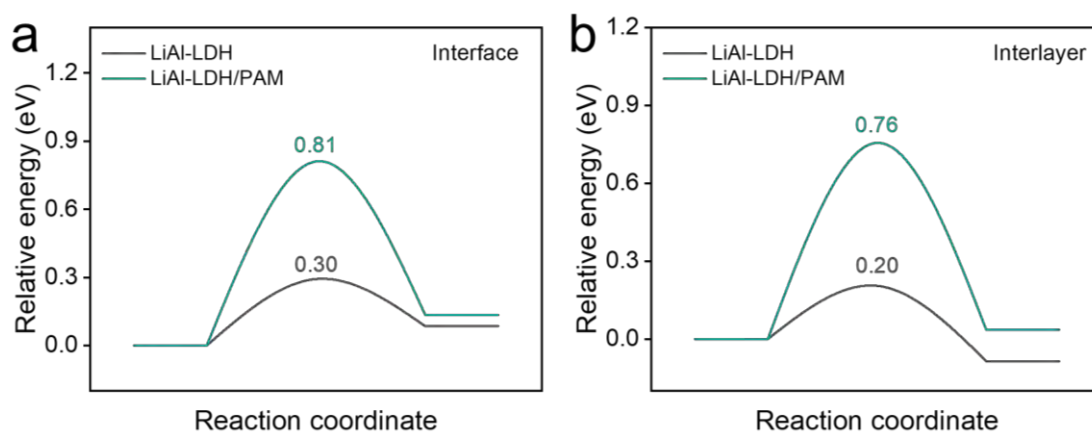
### 5.3.4. Mechanisms of anti-sulfate ion poisoning

To demonstrate the mechanisms of anti-sulfate ion poisoning of the LiAl-LDH/PAM, density functional theory (DFT) calculations were performed. Due to the polar functional groups with rich lone pair electrons, the positive binding energy of the PAM (0.93 eV) for  $\text{SO}_4^{2-}$  were observed, which confirmed the repulsion interaction, favoring to prevent the decline of  $\text{Li}^+$  uptake induced by the  $\text{SO}_4^{2-}$  intercalation into LiAl-LDH (Figure 5.20).

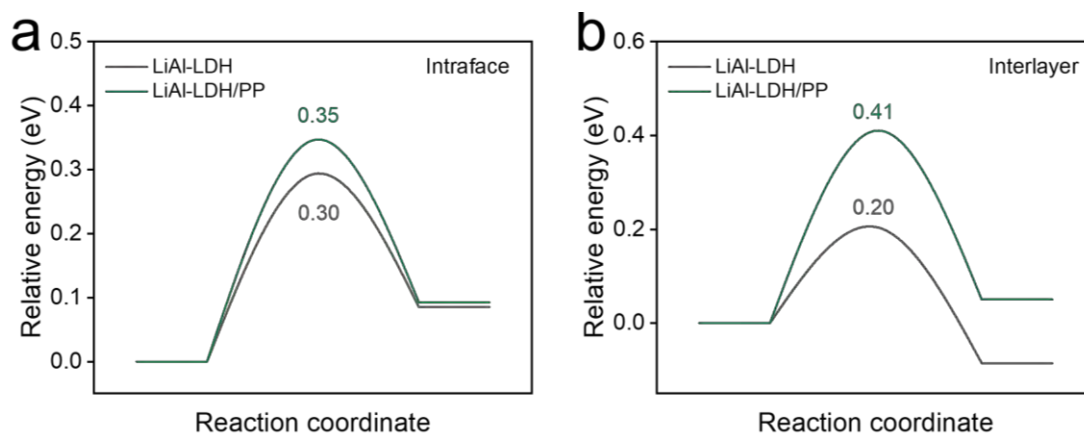


**Figure 5.20** The binding energy between  $\text{SO}_4^{2-}$  and PAA.

Further, the migration of  $\text{SO}_4^{2-}$  over intralayer and interlayer of LiAl-LDHs was simulated, and the diffusion barrier energies were calculated. As shown in Figure 5.21, the barrier energies either from the intralayer or interlayer of LiAl-LDH/PAM are much higher than that from pristine LiAl-LDH. The results demonstrated that the intercalation of polymer modifiers not only inhibit  $\text{SO}_4^{2-}$  accessing the intralayer, but also increases the diffusion energy of  $\text{SO}_4^{2-}$  in LiAl-LDH interlayer, which resulted from the electrostatic repulsion of side groups and steric hindrance effect of polypropylene (PP) backbone (Figure 5.22).

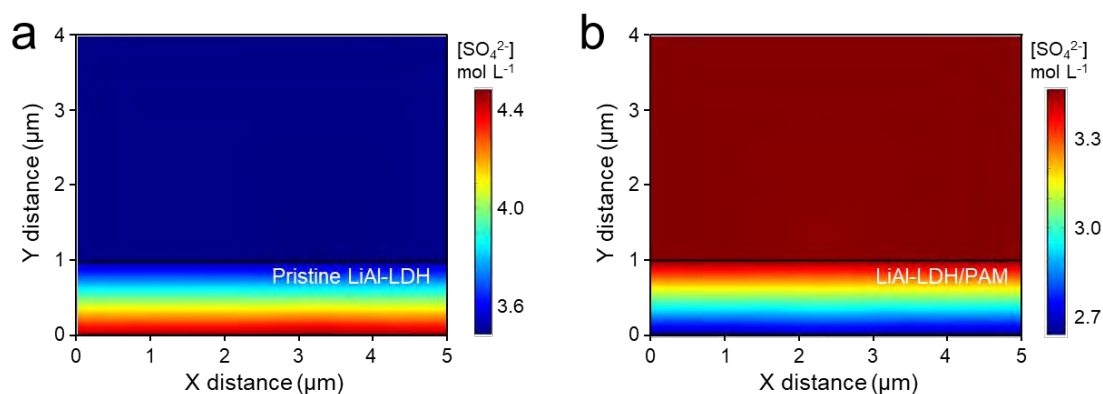


**Figure 5.21** Energy barrier for (a)  $\text{SO}_4^{2-}$  migration over interface and (b) interlayer of the pristine LiAl-LDH and LiAl-LDH/PAM.

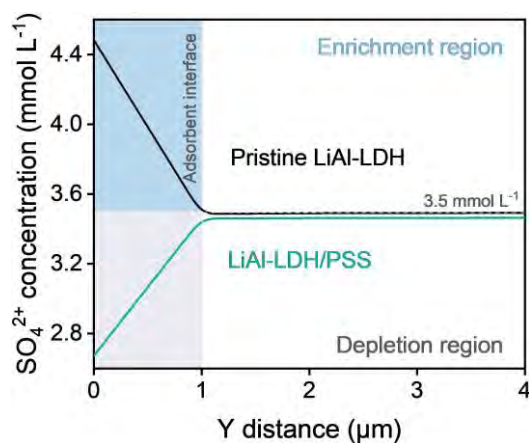


**Figure 5.22** Energy barrier for (a)  $\text{SO}_4^{2-}$  migration over interface and (b) interlayer of the pristine LiAl-LDH and LiAl-LDH/PP.

The advancement of the PAM modification against sulfate ion poisoning were re-confirmed by the numerical simulations. As shown in Figure 5.23, whereby a  $\text{SO}_4^{2-}$  enrichment region was observed on the pristine LiAl-LDH surface while a depletion region of  $\text{SO}_4^{2-}$  was found on the LiAl-LDH/PSS surface (Figure 5.24).



**Figure 5.23** Numerical simulation of  $\text{SO}_4^{2-}$  diffusion in (a) pristine LiAl-LDH, and (b) LiAl-LDH/PAM.



**Figure 5.24** The  $\text{SO}_4^{2-}$  concentration as a function of Y distance from the results of Numerical simulations.

## 5.4. Conclusions

In summary, based on the instinct properties of LiAl-LDHs, a strategy of constructing multiple  $\text{SO}_4^{2-}$  repelling domains in the interface and interlayer using the organic modification with the PAM was proposed for sustainable lithium extraction from  $\text{SO}_4^{2-}$ -type brines. Characterizations and simulations revealed that the electrostatic repulsion induced by negatively charged side-chain groups of the PAM and the steric hindrance effect of polypropylene (PP) backbone delivered the repulsion interaction towards  $\text{SO}_4^{2-}$  and the increased energy barrier for  $\text{SO}_4^{2-}$  migration over interface and interlayer of the LiAl-LDH/PAM. Consequently, the intercalation of  $\text{SO}_4^{2-}$  was greatly hindered to prevent adsorption site blocking, which endowed the LiAl-LDH/PAM excellent anti-sulfate poisoning property for robust lithium extraction from Lop Nor brine, the largest  $\text{SO}_4^{2-}$ -type in the world. Additionally, negatively charged surface enhanced the affinity between the LiAl-LDH/PAM and  $\text{Li}^+$ , enabling the excellent  $\text{Li}^+$  selectivity and the maximum adsorption capacity ( $13.25 \text{ mg g}^{-1}$ ) in the real  $\text{SO}_4^{2-}$ -type brine. This work provides a feasible strategy for sustainable lithium extraction from  $\text{SO}_4^{2-}$ -type brines, and can be extended to other kinds of brines, like  $\text{CO}_3^{2-}$ -type brines.

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## **Chapter 6. Molecular tailoring engineering of lithium aluminum layered double hydroxides for lithium extraction from low-quality brines**

### **6.1. Introduction**

Lithium (Li), a critical metal resource in current global electrification and decarbonization strategies, has become pivotal in powering the novel electric vehicles, consumer electronics and energy storage systems [1-4]. These technological evolution drives exponentially growing global demand, making the sustainable supply of Li particularly urgent [5,6]. Currently, commercial Li is exclusively dependent on high-grade Li ores and continental brines, which are geologically constrained in very few countries [7,8]. Low-quality brines, including salt lakes, geothermal brines, oilfield brines, gas-produced water, and seawater, contain massive untapped Li resources and are distributed throughout the world [9]. Such resources can diversify the Li supplies and offer significant environmental and economic benefits for sustainable lithium extraction. However, Li extraction from brines remains technically and economically feasible only when the Li concentrations exceed 500 mg L<sup>-1</sup> [9-11]. The low concentration of Li<sup>+</sup> (< 260 mg L<sup>-1</sup>) and high concentration of competing Mg<sup>2+</sup> (Mg<sup>2+</sup>/Li<sup>+</sup> ratio, MLR > 6.15) of low-quality brines are main issues in hindering effective Li extraction [12-14].

Conventional evaporation-based Li extraction from low-quality brines is time-consuming and suffers from lithium entrainment losses potentially exceeding 60% during concentrating [7,8,15-18]. The concentrated brines require further purification to remove competing ions (especially Mg<sup>2+</sup>), challenging the sustainable production of Li [19,20]. Adsorption has been a prominent industrial solution for direct lithium extraction from brines due to simple process and low energy consumption [21,22]. In particular, lithium-aluminum layered double hydroxides (LiAl-LDHs) are one of the most successful adsorbents due to their tailored octahedral cavity structure (~1.4 Å) for selective coordination by matching the Li<sup>+</sup> diameters and desorption without dissolution loss [23-25]. As presented in the Figure 6.1, LiAl-LDHs has a brucite-like [LiAl<sub>2</sub>(OH)<sub>6</sub>]<sup>+</sup> layered structure with Li<sup>+</sup> embedded in intralayer octahedral sites, while

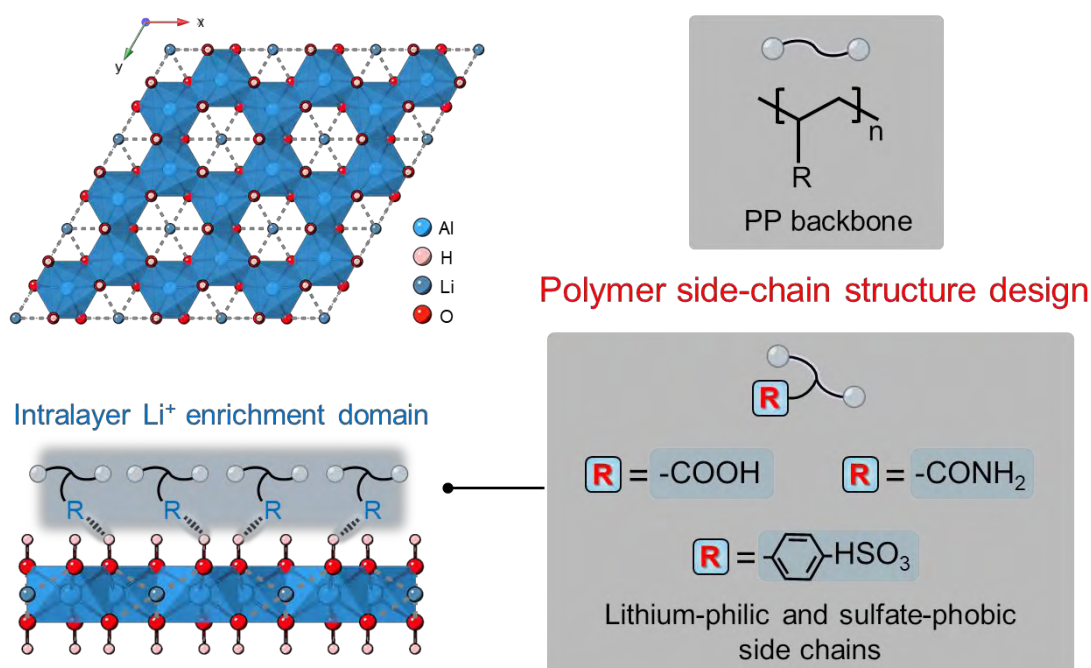
the interlayer is filled with anions (typically  $\text{Cl}^-$ ) and water molecules [26,27]. The reversible  $\text{Li}^+$  intercalation and deintercalation mechanism enables selective lithium extraction from brines and regeneration of LiAl-LDHs adsorbents [24,28]. Current applications of LiAl-LDHs are still restricted in continental brines, while crucial concerns remain regarding lithium extraction from low-quality brines: i) the limited extraction rate and efficiency caused by the low  $\text{Li}^+$  concentration. Although external energy-driven methods (e.g. electric field and photothermal energy) can concentrate  $\text{Li}^+$  [29,30], they require complex operation, energy consumption, and large-scale supporting equipment, making them unsuitable for industrial-scale integration with LiAl-LDHs; ii) the poor universality of even advanced LiAl-LDHs due to the markedly complex components. Low-quality brines are abundant and widely distributed, and their composition is very complicated, and the differences in components, especially the MLR, are very large, which make even advanced LDH difficult to realize efficient lithium extraction from different low-quality brines. Therefore, purpose-driven design and innovation in LiAl-LDHs adsorbents aiming on high-efficiency and versatile Li extraction is important for sustainable Li extraction from low-quality brines.

Polymer side-chain engineering enables manipulation of the local spatial microstructure and chemical microenvironment of architectures through altering the molecular structure of side chains, which is well recognized as an effective and feasible regulation strategy for ion transport [31-33]. The water transport and ion separation of laminate membranes, for example, could be precisely modulated by introducing porphyrin-based aromatic macrocycle with different side chains [34]. In the previous chapter, we have found that polymer-modified LiAl-LDHs not only exhibits excellent anti-sulfate poisoning properties, but also offers enhanced lithium extraction performance. Inspired by these, the unique layered structure of LiAl-LDHs serves as an ideal platform for intralayer engineering with functional polymers. The diversity of the side chains offers great possibility in effectively addressing poor lithium extraction efficiency in low-quality brine. By rational design, the side-chain modified LiAl-LDH integrates the interdisciplinary theoretical prediction with practical implementation, which allows for scalable lithium recovery that demand high selectivity, capacity, and adaptability to different types low-quality brines.

In this work, a polymer side-chain structure design (SCSD) strategy is reported to engineer LiAl-LDHs with a  $\text{Li}^+$ -enriched intralayer domains via hydrogen bond interaction (Figure 6.1). Here, LiAl-LDHs was modified by a polypropylene (PP)

backbone, and the common polar functional groups with rich lone pair electrons involving carboxyl groups (polyacrylic acid, PAA), sulfonic acid groups (polystyrene sulfonate, PSS), and amide groups (polyacrylamide, PAM), are adapted as lithium-philic side chains to modulate the properties of intralayer environment. Based on the SCSD strategy, LiAl-LDHs modified by polymers (LiAl-LDH/PR) presented excellent  $\text{Li}^+$  selectivity and extraordinary  $\text{Li}^+$  enrichment property, enabling  $\text{Li}^+$  recovery of over 90% from the oilfield brine with ultra-low Li concentration ( $19.7 \text{ mg L}^{-1}$ ). Employing Lop Nor brine (one of the largest low-quality brines in the world), SCSD strategy delivered a robust Li extraction repetition achieving ppb-level residual concentration and produced high-purity  $\text{Li}_2\text{CO}_3$ . The strategy significantly develops the feasibility of LiAl-LDHs, can easily tune the lithium extraction procedure, which holds promise for the scalability.

## Molecular tailoring engineering of LiAl-LDHs



**Figure 6.1** Schematic of the LiAl-LDH structure and the effects of polymer side-chain structure design strategy on Li extraction of LiAl-LDHs.

## 6.2. Experimental section

### 6.2.1. Reagents and materials

Lithium chloride ( $\text{LiCl}$ ), aluminum chloride hexahydrate ( $\text{AlCl}_3 \cdot 6\text{H}_2\text{O}$ ), sodium hydroxide ( $\text{NaOH}$ ), polyacrylic acid (PAA), polyacrylamide (PAM) and polystyrene

sulfonic acid (PSS) were purchased from Shanghai Aladdin Biochemical Technology Co., Ltd. All chemical reagents were of analytical grade. The brines used in the experiments are all real brines, see Table 6.1 for details.

**Table 6.1** Composition of brines used in the experiments.

Salt lake brine	Composition (g L <sup>-1</sup> )					
	Li <sup>+</sup>	Mg <sup>2+</sup>	K <sup>+</sup>	Na <sup>+</sup>	Cl <sup>-</sup>	SO <sub>4</sub> <sup>2-</sup>
Lop Nur <sup>a</sup>	0.2222	97.015	2.549	2.899	222.400	37.600
East Taijinar	2.8190	117.573	0.593	0.185	157.200	13.830
Diluted East Taijinar	0.2819	11.757	0.059	0.019	15.720	1.383
Qianjiang Oilfield	0.0197	0.2101	0.8415	89.76	142.014	3.043

<sup>a</sup>: The brine after potassium extraction

### 6.2.2. Preparation of LiAl-LDH/PR

The preparation procedure is similar to that in chapter V. Briefly, the two-step co-precipitation-activation modification method instead of the standard one-step co-precipitation method was employed for LiAl-LDHs synthesis. The LiAl-LDH precursor was first prepared by co-precipitation of Li/Al salts, and then the precursor was mixed with the solution containing modifiers (PAA, PAM, and PSS) for simultaneous activation and modification to obtain engineering adsorbents (LiAl-LDH/PR).

### 6.2.3. Characterizations

The morphological structures of the samples were characterized using a scanning electron microscope (SEM, Zeiss Gemini 300) and transmission electron microscope (TEM, JEM-JEOL-2100) equipped with energy dispersive spectroscopy (EDS) system. X-ray diffraction patterns were recorded using a Bruker diffractometer (XRD, Empyrean) with Cu K $\alpha$  irradiation (40 kV, 100 mA). The surface potentials of the samples were tested using a zeta potential analyzer (Malvern Zetasizer Nano ZS90 zeta). N<sub>2</sub> adsorption-desorption of the samples was carried out using an ASAP2460 pore analyzer, where the specific area, porosity and pore size distributions were determined by the Brunner-Emmett-Taylor method (BET). The contact angles (CA) of the samples were determined by a microscopic contact angle meter. X-ray photoelectron spectra (XPS) were determined by a Thermo Scientific K-Alpha spectrometer. The inductively coupled plasma optical emission spectrometry (ICP-OES, Prodigy 7) measurement was employed to analyze the proportion of metal species in the sample.

#### 6.2.4. Lithium-ion extraction and $\text{Li}_2\text{CO}_3$ production

**Lithium extraction:** The Li extraction experiments, including adsorption, desorption, selectivity experiments, are consistent with those in Chapter V except for the brines used.

**Sequential lithium recovery:** 3 g LiAl-LDH/PAM were added to Lop Nur brine of 300 mL, shaken for 3h and centrifuged to separate, where the supernatant was retained for the following  $\text{Li}^+$  adsorption, and the bottom precipitates were desorbed by adding 150 mL of deionized water at 40 °C for 2 h. At the end of desorption, centrifugal separation was performed to retain the desorbed solution, and the precipitates (*i.e.*, regenerated LiAl-LDH/PAM) were dried and used for the next adsorption-desorption until the  $\text{Li}^+$  in the brine were completely recovery.

**Precipitation of  $\text{Li}_2\text{CO}_3$ :** To ensure  $\text{Li}_2\text{CO}_3$  production, the collected desorption solution (~1.1 L) was further purified with LiAl-LDH/PAM through reabsorption-desorption to increase the Li/Mg ratio. Further, the collected purified  $\text{Li}^+$  solution was heated and concentrated 100 times to prepare the  $\text{Li}^+$ -rich solution. Finally, the excess sodium carbonate ( $\text{Na}_2\text{CO}_3$ ) was added to the  $\text{Li}^+$ -rich solution, inducing lithium carbonate ( $\text{Li}_2\text{CO}_3$ ) precipitation. In order to improve the grade of the precipitated composites, the composites were added to HCl to dissolve and reprecipitation by NaOH to generate insoluble magnesium hydroxide. After filtration to eliminate  $\text{Mg}(\text{OH})_2$ ,  $\text{Na}_2\text{CO}_3$  was added again to precipitate  $\text{Li}^+$ , and high purity  $\text{Li}_2\text{CO}_3$  was obtained.

#### 6.2.5. Theoretical calculations

The electrostatic potential (ESP) distributions of various polymers were calculated by the Gaussian 09 software. The hybridization exchange-correlation generalized Becke-Lee-Yang-Parr (B3LYP) was used to optimize all structures, and described by basis set of 6-31+G(d), and the results were analyzed by GaussView 5.0.

All density functional theory (DFT) calculations were performed through the Materials Studio 8.0 software. The exchange-correlation interactions were described by the generalized gradient approximation of Perdew-Burke-Ernzerhof (GGA-PBE) for structural optimization to minimize the energy. The cut-off energy was set to 570.0 eV, and the convergence criteria for displacement, energy, and force were 0.001 Å,  $1 \times 10^{-5}$  eV/atom, and 0.03 eV/Å, respectively. The binding energies ( $E_b$ ) between ions and polymers were also calculated by Equation 6.1:

$$E_b = E_{A/B} - E_A - E_B \quad (6.1)$$

where  $E_{A/B}$  is the total energy of A and B bonded system;  $E_A$  and  $E_B$  indicate the energies of individual A and B, respectively.

### 6.2.6. Numerical simulation

The numerical simulations are consistent with those in Chapter V except for the key parameters, which are summarized in Table 6.2.

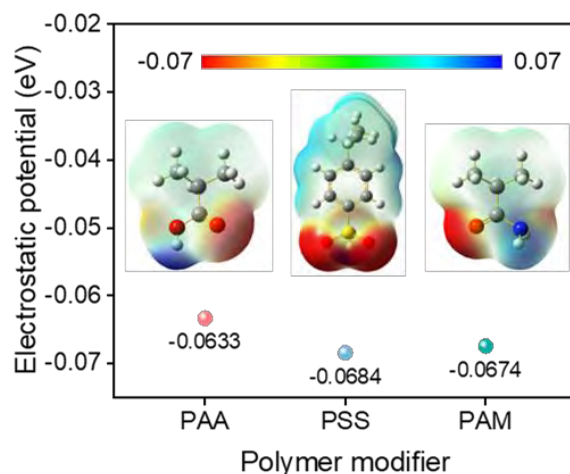
**Table 6.2** Key parameters of multiphysics simulations.

Symbol	Parameter	Value	Unit
$D_{Li}$	Li <sup>+</sup> diffusion coefficient	$1.029 \times 10^{-9}$	m <sup>2</sup> s <sup>-1</sup>
$D_S$	SO <sub>4</sub> <sup>2-</sup> diffusion coefficient	$1.07 \times 10^{-9}$	m <sup>2</sup> s <sup>-1</sup>
$C_{Li}$	Initial Li <sup>+</sup> concentration	7	mol m <sup>-3</sup>
$C_S$	Initial SO <sub>4</sub> <sup>2-</sup> concentration	3.5	mol m <sup>-3</sup>
$z_{Li}$	Number of Li <sup>+</sup> charge	1	Dimensionless
$z_S$	Number of SO <sub>4</sub> <sup>2-</sup> charge	-2	Dimensionless
$\varepsilon$	Permittivity of water	78.4	F/m
$\varepsilon_0$	Permittivity of a vacuum	$8.854 \times 10^{-12}$	F/m
$T$	System temperature	298	K

## 6.3. Results and discussion

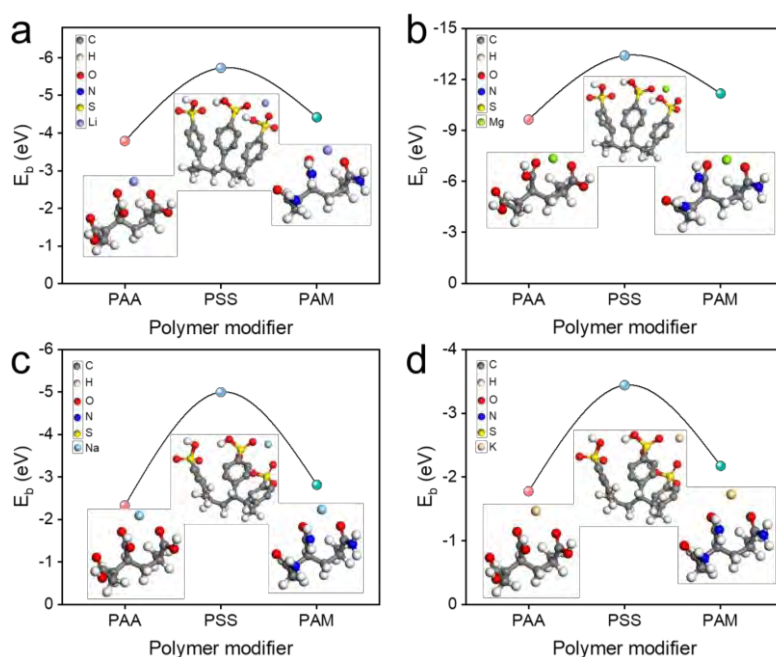
### 6.3.1. Intralayer/interlayer engineering design

First, the theoretical feasibility of the chosen side chains modifiers (PAA, PSS, PAM) in coordinating with Li<sup>+</sup> and SO<sub>4</sub><sup>2-</sup> is evaluated. The electrostatic potential (ESP) distribution of these polymer modifiers was calculated and shown in Figure 1b. The region with electrostatic potential is mainly distributed on the side chains, where van der Waals surface presents different ESP owing to the distinct electron donor and acceptor properties of side groups [35]. The negative electrostatic potential (red area) originates from the ionization of side groups and is primarily around C=O or S=O, with the minimum ESP following the order: PSS < PAM < PAA.



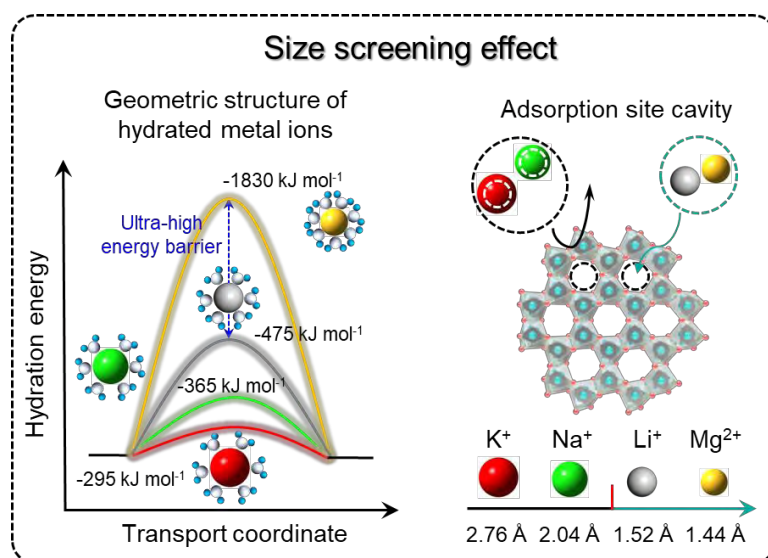
**Figure 6.2** Electrostatic potential and the minimum electrostatic potential value of PAA, PSS, PAM.

Then, density functional theory (DFT) calculations were performed to illustrate how the side-chain structure of each polymer modifier affects the extraction and transport of  $\text{Li}^+$  (Figure 6.3a). According to the binding energy ( $E_b$ ), all three modifiers exhibited a favorable binding towards  $\text{Li}^+$ . It is found that PSS (-5.73 eV) and PAM (-4.42 eV) showed more negative  $E_b$  than PAA (-3.38 eV) demonstrating the more powerful coordination of sulfonic acid and amide side groups with  $\text{Li}^+$  compared to the carboxyl groups. Despite the higher binding energy to  $\text{Mg}^{2+}$ ,  $\text{Na}^+$ , and  $\text{K}^+$  was found (Figure 6.3b-c), it might have a limited effect on the Li extraction process due to the size screening effect of LiAl-LDHs (Figure 6.4) [19,26].



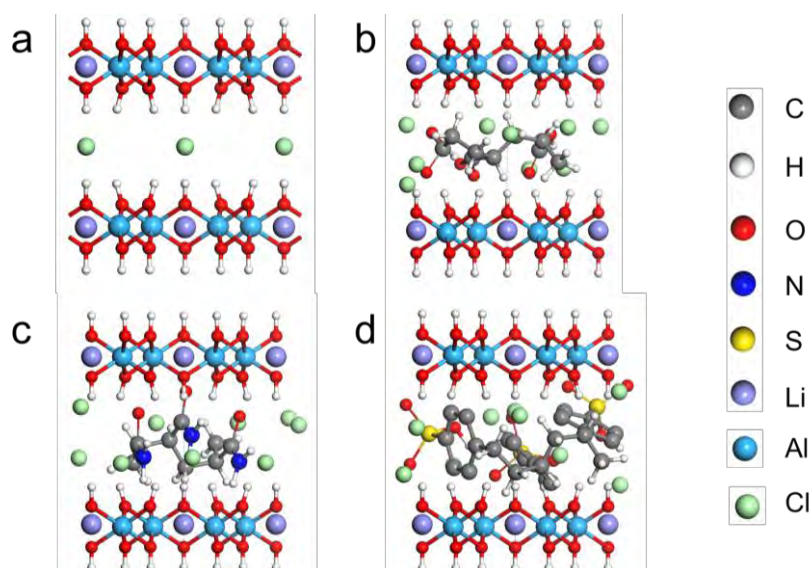
**Figure 6.3** Binding energies between (a)  $\text{Li}^+$ , (b)  $\text{Mg}^{2+}$ , (c)  $\text{Na}^+$ , (d)  $\text{K}^+$  and PAA, PSS,

PAM, respectively.



**Figure 6.4** Schematic of size screening effect of LiAl-LDHs on  $\text{Li}^+$ .

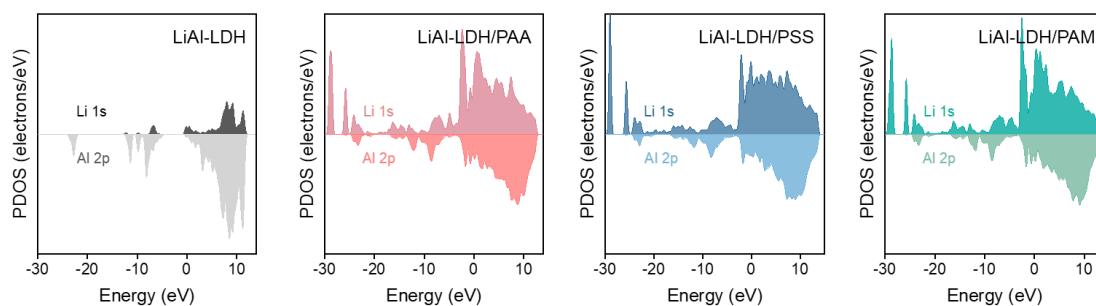
To determine the influence of modifiers on the electric charge properties, theoretical models of LiAl-LDHs modified by polymer building blocks (LiAl-LDH/PR) were constructed, as shown in Figure 6.5.



**Figure 6.5** Optimized structures of (a) LiAl-LDH, (b) LiAl-LDH/PAA, (c) LiAl-LDH/PAM, and (d) LiAl-LDH/PSS.

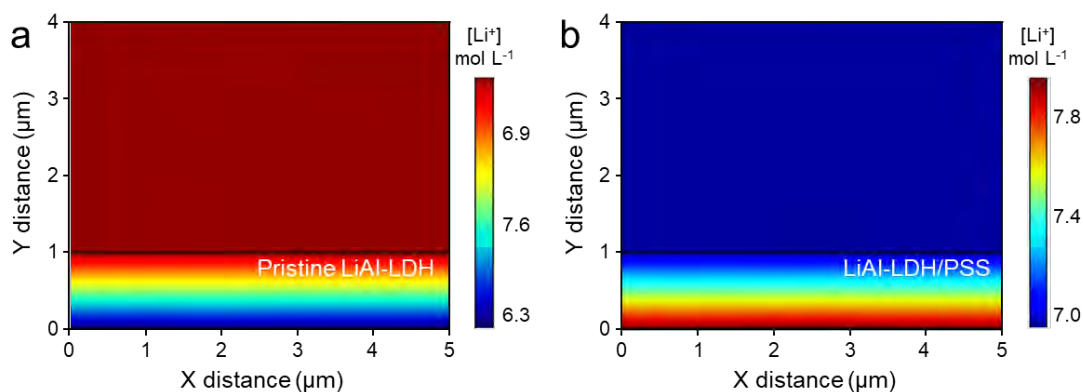
Further, the projected density of states (PDOS) of Li and Al atoms in LiAl-LDH/PR were calculated (Figure 6.6). It can be found that compared to the pristine LiAl-LDH, the overlapping bands of Li 1s and Al 2p in LiAl-LDH/PR are significantly broadened and strengthened, accompanied by a shift to the higher energy, unveiling that the introduction of polymer building blocks enhances  $\text{Li}^+$  adhesion to the laminae and

promotes  $\text{Li}^+$  intercalation into the cavities of  $\text{Al}(\text{OH})_3$  octahedral framework.

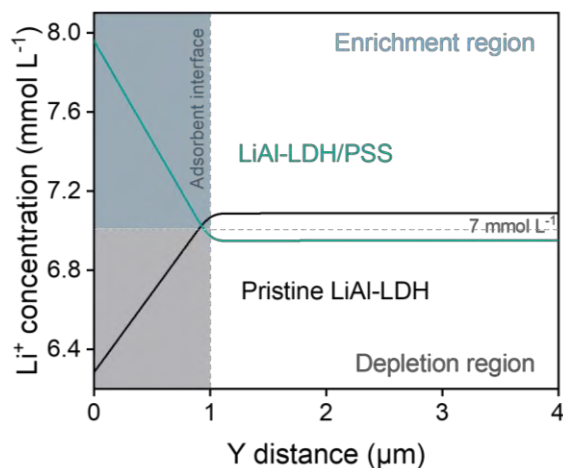


**Figure 6.6** Projected density of states (PDOS) of Li and Al atoms of LiAl-LDH, LiAl-LDH/PAA, LiAl-LDH/PSS, and LiAl-LDH/PAM.

Furthermore, the enrichment effect of polymer modifiers on  $\text{Li}^+$  was analyzed via finite element method, in which the simplified 2D models of ultra-low  $\text{Li}^+$  solutions ( $7 \text{ mol m}^{-3}$ ) containing LiAl-LDHs with different surface charges were constructed. The pristine LiAl-LDH exhibited a significant lower  $\text{Li}^+$  concentration distribution in the adsorbent than that in bulk solution (Figure 6.7a). Such concentration polarization resulted from the repulsion effect of positively charged surface towards  $\text{Li}^+$ . In contrast, the LiAl-LDH/PSS, with a negatively charged surface and strong  $\text{Li}^+$  affinity, could compress the concentration polarization and self-enrich  $\text{Li}^+$  in the adsorbent (Figure 6.7b). These results proved that SCSD strategy develops  $\text{Li}^+$  enrichment domains on the intralayer, facilitating LiAl-LDHs to overcome the diffusion-limited Li extraction in  $\text{Li}^+$ -low brines.



**Figure 6.7** Numerical simulation of  $\text{Li}^+$  diffusion in (a) pristine LiAl-LDH and (b) LiAl-LDH/PSS.

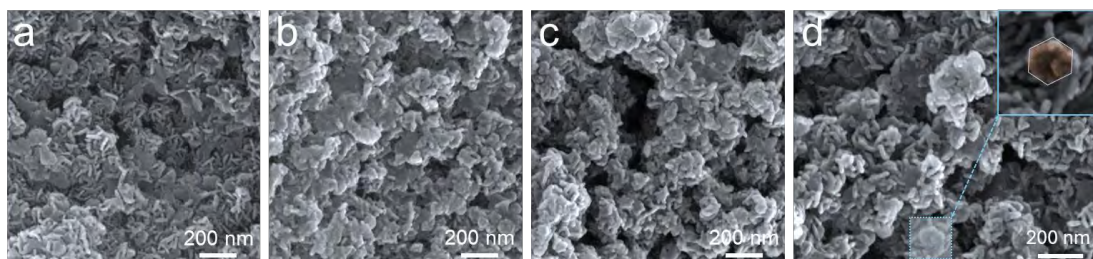


**Figure 6.8** The  $\text{Li}^+$  concentration as a function of Y distance from the results of numerical simulations.

The results of simulation calculations demonstrated that the SCSD strategy is able to develop  $\text{Li}^+$  enrichment domains on the interface, facilitating LiAl-LDHs to overcome the diffusion-limited Li extraction in low-quality brine with  $\text{Li}^+$ -low concentration. Notably, the chemical microenvironment of these functional domains and spatial microstructure of LiAl-LDHs could be fine-tuned by controlling the side chains of polymers.

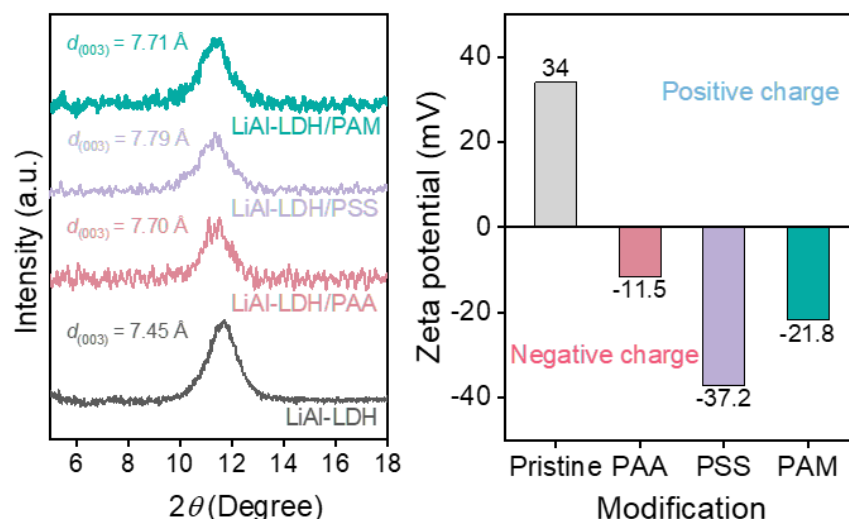
### 6.3.2. Synthesis and characterization

To test the SCSD strategy, three types of polymer-modified LiAl-LDHs (denoted as LiAl-LDH/PR, where R refers to side chain structures) were prepared to evaluate the effects of the three side chain modifiers on continuous Li recovery from sulfate-type brines. Scanning electron microscope (SEM) images showed that due to the high surface energy, all samples exhibited a typical lamellar stacking structure consisting of irregular hexagonal nanosheets with a lateral size of 80 nm (Figure 6.9). In particular, LiAl-LDH/PR were more tightly stacked after modification due to the bridging of polymers with the positively charged nanosheets.



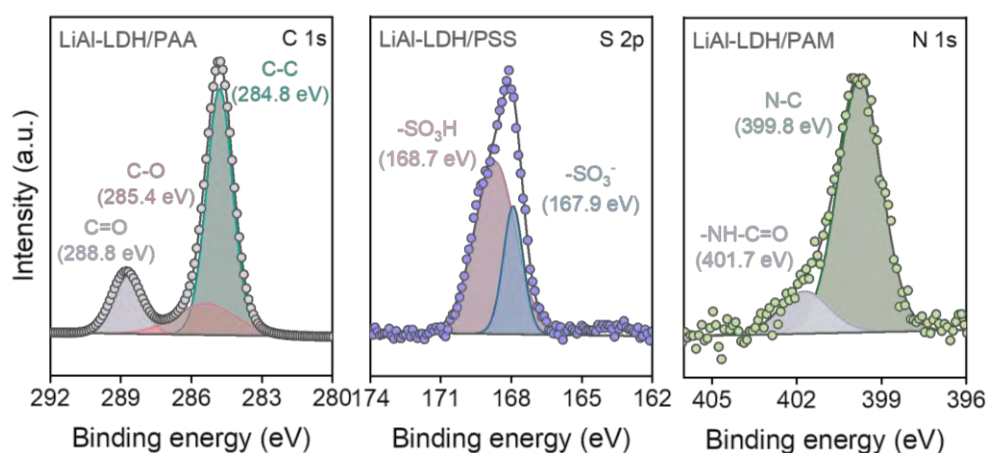
**Figure 6.9** SEM images of (a) LiAl-LDH, (b) LiAl-LDH/PAA, (c) LiAl-LDH/PAM, and (d) LiAl-LDH/PSS.

X-ray diffraction (XRD) patterns further demonstrated the successful preparation of LiAl-LDH/PR with expanded interlayer spacing (Figure 6.10a). And the modification tuned the originally positive zeta potential of pristine LiAl-LDH to negative values, indicating polymer availability on the surface, thereby enabling the electrostatic attraction towards  $\text{Li}^+$  (Figure 6.10b).

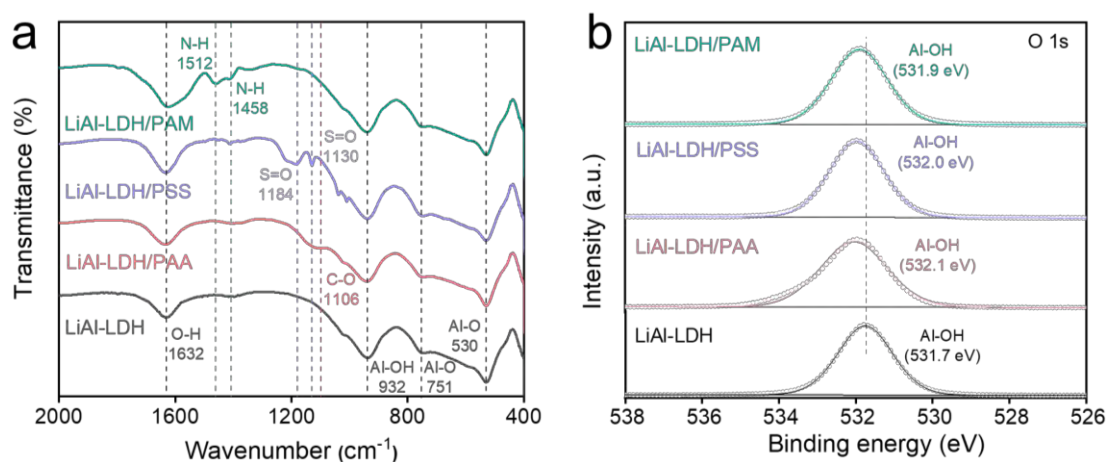


**Figure 6.10** (a) XRD patterns and (b) zeta potentials of the pristine LiAl-LDH and LiAl-LDH/PR.

X-ray photoelectron spectroscopy (XPS) spectra for the characteristic elemental C 1s, S 2p, and N 1s core levels indicated the existence of polymer modifiers with side chains of  $-\text{COOH}$ ,  $-\text{SO}_3\text{H}$ , and  $-\text{CONH}_2$  on the surface of the LiAl-LDH (Figure 6.11), which was proved by Fourier transform infrared (FT-IR) spectra (Figure 6.12b) [36-38].



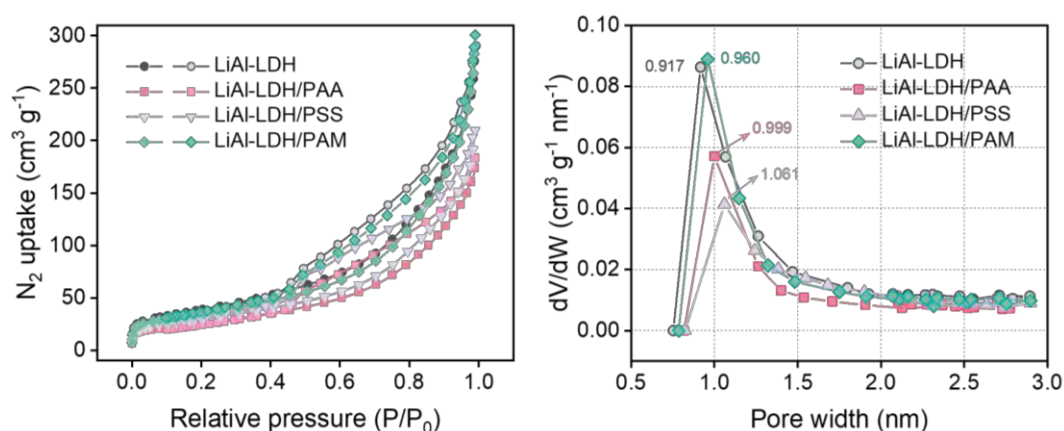
**Figure 6.11** XPS spectra for the C 1s, S 2p, and N 1s core level of the pristine LiAl-LDH and LiAl-LDH/PR.



**Figure 6.12** (a) FT-IR spectra and (b) XPS spectra for O 1s core levels of the pristine LiAl-LDH and LiAl-LDH/PR.

Furthermore, the shift of O 1s core level toward higher binding energy demonstrated the hydrogen bond interaction between the polymer modifiers and the LiAl-LDH (Figure 6.12b), where the electrons around O atoms in Al-OH were transferred to the H atoms on the polymer side chain, consistent with the ESP results [39].

Moreover, N<sub>2</sub> adsorption-desorption isotherms showed type IV reversible isotherms with H4 hysteresis loops for all LiAl-LDHs, indicating their microporous and mesoporous characteristics, which favored to eliminate concentration polarization (Figure 6.13) [14]. Brunner-Emmet-Teller specific surface areas (SSA) of LiAl-LDH/PR decreased after introducing polymers, reconfirming that polymer chains partially occupied the original surfaces and interlayer channels of LiAl-LDHs (Table 6.3) [40].

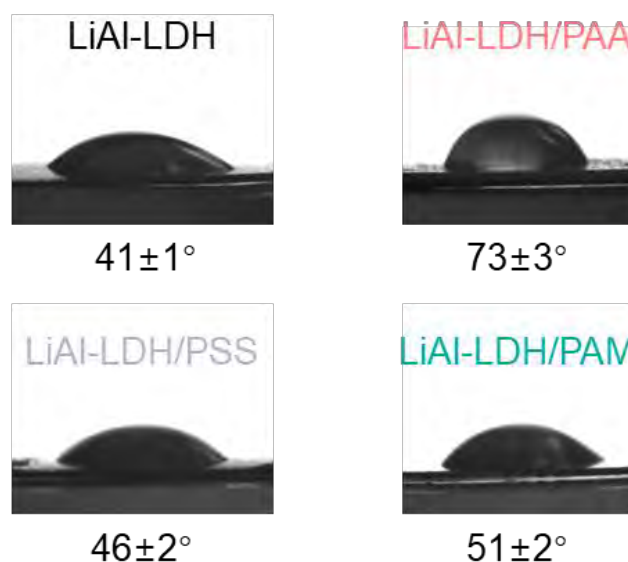


**Figure 6.13** (a) N<sub>2</sub> adsorption-desorption isotherms and (b) pore size distributions of the pristine LiAl-LDH and LiAl-LDH/PR.

**Table 6.3** The textural properties of pristine LiAl-LDH, LiAl-LDH/PAA, LiAl-LDH/PSS and LiAl-LDH/PAM.

Samples	Specific surface area ( $\text{m}^2 \text{g}^{-1}$ )	Total pore volume ( $\text{cm}^3 \text{g}^{-1}$ )	Mean pore diameter (nm)
LiAl-LDH	139.63	0.4491	12.87
LiAl-LDH/PAA	93.19	0.2836	12.17
LiAl-LDH/PSS	108.63	0.3245	11.95
LiAl-LDH/PAM	123.10	0.4654	15.12

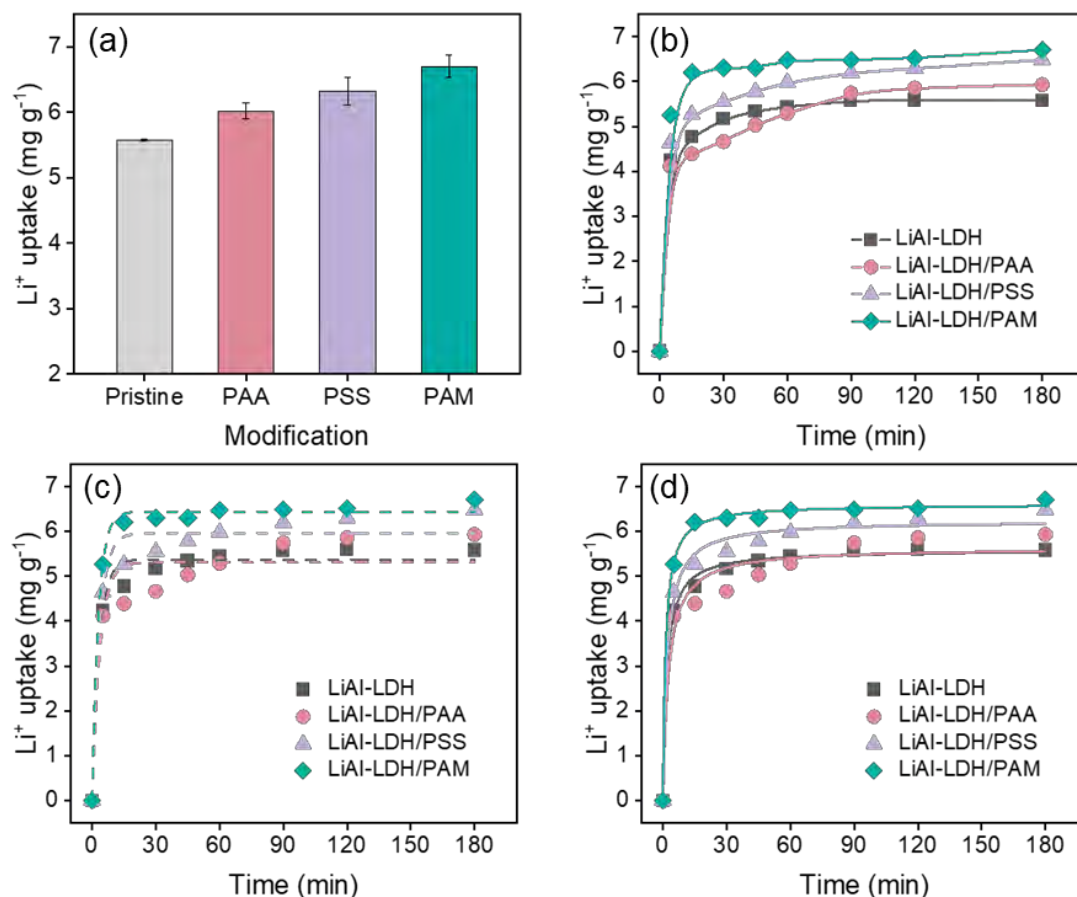
Also, polymer modification reduced the hydrophilicity of pristine LiAl-LDH, with the resulting hydrophobicity varying depending on the side chain groups (Figure 6.14). The phenomena were attributed to the hydrogen bonds between the side chain groups and the LiAl-LDH, preventing the formation of hydrogen bonds between water molecules and these groups on the LiAl-LDH surface, thus resulting in a decrease in hydrophilicity [41]. In particular, the stronger hydrogen bond connection between PAA and LDH led to the enhanced hydrophobicity of LiAl-LDH/PAA compared to the modifications with PAM and PSS.

**Figure 6.14** Contact angle images of the pristine LiAl-LDH and LiAl-LDH/PR.

### 6.3.3. Lithium extraction performance

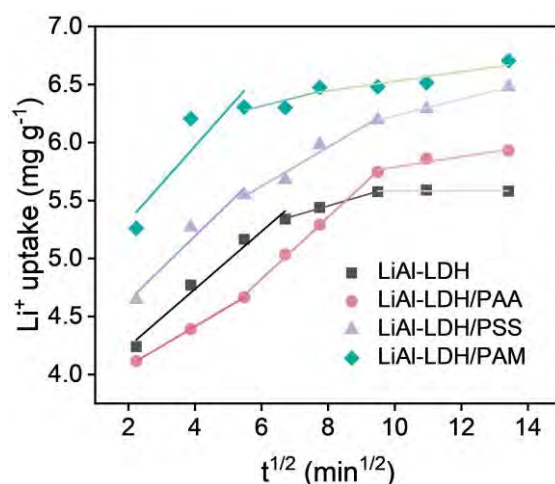
To evaluate the practical feasibility of the proposed strategy, the SCSD-designed LiAl-LDH/PR was first applied to extract lithium from Lop Nor brine that is a typical

low-quality  $\text{SO}_4^{2-}$ -type brine, occurring low  $\text{Li}^+$  concentration ( $0.222 \text{ g L}^{-1}$ ) and ultrahigh  $\text{Mg}^{2+}/\text{Li}^+$  ratio (MLR, 437). As shown in Figure 6.15a, the LiAl-LDH/PR showed improved viability for lithium extraction from such low-quality brine with significantly increased  $\text{Li}^+$  uptake ( $> 6 \text{ mg g}^{-1}$ ) compared to the pristine LiAl-LDH, which was attributed to the strong attraction of polymer modifiers towards  $\text{Li}^+$ . Kinetics experiments demonstrated the chemisorption-dominated Li extraction for four adsorbents (Figure 6.15b-d).



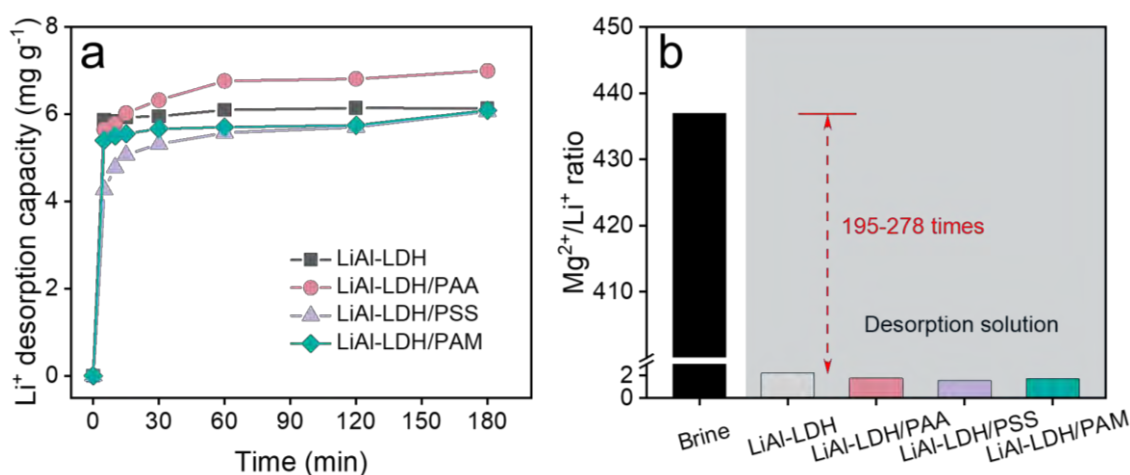
**Figure 6.15** (a)  $\text{Li}^+$  uptake and (b) uptake kinetics of the pristine LiAl-LDH and LiAl-LDH/PR in Lop Nor brine. (c) Pseudo-first-order and (d) pseudo-second-order kinetic models of  $\text{Li}^+$  uptake on the pristine LiAl-LDH and LiAl-LDH/PR.

Such extraction process fitted with three major stages of intraparticle diffusion model in our previous study[23], including rapid transfer to the intralayer, intercalation into octahedral voids, and interior diffusion to release the external active sites (Figure 6.16).



**Figure 6.16** The intraparticle diffusion model for  $\text{Li}^+$  adsorption process of the pristine LiAl-LDH and LiAl-LDH/PR in Lop Nor brine.

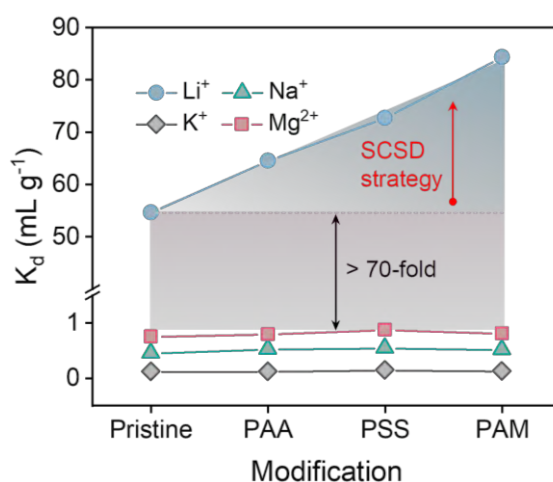
The desorption of LiAl-LDH/PR was slightly slowed due to the attraction between polymers and  $\text{Li}^+$ , whereas the complete desorption was still finished within 60 min (Figure 6.17a). Even the MLR of desorption solution of LiAl-LDH/PR dropped below 2, a reduction of more than 240 times compared to the original solution, which facilitated the subsequent  $\text{Li}^+$  recovery (Figure 6.17b).



**Figure 6.17** (a)  $\text{Li}^+$  desorption kinetics of the pristine LiAl-LDH and LiAl-LDH/PR. (b)  $\text{Mg}^{2+}/\text{Li}^+$  ratios before and after extraction by the pristine LiAl-LDH and LiAl-LDH/PR.

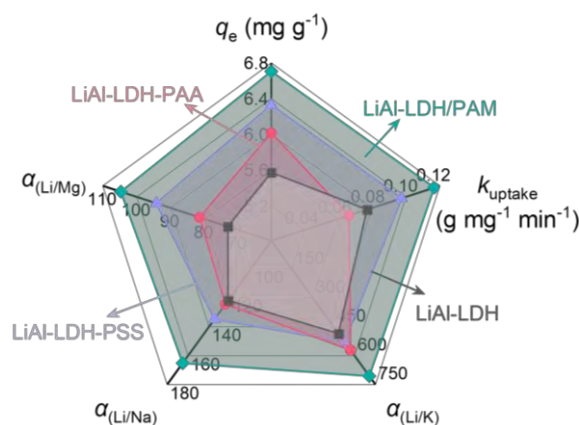
As well, the selectivity was investigated in detail. As shown in Figure 6.18, the distribution coefficient ( $K_d$ ) values of all LiAl-LDHs for  $\text{Li}^+$  were larger than 50, while those for the other main coexisting metal ions below 1, indicating the well selectivity. Further, the separation factors ( $\alpha$ ) of  $\text{Li}^+/\text{Mg}^{2+}$ ,  $\text{Li}^+/\text{Na}^+$  and  $\text{Li}^+/\text{K}^+$  were determined. The LiAl-LDH/PR presented significant higher  $\alpha_{\text{Li}/\text{Mg}}$  than pristine LiAl-LDH,

following the order: LiAl-LDH/PAM (104.65) > LiAl-LDH/PSS (94.13) > LiAl-LDH/PAA (81.37) > LiAl-LDH (72.99). Notably, sulfonate groups in the side chains of PSS offered the highest  $\text{Li}^+$  affinity according to the DFT calculation results, but both  $\text{Li}^+$  uptake and selectivity of LiAl-LDH/PSS were lower than these of LiAl-LDH/PAM. This could be explained by the fact that PSS bonded more strongly with  $\text{Mg}^{2+}$  as well, yielding the greater competition in Lop Nor brine with ultrahigh MLR. The selectivity of LiAl-LDH/PR for  $\text{Li}^+/\text{Na}^+$  and  $\text{Li}^+/\text{K}^+$  was higher than that for  $\text{Li}^+/\text{Mg}^{2+}$  due to the weaker binding of functional groups to  $\text{Na}^+$  and  $\text{K}^+$  than  $\text{Mg}^{2+}$ , and the apparently larger ionic sizes of  $\text{Na}^+$  (2.76 Å) and  $\text{K}^+$  (2.04 Å) [42].



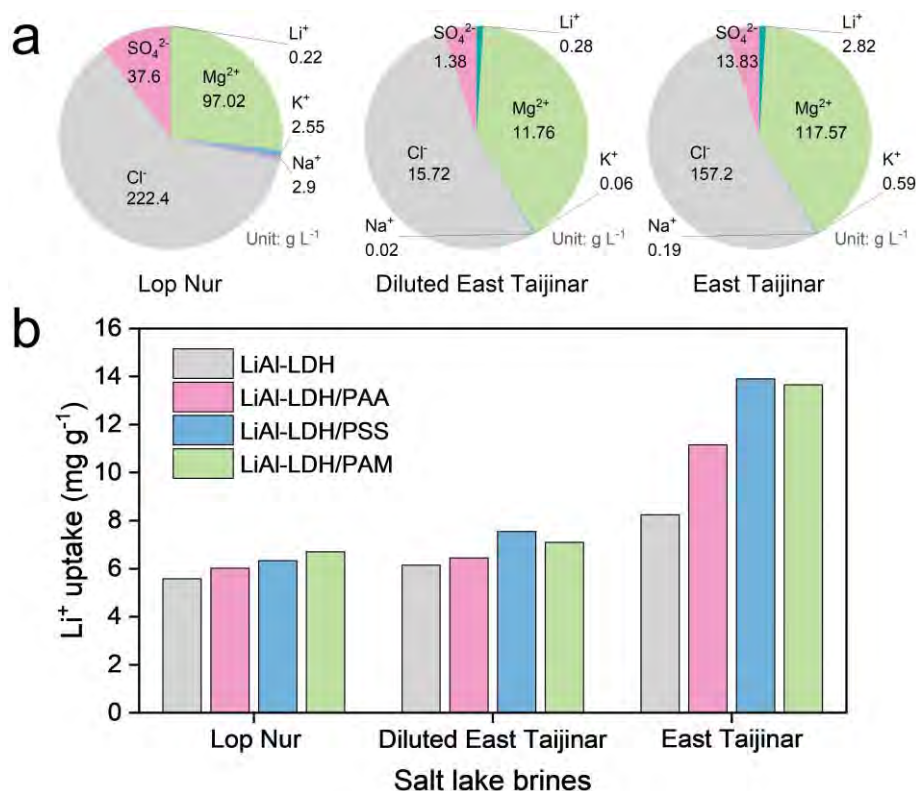
**Figure 6.18** Dispersion coefficient ( $K_d$ ) values of the pristine LiAl-LDH and LiAl-LDH/PR in Lop Nor brine.

Furthermore, the performance of LiAl-LDHs was comprehensively compared by radar chart (Figure 6.19). Generally, the  $\text{Li}^+$  uptake, adsorption efficiency and selectivity of LiAl-LDH/PR were enhanced to some extent, unveiling the sophistication of the proposed strategy for lithium extraction from low-quality brines.



**Figure 6.19** The radar chart for performance comparison analysis of LiAl-LDHs.

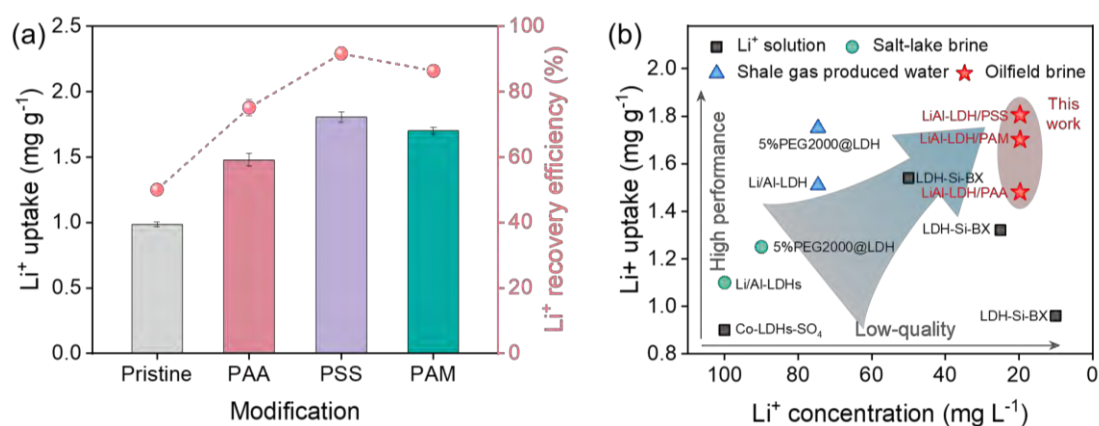
The universality of the SCSD strategy was evaluated in East Taijinar Salt-Lake brine (Figure 6.20). Due to the high  $\text{Li}^+$  concentration ( $2.82 \text{ g L}^{-1}$ ) and relatively low MLR (41.69) of East Taijinar brine, the  $\text{Li}^+$  uptake of pristine LiAl-LDH increased to  $8.25 \text{ mg g}^{-1}$ . After modification, uptake was improved to 11.15, 13.90, and  $13.65 \text{ mg g}^{-1}$  for LiAl-LDH/PAA, LiAl-LDH/PSS, and LiAl-LDH/PAM with the 35.15%, 68.48% and 65.45% higher than the pristine one, respectively (Figure 3c). Among them, LiAl-LDH/PSS demonstrated the highest uptake of  $13.90 \text{ mg g}^{-1}$ , exceeding previously reported LiAl-LDH-based adsorbents. To reveal the Li extraction performance from the brine with low  $\text{Li}^+$  concentration, East Taijinar brine was diluted ( $V_{\text{H}_2\text{O}}/V_{\text{brine}} = 9:1$ ). The similar results of enhanced  $\text{Li}^+$  uptake were observed in diluted brine, showing the availability of this strategy (Figure 6.20). To speak of, the performance of LiAl-LDH/PSS surpassed that of LiAl-LDH/PAM in East Taijinar brine before and after dilution, counter to the results in Lop Nor brine. The phenomenon resulted from the lower MLR of the former and thereby weaker competitive effect from  $\text{Mg}^{2+}$ .



**Figure 6.20** (a) Comparative analysis of brine composition (pie charts) and (b) Li uptake (bar plots) for Lop Nur brine, Diluted East Taijinar brine, and East Taijinar brine.

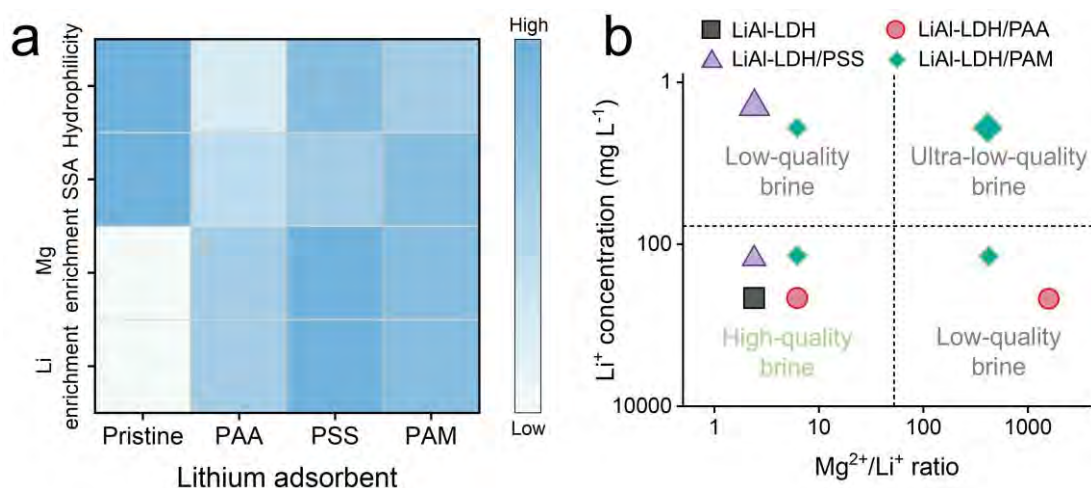
For directly exposing the advancement of the proposed strategy for lithium

extraction in low-quality brines, LiAl-LDH/PR was used for Li extraction from Qianjiang Oilfield brine with ultra-low  $\text{Li}^+$  concentration ( $19.7 \text{ mg L}^{-1}$ ). Encouragingly, LiAl-LDH/PR presented markedly improved lithium extraction efficiency in such  $\text{Li}^+$ -low brine, where  $\text{Li}^+$  recoveries were all higher than 75%, while that of pristine LiAl-LDH was less than 50%, offering the solid proof for the attraction and enrichment effects of polymer building blocks on  $\text{Li}^+$  (Figure 6.21a). Moreover, LiAl-LDH/PSS also exhibited the highest  $\text{Li}^+$  uptake in Qianjiang Oilfield brine with relatively low MLR (10.66) Compared to reported state-of-the-art LiAl-LDH-based adsorbents, the LiAl-LDH/PR demonstrates superior lithium extraction from brines with ultra-low  $\text{Li}^+$  concentration as well (Figure 6.21b).



**Figure 6.21** (a)  $\text{Li}^+$  uptake of LiAl-LDHs in Qianjiang Oilfield brine. (b) Comparison of lithium extraction of LiAl-LDH/PR to other LiAl-LDH-based adsorbents in  $\text{Li}^+$ -low aqueous with concentrations below  $100 \text{ mg L}^{-1}$ .

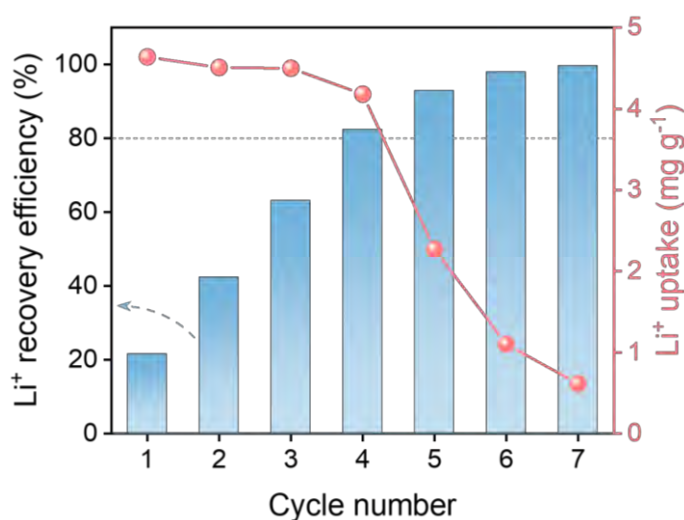
Based on above results, the lithium extraction property heatmap and application scope chart of LiAl-LDH/PR in low-quality brine were plotted (Figure 6.22). Specifically, LiAl-LDH/PSS is more suitable for brines with lower MLR, especially  $\text{Li}^+$ -low brines, due to slightly reduced SSA and hydrophilicity, and the highest  $\text{Li}^+$  enrichment effect but the strongest  $\text{Mg}^{2+}$  competitive effect. Whereas LiAl-LDH/PAM is more appropriate for brines with higher MLR than LiAl-LDH/PSS due to the high  $\text{Li}^+$  enrichment and insignificant  $\text{Mg}^{2+}$  competition, but desires higher  $\text{Li}^+$  concentration as well. Overall, the SCSD strategy enables optimized and efficient lithium extraction from a wide range of brine resources.



**Figure 6.22** (a) The lithium extraction property heatmap and (b) application scope chart of LiAl-LDH/PR in low-quality brine.

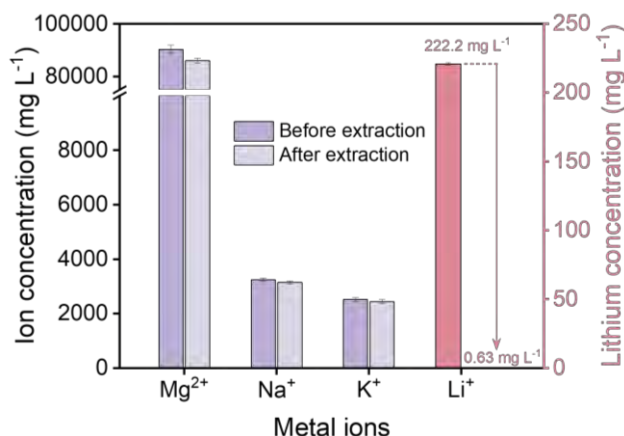
#### 6.3.4. Lithium recovery and precipitation of $\text{Li}_2\text{CO}_3$

Motivated by distinctive performance of LiAl-LDH/PAM on lithium extraction and reusability in Lop Nor brine, the repeated  $\text{Li}^+$  recovery from this brine was explored. As expected, LiAl-LDH/PAM displayed excellent stability during seven adsorption-desorption repetitions with a high  $\text{Li}^+$  recovery efficiency of 99.72% (Figure 6.23). Notably, the  $\text{Li}^+$  concentration in the brine was only  $79.8 \text{ mg L}^{-1}$  after three repetitions, while the adsorption capacity of LiAl-LDH/PAM could reach up  $4.18 \text{ mg g}^{-1}$ . These phenomena confirmed the effect of polymer modifiers in  $\text{Li}^+$  enrichment in low-quality brines with  $\text{Li}^+$ -low concentration.



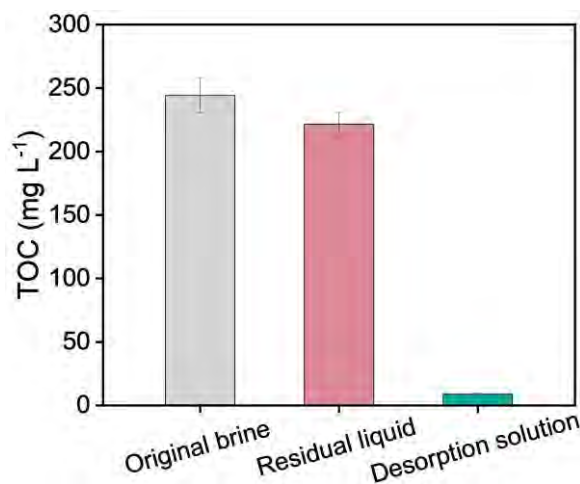
**Figure 6.23** Repeated  $\text{Li}^+$  uptake and accumulated  $\text{Li}^+$  recovery efficiency in Lop Nor brine.

Meanwhile, the  $\text{Li}^+$  concentration of the residual brine was only  $0.63 \text{ mg L}^{-1}$  after repeat extraction, indicating that LiAl-LDH/PAM is able to extract  $\text{Li}^+$  down to the ppb-level ( $< 1000$  part per billion). In contrast, the concentration of competing metal ions remained almost constant, demonstrating the ultra-stable selectivity during the repeated procedures (Figure 6.24).



**Figure 6.24** The Li extraction efficiency in Lop Nor brine.

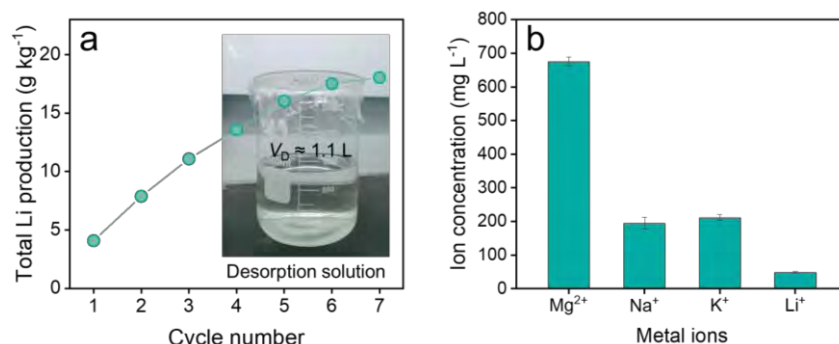
The total organic carbon (TOC) throughout the process were also detected to investigate the dissolution of the polymer modifier. The results indicated that the TOC of the residual liquid was lower than that of the original brine, and the summation of the TOC of the desorption solution coupled with the TOC of residual liquid was close to that of the original brine, which suggested almost no dissolution of PAM, revealing excellent stability (Figure 6.25).



**Figure 6.25** TOC values of original brine, residual liquid and desorption solution during the adsorption-desorption process.

In parallel, the  $\text{Li}^+$  was recovered through repeated desorption using deionized water after each Li extraction. The total lithium production at the end of the recovery

process reached  $23.92 \text{ mg g}^{-1}$  (Figure 6.26a). The concentration of all metal species in the original desorption solution was summarized in Figure 6.26b.

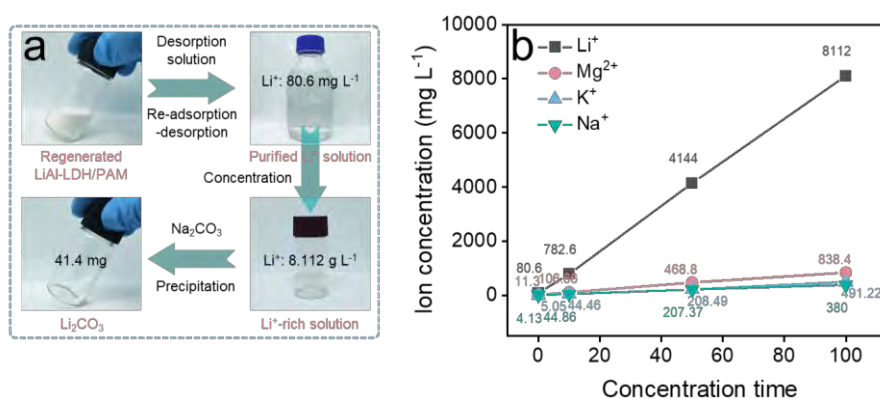


**Figure 6.26** (a) The accumulated  $\text{Li}^+$  recovery amount in the eluent. (b) The metal ion concentration of desorption solution.

Considering the unsatisfied  $\text{Li}^+/\text{Mg}^{2+}$  ratio (LMR) after only one whole adsorption-desorption repetition, another extraction-recovery using LiAl-LDH/PAM was proceeded to obtain purified  $\text{Li}^+$  solution with the LMR to 7.1 (Table 6.4). Then, a  $\text{Li}^+$ -rich solution ( $8.112 \text{ g L}^{-1}$ ) was attained by evaporation-concentration (Figure 6.27), following which excess  $\text{Na}_2\text{CO}_3$  was added into  $\text{Li}^+$ -rich solution at  $80^\circ\text{C}$  to induce lithium precipitation.

**Table 6.4** Composition variation during the re-adsorption-desorption purification of desorption solution.

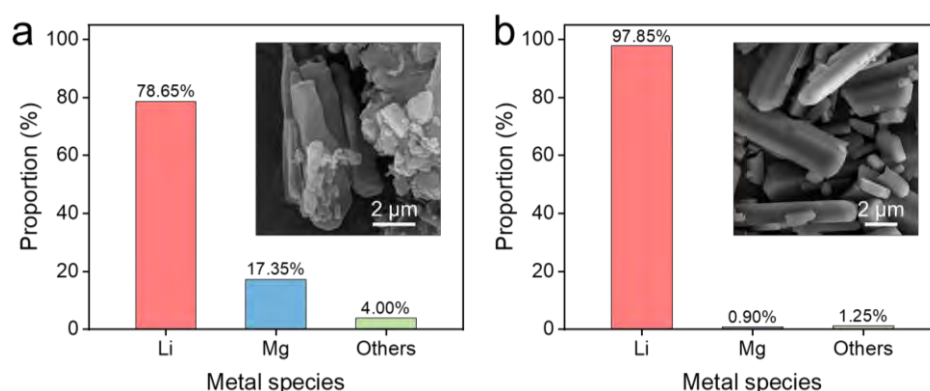
Solution	Composition ( $\text{mg L}^{-1}$ )			
	$\text{Li}^+$	$\text{Mg}^{2+}$	$\text{K}^+$	$\text{Na}^+$
Original desorption solution	49.5	675.66	211.41	195.11
Residual solution	3.7	624.53	176.57	206.83
Purified solution	80.6	11.3	5.05	4.13



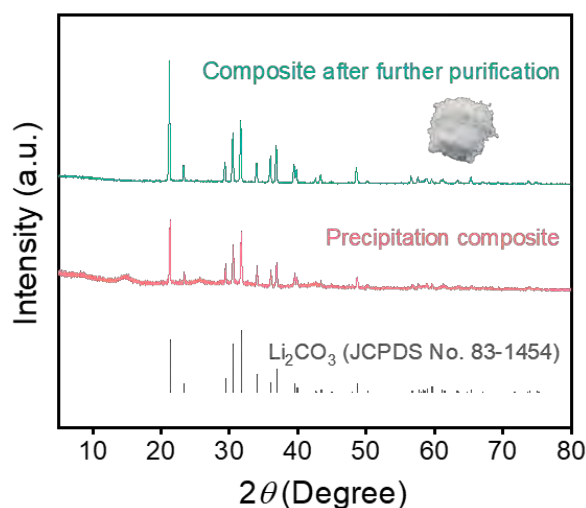
**Figure 6.27** (a) Schematic diagram of the purification-concentration-precipitation

process for  $\text{Li}_2\text{CO}_3$  production. (b) Change curves of metal ion concentration during the concentration stage of desorption solution.

The proportion of metal species in the precipitation was analyzed by ICP optical emission spectrometer (ICP-OES) test (Figure 6.28a). The proportion of Li was 78.65% among the metal elements. Further, a dissolution-reprecipitation process was conducted to purify lithium product. The resulting  $\text{Li}_2\text{CO}_3$  showed a purity of 97.85% (Figure 6.28b), approaching the battery-grade standard, and was characterized by SEM and XRD.



**Figure 6.28** The proportion of lithium among the metal species in (a) the precipitation powder and (b) the purification powder. Inset is SEM images of the corresponding powder.



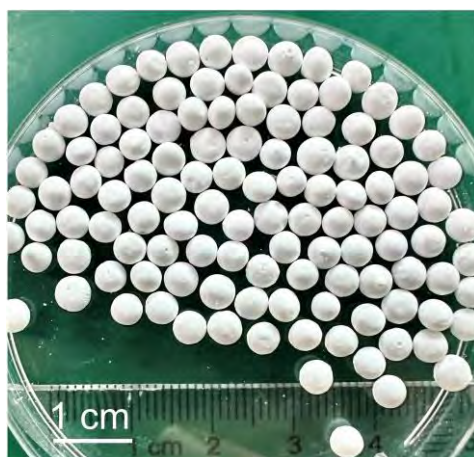
**Figure 6.29** XRD patterns of precipitated  $\text{Li}_2\text{CO}_3$  before and after purification. Inset picture is the obtained  $\text{Li}_2\text{CO}_3$  product.

The lithium extraction and recovery using  $\text{LiAl-LDH/PAM}$  was unable to generate battery-grade  $\text{Li}_2\text{CO}_3$  directly, however, the near 98% purity achieved by adsorption alone suggested that the vast majority of impurity ions had been removed from the brine,

which was clearly conducive to the subsequent membrane and resin treatment processes.

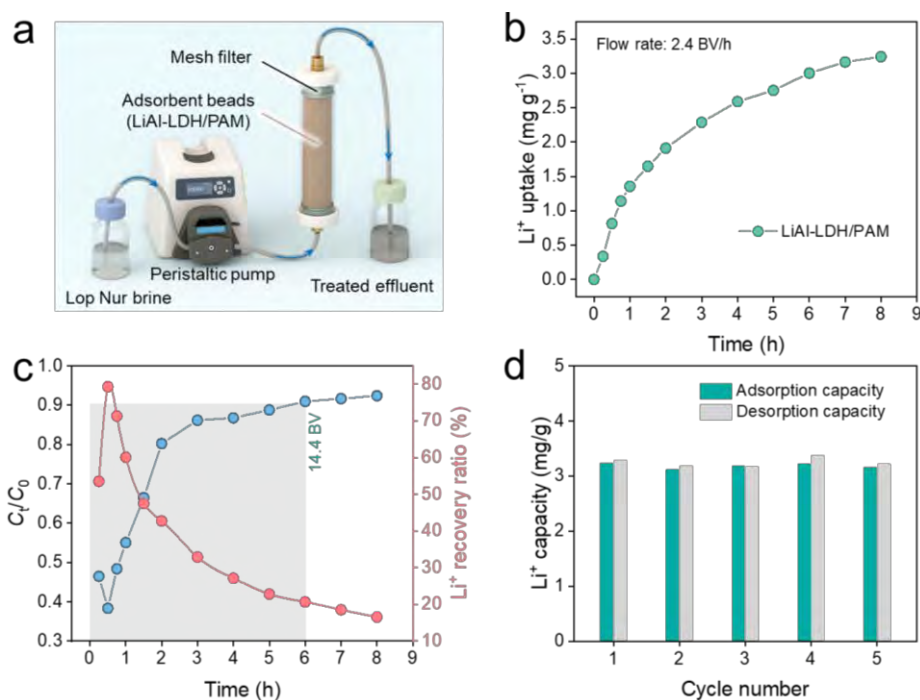
### 6.3.5. Practical application assessment

To explore the industrial application potential of SCSD-engineered LiAl-LDHs, LiAl-LDH/PAM beads were prepared based on the method presented in Section 4.2.2. In brief, the high mechanical polyvinyl chloride (PVC) and hydrophilic polyacrylonitrile (PAN) were selected as the hybrid binders. LiAl-LDH/PAM powders were mixed with PAN/PVC in weight ratio of 8:2 using DMF as solvent to produce adsorption-binder slurry, and then the slurry was dropped into deionized water using the injector to form adsorbent beads. As shown in Figure 6.30, the resultant LiAl-LDH/PAM beads appeared white with the diameters of  $\sim 3$  mm.



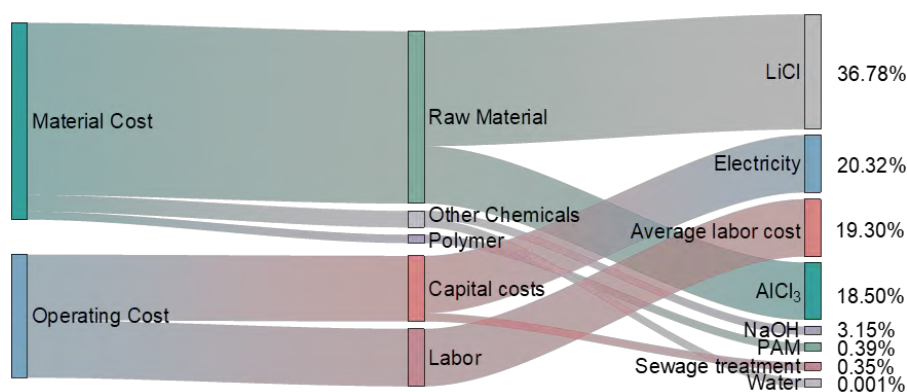
**Figure 6.30** The optical photograph of the LiAl-LDH/PAM beads.

Further, to evaluate the dynamic lithium extraction performance of SCSD-engineered LiAl-LDHs, LiAl-LDH/PAM beads were loaded into a fixed bed with an inner diameter of 2.5 cm and a bed height of 30 cm for the dynamic lithium extraction (Figure 6.31a). In a typical dynamic adsorption process, Lop Nor brine was pumped from the bottom at 2.4 BV/h for 8h, with  $C/C_0 = 0.9$  as the adsorption breakthrough point. Then, ice water of 20 mL was quickly pumped from the top for a washing process. Next, the desorption process was performed using deionized water from the bottom at 1.2 BV/h for 2 h. After treating 19.2 bed volumes (BV) of Lop Nor brine, the beads achieved a high total  $\text{Li}^+$  adsorption capacity of  $3.24 \text{ mg g}^{-1}$  (Figure 6.31b). The  $\text{Li}^+$  breakthrough curve of LiAl-LDH/PAM beads showed a breakthrough point of up to 12.4 BV, highlighting the excellent dynamic lithium extraction performance (Figure 6.31c). Moreover, beads maintained stable performance over five adsorption-desorption cycles, demonstrating the strong practical applicability (Figure 6.31d).



**Figure 6.31** (a) Schematic of the fixed bed column device, (b) Li<sup>+</sup> adsorption capacity curves, (c) Li<sup>+</sup> breakthrough and recovery ratio curves in dynamic lithium extraction process, and (d) the dynamic adsorption-desorption cycling adsorption performance of LiAl-LDH/PAM beads.

Finally, the economic viability of the SCSD-engineered LiAl-LDH/PAM was evaluated. The economic process for practical production conditions was simulated using the latest prices of each raw material (Table 6.5). The Sankey diagram presented the major expenses involved in the production of LiAl-LDH/PAM. LiCl accounts for 36.78% of the material cost, whereas PAM contributes only 0.39%, indicating an almost negligible increase in cost from polymer modifier (Figure 6.32). According to the production economic analysis, the production cost of LiAl-LDH/PAM is estimated at \$5.28 per kilogram, demonstrating its strong practical competitiveness.



**Figure 6.32** Inputs and shares of the preparation of the LiAl-LDH/PAM.

**Table 6.5** Prices of substances required to synthesize materials.

	Item	Market price	Unit	Update date	Date source
1	LiCl	67	¥/kg	15-August-25	100PPI
2	AlCl <sub>3</sub>	5.35	¥/kg	15-August-25	100PPI
3	PAM (anionic, 18 million molecular weight)	3.4	¥/kg	15-August-25	100PPI
4	NaOH	0.859	¥/kg	15-August-25	100PPI
5	Water	0.005	¥/kg	15-August-25	100PPI
6	Electricity	0.67	¥Kw/h	15-August-25	BDB
7	Average labor cost	7000	¥/month	15-August-25	JOBUI
8	Sewage treatment	3.00	¥/t	15-August-25	BDB

Note: a. Chemical raw materials are industrial grade.

b. 1 \$ = 7.18 ¥ (Update time: 2025/08/15).

c. Data Sources: 100PPI (<http://www.100ppi.com/ppi>), BDB (<http://sz.bendibao.com/>), and JOBUI (<https://www.jobui.com/>).

## 6.4. Conclusions

In conclusion, to tackle issues of low efficiency of lithium extraction of LiAl-LDHs in low-quality brines, a proof-of-concept polymer side-chain structure design (SCSD) strategy was developed for construction of a Li<sup>+</sup> enrichment domain on the intralayer of the LiAl-LDHs. Such functional domain enabled LiAl-LDH/PR to overcome the diffusion-limited Li<sup>+</sup> uptake caused by the Li<sup>+</sup>-low concentration, which delivered an 83.1% increase in Li<sup>+</sup> uptake over pristine LiAl-LDH and an ultrahigh recovery efficiency of 91.62% from genuine oilfield brine with ultra-low Li<sup>+</sup> concentration. The maximum uptake was as high as 13.9 mg g<sup>-1</sup>, exceeding most of the reported LiAl-LDH-based adsorbents. Additionally, the LiAl-LDH/PR exhibited robust lithium extraction from Lop Nor brine, the one of the largest low-quality brines in the world, by the continuous extraction procedure, enabling residual concentrations down to ppb level. On the basis of these merits, high-purity (97.85%) Li<sub>2</sub>CO<sub>3</sub> was produced from the brine using LiAl-LDH/PR. The concept of SCSD can modulate local microenvironment and spatial microstructure of LiAl-LDHs by tuning side-chain groups, that provides a versatile strategy for sustainable lithium extraction from low-quality brines, and can be extended to other kinds of brines or for the extraction of other

critical resources.

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## Chapter 7. Conclusions

Global electrification and decarbonization drive exponentially growing lithium (Li) demand. While brines offer a virtually abundant lithium source for the sustainable supply of Li, the efficient and stable Li extraction from brines are challenging, even for the industrialized lithium-aluminum layered double hydroxides (LiAl-LDHs) lithium ion-sieves. Several crucial concerns remain regarding lithium extraction by LiAl-LDHs: i) low  $\text{Li}^+$  adsorption capacity; ii) ‘ $\text{SO}_4^{2-}$ -poisoning’ effect in sulfate-type brines; iii) poor efficiency in low-quality brines. In this thesis, a series of state-of-art LiAl-LDH-based adsorbents have been innovated and designed to address the bottlenecks of current LiAl-LDHs based on their intrinsic structures and properties. The findings are of sufficient impact to ion-sieve development and Li extraction from brines communities. The general conclusions are summarized as follows:

1. The doping engineering strategy was developed to fabricate novel  $\text{Zn}^{2+}$ -doped LiAl-LDHs (LiZnAl-LDH) with superior Li extraction performance. This strategy endowed tunable surface properties and favorable nanostructures, which enabled the stronger adsorption energy ( $E_{\text{ad}}$ ) towards  $\text{Li}^+$ , reduced Gibbs free energy ( $\Delta G$ ) for  $\text{Li}^+$  transfer and insertion lithium, and depressed diffusion energy barrier of  $\text{Li}^+$ . Accordingly, the maximum adsorption capacity for  $\text{Li}^+$  was raised by about 39% than without doping, while the  $\text{Li}^+/\text{K}^+$ ,  $\text{Li}^+/\text{Na}^+$ , and  $\text{Li}^+/\text{Mg}^{2+}$  selectivity in Lop Nor brine is as high as 213, 834, and 171, respectively.

2. The steering interlayer interaction strategy was developed to introduce  $\text{PO}_4^{3-}$  into the interlayer of beaded LiAl-LDHs (BLDH-P) prevents the intercalation of  $\text{SO}_4^{2-}$  by selective electrostatic repulsion and enhanced diffusion energy barrier. Based on the rational design, the adsorption and desorption capacity of LiAl-LDHs remained almost identical during the cycling extraction in Lop Nor brine, the largest  $\text{SO}_4^{2-}$ -type brine in the world. Besides, the static and dynamic  $\text{Li}^+$  uptake reached 5.26 mg/g and 3.96 mg/g with a minimum 105% higher selectivity, superior to those of reported and commercialized adsorbents.

3. The organic modification strategy was developed to construct multiple functional domains of LiAl-LDHs (LiAl-LDH/PAM) using polyacrylamide (PAM) for sustainable lithium extraction in  $\text{SO}_4^{2-}$ -type brines. Through creating multiple  $\text{SO}_4^{2-}$ -repelling domains in the interface and interlayer of the LiAl-LDH/PAM, the energy

barrier for  $\text{SO}_4^{2-}$  migration over interface and interlayer was increased, which offered extraordinary anti-sulfate poisoning during long-term Li cycling extraction in Lop Nor brine. The anti-sulfate poisoning properties exceeded all previously reported LiAl-LDHs.

4. The proof-of-concept polymer side-chain structure design (SCSD) strategy was developed that delivers intralayer engineering of LiAl-LDHs (LiAl-LDH/PR) with functional polymers for efficient and highly selective Li extraction from low-quality brines. The SCSD strategy engineered LiAl-LDH/PR with a  $\text{Li}^+$ -enriched intralayer domain that can be readily tuned through rational designs of side-chains of polymer to accommodate lithium extraction from different brines. Accordingly, LiAl-LDH/PR realized an ultrahigh recovery efficiency of 91.62% from genuine oilfield brine with ultra-low  $\text{Li}^+$  concentration. Moreover, sustainable Li extraction enables ppb-level  $\text{Li}^+$  residual concentration and high-purity  $\text{Li}_2\text{CO}_3$  production from the world's largest low-quality salt lake brine.

## Chapter 8. Perspectives

In this thesis, several promising strategies were developed for improving the efficiency, stability, and feasibility of LiAl-LDHs. Despite considerable progresses, high-efficiency lithium extraction using LiAl-LDHs remains difficulties and challenges in terms of discovery of new materials with various cation-doping and/or anion intercalation, and availability in lithium resources with lower  $\text{Li}^+$  concentration (e.g., seawater). The following two perspectives can provide promising views.

### **Interpretable machine learning (ML) for rapid determination of high-performance modification strategies.**

While the feasibility of the  $\text{Zn}^{2+}$ -doping and  $\text{PO}_4^{3-}$ -intercalation strategies has been verified, it does not represent that they are the most optimal solutions. Obviously, the workload associated with the preparation and performance verification for the doping and intercalation of LiAl-LDHs is complicated, time-consuming and costly.

With the coming of the era of artificial intelligence, machine learning (ML) methods have shown great potential in reducing experimental costs and accelerating the discovery of new materials. These methods established a link between the raw structure or experimental conditions and the target performance, enabling rapid prediction of properties of modified LiAl-LDHs and increasing screening efficiency greatly.

### **Solar-driven direct lithium extraction and water harvesting from seawater**

Seawater is a vast treasure trove of lithium resources, with over 230 billion tons. However, efficient lithium extraction from seawater by current evaporation and the direct lithium extraction techniques (e.g., LiAl-LDHs ion-sieving) suffers from inefficiency and energy-intensity due to the low concentration of lithium ions ( $\text{Li}^+$ ) ( $\sim 0.2 \text{ mg L}^{-1}$ ) and high concentration of interfering ions ( $500\text{-}10000 \text{ mg L}^{-1}$ ) in seawater.

Solar-driven direct lithium extraction (SDLE) systems combining conventional evaporation and DLE techniques can overcome the present challenges of Li extraction, allow for spontaneous, continuous  $\text{Li}^+$  transport and enrichment under sunlight, achieving efficient and durable lithium extraction from seawater, and promise to advance the exploitation of low-quality brines while simultaneously producing fresh water.

It is convinced for me that ML and SDLE techniques, through continuous evolution, offers a unique perspective on the sustainable development of lithium resources and an important avenue for solving global energy and water issues.

## Appendix I. Articles published during the Ph. D studies

(\*indicates corresponding author.)

[1] **Lingjie Zhang**, Yunjia Ling, Jianglin Yan, Zhenlei Wang, Yanhui Miao, Haoyu Bai, Tingting Zhang, Shaoxian Song, Mildred Quintana, Yunliang Zhao. Charged two-dimensional nanochannels with high ion density enabling ultrafast monovalent and multivalent ion conductivity. *Chem. Sci.*, 2026, 17, 1735-1744. (JCR Q1, **Nature Index**)

[2] **Lingjie Zhang**, Jianglin Yan, Zhenlei Wang, Tingting Zhang, Shaoxian Song, Mildred Quintana, Yunliang Zhao. Solar-Driven Direct Lithium Extraction from Low-Quality Brines. *Adv. Mater.*, 2026, 38, e12998. (JCR Q1, **IF 26.8, Nature Index**)

[3] **Lingjie Zhang**, Jianglin Yan, Shichang Kang, Zhenlei Wang, Yanhui Miao, Renbo Gao, Tingting Zhang, Hiram Joazet Ojeda-Galván, Mildred Quintana, Haoyu Bai, Shaoxian Song, Yunliang Zhao. Tailoring Multiple Functional Domains of Lithium-Ion Sieves for Sustainable Lithium Extraction from Low-Quality Brines. *ACS NANO*, 2025, 19, 33620-33631. (JCR Q1, **IF 16.1, Nature Index**)

[4] **Lingjie Zhang**, Zhenlei Wang, Tingting Zhang, Xiongrui Jiang, Licai Chen, Hiram Joazet Ojeda Galván, Mildred Quintana, Shaoxian Song, Sridhar Komarneni, Yunliang Zhao. Bioinspired Tunable Subnanochannels in Two-Dimensional Montmorillonite Membranes for Fast and Stable Proton Transport. *ACS Materials Lett.*, 2025, 7, 2835-2843. (JCR Q1, **Highlighted as Front Cover Paper**)

[5] **Lingjie Zhang**, Tingting Zhang, Shuaike Lv, Shaoxian Song, Hiram Joazet Ojeda Galván, Mildred Quintana, Yunliang Zhao. Adsorbents for lithium extraction from salt lake brine with high magnesium/lithium ratio: from structure-performance relationship to industrial applications. *Desalination*, 2024, 579, 117480. (JCR Q1, **ESI Highly Cited Paper**)

[6] **Lingjie Zhang**, Tingting Zhang, Yunliang Zhao, Guangfeng Dong, Shuaike Lv, Songliang Ma, Shaoxian Song, Mildred Quintana. Doping engineering of lithium-aluminum layered double hydroxides for high-efficiency lithium extraction from salt lake brines. *Nano Res.*, 2024, 17(3): 1650-1658. (JCR Q1, **ESI Hot Paper, ESI Highly Cited Paper, Top Papers Award 2025**)

- [7] **Lingjie Zhang**, Tingting Zhang, Shuaike Lv, Shuai Cheng, Guangfeng Dong, Mildred Quintana, Shaoxian Song, Yunliang Zhao. Steering interlayer interaction of lithium-aluminum layered double hydroxide beads for stable lithium extraction from sulfate-type brines. *Desalination*, 2024, 592, 118130. (JCR Q1)
- [8] **Lingjie Zhang**, Tingting Zhang, Yue Cai, Yunliang Zhao, Shaoxian Song, Mildred Quintana. Engineering sulfuric acid-pretreated biochar supporting MnO<sub>2</sub> for efficient toxic organic pollutants removal from aqueous solution in a wide pH range. *J. Clean. Prod.*, 2023, 416, 137968. (JCR Q1)
- [9] Ying Li, **Lingjie Zhang\***, Licai Chen, Yanhui Miao, Jierui Wang, Bowen Kuang, Tingting Zhang, Yunliang Zhao. Interlocking nanoconfined two-dimensional montmorillonite membranes for precise and sustainable antibiotic desalination. *J. Environ. Chem. Eng.*, 2026, 14, 121132. (JCR Q1)
- [10] Xiongrui Jiang, **Lingjie Zhang\***, Yanhui Miao, Licai Chen, Jiaoyan Liu, Tingting Zhang, Shuai Cheng, Yuhan Song, Yunliang Zhao. Intrinsic roles of nanosheet characteristics in two-dimensional montmorillonite membranes for efficient Li<sup>+</sup>/Mg<sup>2+</sup> separation, *Water Res.*, 2025, 276, 123291. (JCR Q1, **ESI Highly Cited Paper, Nature Index**)
- [11] Zhenlei Wang, Lianqiu Huang, **Lingjie Zhang\***, Tingting Zhang, Jianglin Yan, Licai Chen, Xiongrui Jiang, Damiano Sarocchi, Shaoxian Song, Viridiana García Meza, Mildred Quintana, Yunliang Zhao. A dual-constrained assembly strategy of highly aligned two-dimensional montmorillonite membranes for efficient proton transport, *J. Mater. Chem. A*, 2025, 13, 25489-25497. (JCR Q1)
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[14] Tingting Zhang, Yinxing Zhao, **Lingjie Zhang\***, Qiwu Zhang, Guangsen Song, Guozhi Fan, Yunliang Zhao. Efficient removal of para arsanilic acid with Ca-Al-Fe composite: Performances and mechanisms, *J. Mol. Liq.* 2023, 388, 122773. (JCR Q1)

## Appendix II. Experimental data

**Table II.1** The  $\text{Li}^+$  adsorption capacity of LiZnAl-LDH with different  $\text{Zn}^{2+}$  doping amounts in brine.

Time (min)	Adsorption capacity (mg/g)				
	LiAl-LDH	LiZnAl-LDH-1%	LiZnAl-LDH-5%	LiZnAl-LDH-10%	LiZnAl-LDH-20%
0	0	0	0	0	0
2	3.408	4.032	4.3	4.41	3.715
5	3.993	4.651	4.915	5.055	4.205
15	4.831	5.065	5.485	5.445	4.76
30	4.934	5.367	5.645	5.71	4.87
60	5.031	5.670	5.89	5.845	4.99
180	5.114	5.792	6.04	6.005	5.235

**Table II.2** The selectivity of LiZnAl-LDH with different content of  $\text{Zn}^{2+}$  for  $\text{Li}^+/\text{K}^+$ ,  $\text{Li}^+/\text{Na}^+$ ,  $\text{Li}^+/\text{Mg}^{2+}$  in brine.

$\text{Li}^+/\text{M}$	Selectivity				
	LiAl-LDH	LiZnAl-LDH-1%	LiZnAl-LDH-5%	LiZnAl-LDH-10%	LiZnAl-LDH-20%
$\text{K}^+$	65.75	121.31	213.07	193.03	53.82
$\text{Na}^+$	68.07	104.31	834.16	465.30	414.19
$\text{Mg}^{2+}$	75.09	149.36	171.32	184.49	80.52

**Table II.3** The mass losses, dissolution amounts of  $\text{Al}^{3+}$  and dissolution COD of BLDH-P beads with various PVC/PAN ratios in strong acid and alkali solutions

Time (min)	Dissolution of material									
	PAN-0%		PAN-20%		PAN-40%		PAN-50%		PAN-60%	
	pH=3	pH=11	pH=3	pH=11	pH=3	pH=11	pH=3	pH=11	pH=3	pH=11
Mass	4.86	3.57	5.28	5.41	5.75	5.74	5.67	5.90	6.61	6.46
$\text{Al}^{3+}$	0.31	0.00	0.42	0.00	0.30	0.00	0.55	0.00	0.38	0.00
COD	1.09	1.16	1.27	1.26	1.52	1.50	1.20	1.17	1.38	1.36

**Table II.4** The Li<sup>+</sup> adsorption capacity of BLDH-P beads with various PVC/PAN ratios.

Time (h)	Adsorption capacity (mg/g)				
	PAN-0%	PAN-20%	PAN-40%	PAN-50%	PAN-60%
0	0	0	0	0	0
1	1.235	1.43	1.85	1.855	2.04
2	1.935	2.015	2.39	2.47	2.645
4	2.84	2.875	3.09	3.43	3.575
6	3.175	3.57	3.625	3.765	3.87
18	4.525	4.63	4.825	5.03	5.015
24	4.86	5.11	5.19	5.38	5.345

**Table II.5** Adsorption kinetics I of Li<sup>+</sup> on BLDH-P and BLDH-Cl during the adsorption process.

Time (h)	Adsorption capacity (mg/g)	
	BLDH-P	BLDH-Cl
0	0	0
0.25	0.955	0.635
0.5	1.36	1.135
1	1.98	1.56
2	2.47	2.235
4	2.975	2.73
6	3.405	3.145
8	3.82	3.51
10	4.095	3.705
12	4.2	3.86
24	4.855	4.52

**Table II.6** The Li<sup>+</sup> breakthrough curves and the Li<sup>+</sup> dynamic adsorption curves of BLDH-Cl and BLDH-P.

Effluent volume (mL)	BLDH-P		Effluent volume (mL)	BLDH-Cl	
	C <sub>t</sub> /C <sub>0</sub>	q <sub>t</sub> (mg/g)		C <sub>t</sub> /C <sub>0</sub>	q <sub>t</sub> (mg/g)
0.00	0.14	0.00	0.00	0.41	0.00
58.08	0.27	0.62	55.50	0.22	0.37
116.17	0.43	1.09	111.00	0.48	1.08
174.25	0.53	1.42	166.50	0.59	1.35
232.33	0.60	1.70	222.00	0.64	1.59
290.42	0.66	1.94	277.50	0.68	1.82
348.50	0.68	2.14	333.00	0.72	1.99
406.58	0.72	2.58	388.50	0.74	2.22
522.75	0.78	2.84	444.00	0.77	2.39
638.92	0.80	3.09	499.50	0.80	2.61
755.09	0.83	3.38	610.50	0.83	2.82
871.25	0.84	3.65	721.50	0.85	3.08
987.42	0.86	3.90	832.50	0.86	3.34
1103.59	0.87	3.96	943.50	0.89	3.46

**Table II.7** The Li<sup>+</sup> adsorption kinetics of LiAl-LDH, LiAl-LDH/PAA, LiAl-LDH/PSS, and LiAl-LDH/PAM.

Time (min)	Adsorption capacity (mg/g)			
	LiAl-LDH	LiAl-LDH/PAA	LiAl-LDH/PSS	LiAl-LDH/PAM
5	4.24	4.115	4.645	5.26
15	4.77	4.39	5.27	6.205
30	5.165	4.665	5.55	6.305
45	5.34	5.035	5.68	6.3
60	5.44	5.29	5.98	6.475
90	5.575	5.745	6.195	6.48
120	5.59	5.86	6.29	6.515
180	5.58	5.93	6.48	6.705

**Table II.8** Li<sup>+</sup> uptakes of LiAl-LDHs during the adsorption-desorption cycling experiments.

Cycle number	Adsorption (Ads.)/Desorption (Des.) capacity (mg/g)							
	LiAl-LDH		LiAl-LDH/PAA		LiAl-LDH/PSS		LiAl-LDH/PAM	
	Ads.	Des.	Ads.	Des.	Ads.	Des.	Ads.	Des.
1	6.135	6.995	6.085	6.060	5.580	5.930	6.480	6.705
2	7.137	6.650	6.745	7.328	6.233	5.930	6.058	6.885
3	6.750	6.682	6.248	6.681	6.148	5.325	6.080	6.805
4	5.943	5.474	5.173	6.257	5.698	5.723	5.943	6.525
5	5.570	4.794	4.959	5.669	5.238	5.108	5.648	6.463
6	4.251	4.541	5.245	5.759	4.905	5.493	5.790	6.300
7	4.559	4.346	4.209	5.975	4.435	5.593	5.900	6.503
8	4.891	4.481	4.911	5.911	4.340	5.070	5.603	6.420
9	4.042	4.658	4.806	5.898	4.003	4.790	5.250	6.153
10	3.779	4.469	4.980	5.588	3.678	4.748	5.438	6.208

**Table II.9** The Li<sup>+</sup> adsorption isotherms of LiAl-LDH, LiAl-LDH/PAA, LiAl-LDH/PSS, and LiAl-LDH/PAM.

Li <sup>+</sup> concentration (mg/L)	Adsorption capacity (mg/g)			
	LiAl-LDH	LiAl-LDH/PAA	LiAl-LDH/PSS	LiAl-LDH/PAM
213	5.58	5.93	6.48	6.705
412.4	7.24	7.16	7.78	8.22
562.6	8.59	8.89	9.53	10.05
730	9.24	9.34	9.76	10.94
894.8	9.42	9.7	10.08	11.58

**Table II.10** The selectivity of LiAl-LDH, LiAl-LDH/PAA, LiAl-LDH/PSS, and LiAl-LDH/PAM for  $\text{Li}^+/\text{K}^+$ ,  $\text{Li}^+/\text{Na}^+$ ,  $\text{Li}^+/\text{Mg}^{2+}$  in brine.

$\text{Li}^+/\text{M}$	Selectivity			
	LiAl-LDH	LiAl-LDH/PAA	LiAl-LDH/PSS	LiAl-LDH/PAM
$\text{K}^+$	483.74	569.61	526.44	705.52
$\text{Na}^+$	122.08	124.65	134.96	165.24
$\text{Mg}^{2+}$	73.00	81.37	94.13	104.64